

Groundwater Transfer Review Summary Form

Transfer/PA # T- 13973

GW Reviewer Gerald H. Grondin

Date Review Completed: 19 December 2022

Summary of Same Source Review:

☐ The proposed change in point of appropriation is not within the same aquifer as per OAR 690-380-2110(2).

Summary of Injury Review:

☐ The proposed transfer will result in another, existing water right not receiving previously available water to which it is legally entitled or result in significant interference with a surface water source as per 690-380-0100(3).

Summary of GW-SW Transfer Similarity Review:

☐ The proposed SW-GW transfer doesn't meet the definition of "similarly" as per OAR 690-380-2130.

☒ None of the Above

This is only a summary. Documentation is attached and should be read thoroughly to understand the basis for determinations.



Oregon Water Resources Department
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Ground Water Review Form:

- ☒ **Water Right Transfer**
☐ **Permit Amendment**
☐ **GR Modification**
☐ **Other**

Application: **T-13973**

Applicant Name: **Daniel Roth**

Proposed Changes: ☒ POA ☐ APOA ☐ SW→GW ☐ RA
☐ USE ☒ POU ☐ OTHER

Reviewer(s): **Gerald H. Grondin**

Date of Review: **19 December 2022**

Date Reviewed by GW Mgr. and Returned to WRSD: jti 2/16/23

The information provided in the application is insufficient to evaluate whether the proposed transfer may be approved because:

- ☐ The water well reports provided with the application do not correspond to the water rights affected by the transfer.
- ☐ The application does not include water well reports or a description of the well construction details sufficient to establish the ground water body developed or proposed to be developed.
- ☐ Other _____
-

1. Basic description of the changes proposed in this transfer: _____

This transfer application relates to three water right certificates 53450, 53452, and 84982. The explanation statement says the applicant seeks "Transfer of water from the outer edges of 3 existing pivots to fill in the remaining area of an existing partial pivot not currently covered. Also, change the point of appropriation on one of the pivots to an existing well that is located at the center of the pivot, replacing the approved well which is located approximately ½ mile away."

The transfer application proposes moving 18.30 authorized POU acres on the outer edges of three center pivots (two are in T25S/R18E-sections 3 in the SW qtr & SE qtr; the third is in T25S/R18E-sections 7 & 18) moved to a center pivot located in T25S/R18E-section 3 NE qtr.

The transfer application further proposes redistributing groundwater pumping (1.71 cfs, 766.38 gpm) related to 136.60 authorized POU acres from three authorized POA wells (owner wells 2, 7, & 8: LAKE 238, LAKE 223, & LAKE 225, 0.11 cfs, 0.05 cfs, & 1.54 cfs respectively) to one authorized POA well (owner well 8, LAKE 225, 0.17 cfs) and to one proposed POA well (owner well 9, LAKE 51691, 1.54 cfs).

The authorized and proposed POA wells are shown in the attached maps.

2. Will the proposed POA develop the same aquifer (source) as the existing authorized POA?

☒ Yes ☐ No Comments: _____

Essentially yes, the "same aquifer" (source) given the same groundwater system will likely be tapped despite the authorized and proposed POA wells are constructed to varying depths and tap varying geologic units (see attached well logs). Long term groundwater level data indicates groundwater levels at wells in the vicinity of the currently authorized and proposed POA locations have similar elevations, seasonally fluctuate similarly, and show the same long-term trends (see attached hydrograph) despite being completed at varying depths and different geologic units.

Additionally, groundwater in the Fort Rock--Valley-Christmas Valley area (Fort Rock Classified Area) is identified as a single groundwater system. Groundwater is found in both a shallower predominantly basin-fill sediment unit and a deeper predominantly volcanic rocks and sediments unit below. The two units are hydraulically connected. Both units can yield groundwater readily with some exceptions.

Miller (1984 and 1986) describes the groundwater source as the main groundwater reservoir. That reservoir includes groundwater in different geologic units. The reservoir has three characteristics. First, the "natural" groundwater level changes less than 1.5 feet annually, indicating the system is highly modulated. Second, the 1980s potentiometric surface was approximately 4292 feet elevation amsl basin-wide with Silver Lake an exception. Third, the reservoir consists of numerous water producing zones in several formations, all having an essentially common potentiometric level, and all being very transmissive in general.

3. a) Is there more than one source developed under the right (e.g., basalt and alluvium)?
☐ Yes ☒ No _____

Essentially no. Single hydraulically connected groundwater system. See discussion in part 2 above.

- b) If yes, estimate the portion of the right supplied by each of the sources and describe any limitations that will need to be placed on the proposed change (rate, duty, etc.): _____

No estimate made and no limitation recommended. Single groundwater system. See item 2 and 3a above.

4. a) Will this proposed change, at its maximum allowed rate of use, likely result in an increase in interference with **another ground water right**?
☒ Yes ☐ No Comments: _____

The proposed POA well change and pumping redistribution will move the net groundwater pumping change further away from some POA wells (seasonal interference at those wells should decrease, see attached calculation for well LAKE 221) and closer to other POA wells (seasonal interference at those wells should increase, see attached calculation for an unidentified water right well in T25S/R18E-sec 10, NE qtr).

The proposed POA well change and pumping redistribution will move net groundwater pumping change closer to an unidentified groundwater right POA within T25S/R18E-sec 10, NE qtr (see attached). The net increase in seasonal drawdown is calculated to be less than 1.0 feet. That POA well should be able to accommodate the seasonal drawdown change. The net increase in seasonal drawdown at other wells further away should be less.

The long-term impact on the groundwater system should be the same. That impact is to continue contributing to the ongoing annual Fort Rock Classified Area groundwater level decline (see the attached hydrograph...it shows an annual decline rate from 0.30 to 0.50 feet per year).

- b) If yes, would this proposed change, at its maximum allowed rate of use, likely result in another groundwater right not receiving the water to which it is legally entitled?

☐ Yes ☒ No If yes, explain: _____

See discussion in part 4a above.

5. a) Will this proposed change, at its maximum allowed rate of use, likely result in an increase in interference with **another surface water source**?

☒ Yes ☒ No Comments: _____

Yes for Silver Lake and No for Paulina Marsh.

The seasonal groundwater level drawdown at the closest Silver Lake shoreline is calculated to increase less than 0.002 feet. The resultant increase in interference at the lake is calculated to be less than 1200 ft³/day (less than 0.02 cfs, 6.5 gpm). See attached calculation for a full lake.

The seasonal groundwater level drawdown at the closest Paulina Marsh boundary is calculated to decrease. The interference at the marsh should decrease.

The long-term interference at Paulina Marsh and Silver Lake should be the same.

- b) If yes, at its maximum allowed rate of use, what is the expected change in degree of interference with any **surface water sources** resulting from the proposed change?

Stream: Silver Lake ☒ Minimal ☐ Significant

Stream: Paulina Marsh ☒ Minimal ☐ Significant

Provide context for minimal/significant impact: _____

See comment in part 5a above.

6. For SW-GW transfers, will the proposed change in point of diversion affect the surface water source similarly (as per OAR 690-380-2130) to the authorized point of diversion specified in the water use subject to transfer?

☐ Yes ☒ No Comments: _____

Not Applicable. No SW-GW transfer.

7. What conditions or other changes in the application are necessary to address any potential issues identified above: _____

Note: the proposed transfer is within the Fort Rock groundwater limited area.

The following are technical groundwater review recommendations. It is recognized that one or more technically recommended conditions may or may not be allowed under the transfer process rules and statutes. This technical groundwater review relies on other appropriate and authorized Department staff to make that determination.

“Large” flow meter condition for any proposed “To” POA and/or APOA well. Require the flow meter for any POA and/or APOA well to be properly installed and maintained. Each meter shall be either within 50 feet of the well head with a clearly visible monument adjacent to the meter or a surveyed location shall be provided and a clearly visible monument adjacent to the meter shall be installed for each meter more than 50 feet from the well head.

Condition 7P (well tag condition) for all the “To” and “From” POA wells.

Condition 7T (modified) for all “To” POA wells: “Prior to use, all POA wells shall be configured to allow a strictly clean water (no oil) static water level measurements with an electric-tape. That can include measurement access via an unobstructed vertical discharge pipe that allows the groundwater level to fluctuate freely within the discharge pipe (no valves, etc.). Otherwise, a dedicated measuring tube must be installed prior to use. The tube must be unobstructed, have a diameter of ¾ inch (0.75 inch) or greater, and pursuant to figure 200-5 in OAR 690-200.”

8. Any additional comments: _____

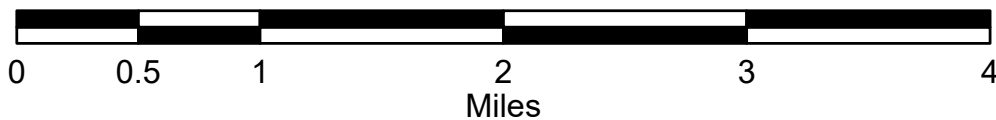
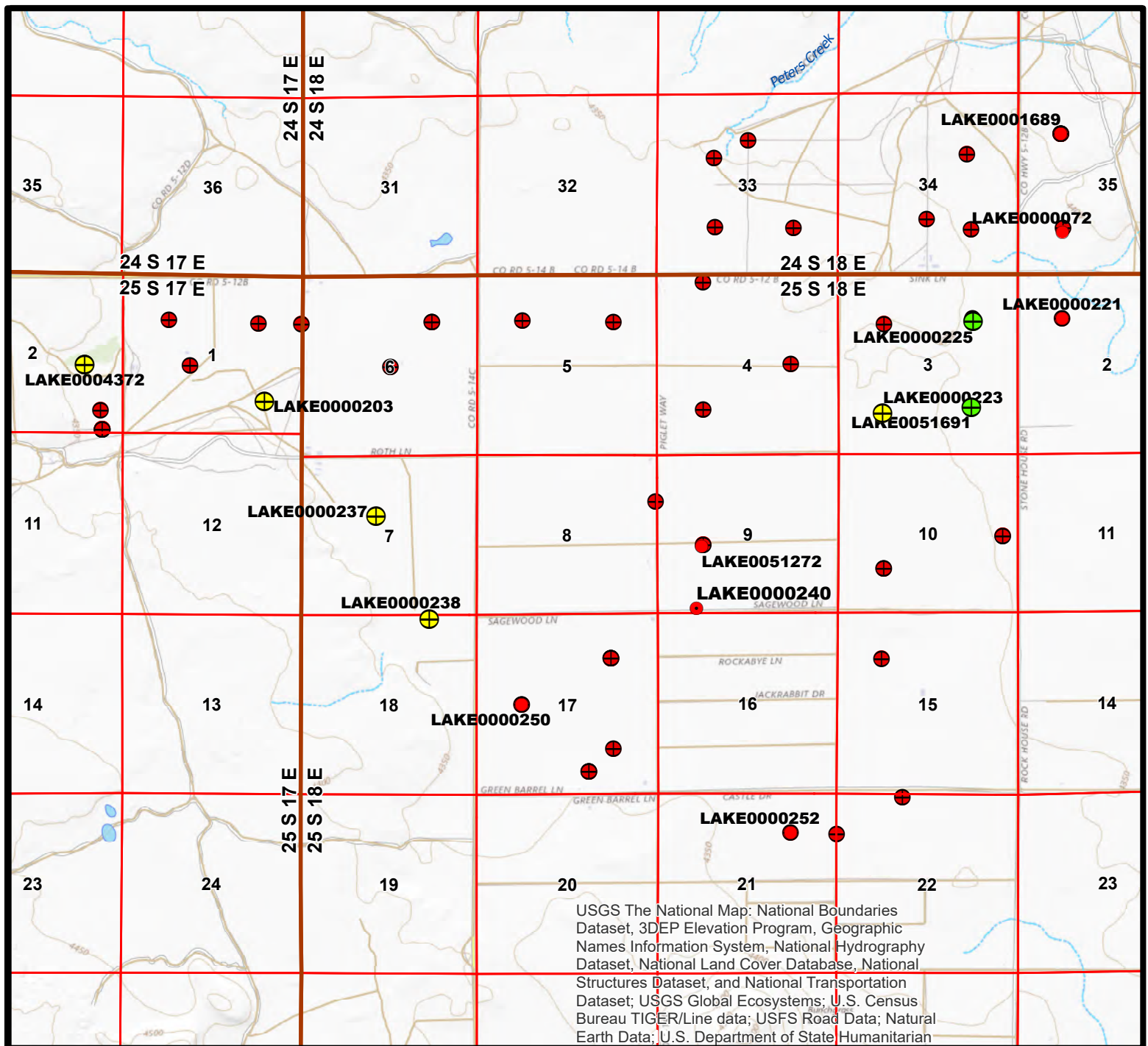
No additional comments.

References:

Miller, D.W., 1986, Appraisal of ground-water conditions in the Fort Rock Basin, Lake County, Oregon: Oregon Water Resources Department, Ground Water Report No. 31, 196 p and plates.

Groundwater Transfer Application T-13973

Daniel Roth

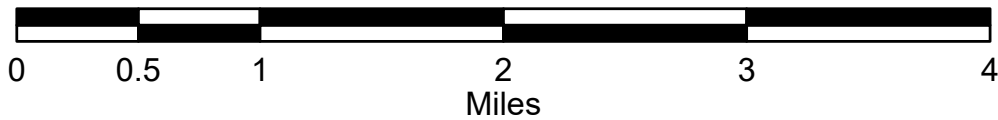
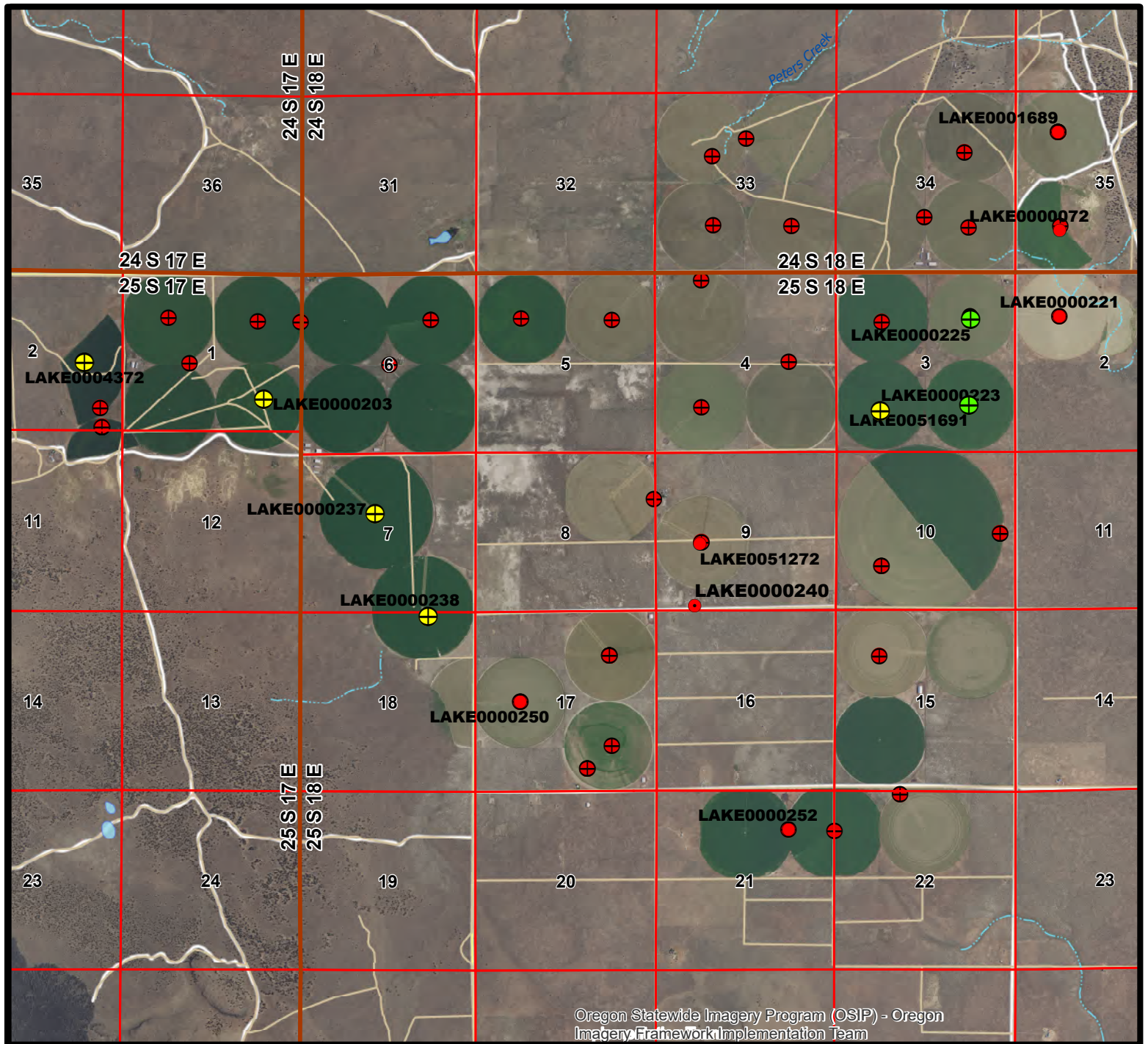


Green = Proposed Well
Yellow = Authorized Wells
Red = Groundwater PODs or Other Wells
Blue = Surface Water PODs



Groundwater Transfer Application T-13973

Daniel Roth



Green = Proposed Well
Yellow = Authorized Wells
Red = Groundwater PODs or Other Wells
Blue = Surface Water PODs



T-13973 (Daniel Roth)
Proposed Change
Christmas Valley (Fort Rock Groundwater Limited Area)

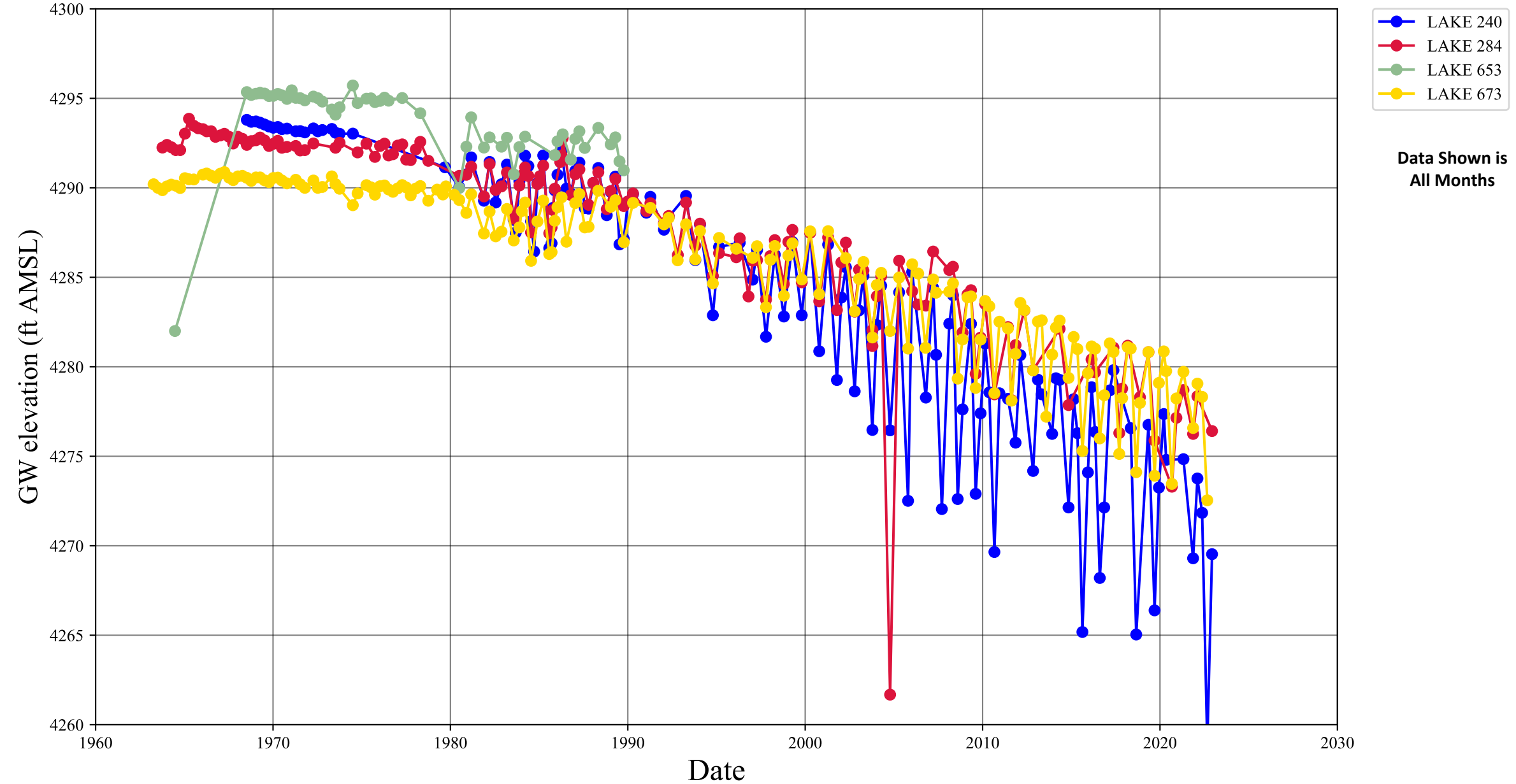
Certificate	From Acres	From CFS	From POD/POA Well		To Acres	To CFS	To POD/POA Well		Change Calculation Comment
			Owner	OWRD			Owner	OWRD	
53450	0.00	0.0000	Well 1	LAKE 203	0.00	0.0000	Well 1	LAKE 203	
	0.00	0.0000	Well 2	LAKE 238	0.00	0.0000	Well 2	LAKE 238	
	0.00	0.0000	Well 3	LAKE 237	0.00	0.0000	Well 3	LAKE 237	
	0.00	0.0000	Well 5	LAKE 4372	0.00	0.0000	Well 5	LAKE 4372	
	4.10	0.0513	Well 7	LAKE 223	0.00	0.0000	Well 7	LAKE 223	
	0.00	0.0000	Well 8	LAKE 225	4.10	0.0513	Well 8	LAKE 225	
	0.00	0.0000	Well 9	LAKE 51691	0.00	0.0000	Well 9	LAKE 51691	
	4.10	0.0513			4.10	0.0513			
53452	0.00	0.0000	Well 1	LAKE 203	0.00	0.0000	Well 1	LAKE 203	
	0.00	0.0000	Well 2	LAKE 238	0.00	0.0000	Well 2	LAKE 238	
	0.00	0.0000	Well 3	LAKE 237	0.00	0.0000	Well 3	LAKE 237	
	0.00	0.0000	Well 5	LAKE 4372	0.00	0.0000	Well 5	LAKE 4372	
	0.00	0.0000	Well 7	LAKE 223	0.00	0.0000	Well 7	LAKE 223	
	123.40	1.5425	Well 8	LAKE 225	0.00	0.0000	Well 8	LAKE 225	Net Decrease
	0.00	0.0000	Well 9	LAKE 51691	123.40	1.5425	Well 9	LAKE 51691	Net Increase
	123.40	1.5425			123.40	1.5425			
84982	0.00	0.0000	Well 1	LAKE 203	0.00	0.0000	Well 1	LAKE 203	No Change
	9.10	0.1138	Well 2	LAKE 238	0.00	0.0000	Well 2	LAKE 238	Net Decrease
	0.00	0.0000	Well 3	LAKE 237	0.00	0.0000	Well 3	LAKE 237	No Change
	0.00	0.0000	Well 5	LAKE 4372	0.00	0.0000	Well 5	LAKE 4372	No Change
	0.00	0.0000	Well 7	LAKE 223	0.00	0.0000	Well 7	LAKE 223	
	0.00	0.0000	Well 8	LAKE 225	9.10	0.1138	Well 8	LAKE 225	Net Increase
	0.00	0.0000	Well 9	LAKE 51691	0.00	0.0000	Well 9	LAKE 51691	
	9.10	0.1138			9.10	0.1138			
Overall Totals	136.60	1.7075			136.60	1.7075			
Totals per Well	0.00	0.0000	Well 1	LAKE 203	0.00	0.0000	Well 1	LAKE 203	No Change
	9.10	0.1138	Well 2	LAKE 238	0.00	0.0000	Well 2	LAKE 238	Net Decrease
	0.00	0.0000	Well 3	LAKE 237	0.00	0.0000	Well 3	LAKE 237	No Change
	0.00	0.0000	Well 5	LAKE 4372	0.00	0.0000	Well 5	LAKE 4372	No Change
	4.10	0.0513	Well 7	LAKE 223	0.00	0.0000	Well 7	LAKE 223	Net Decrease
	123.40	1.5425	Well 8	LAKE 225	13.20	0.1650	Well 8	LAKE 225	Net Decrease
	0.00	0.0000	Well 9	LAKE 51691	123.40	1.5425	Well 9	LAKE 51691	Net Increase
	136.60	1.7075			136.60	1.7075			

Note: CFS in Table = (Total Acres) / (80 Acre/CFS)

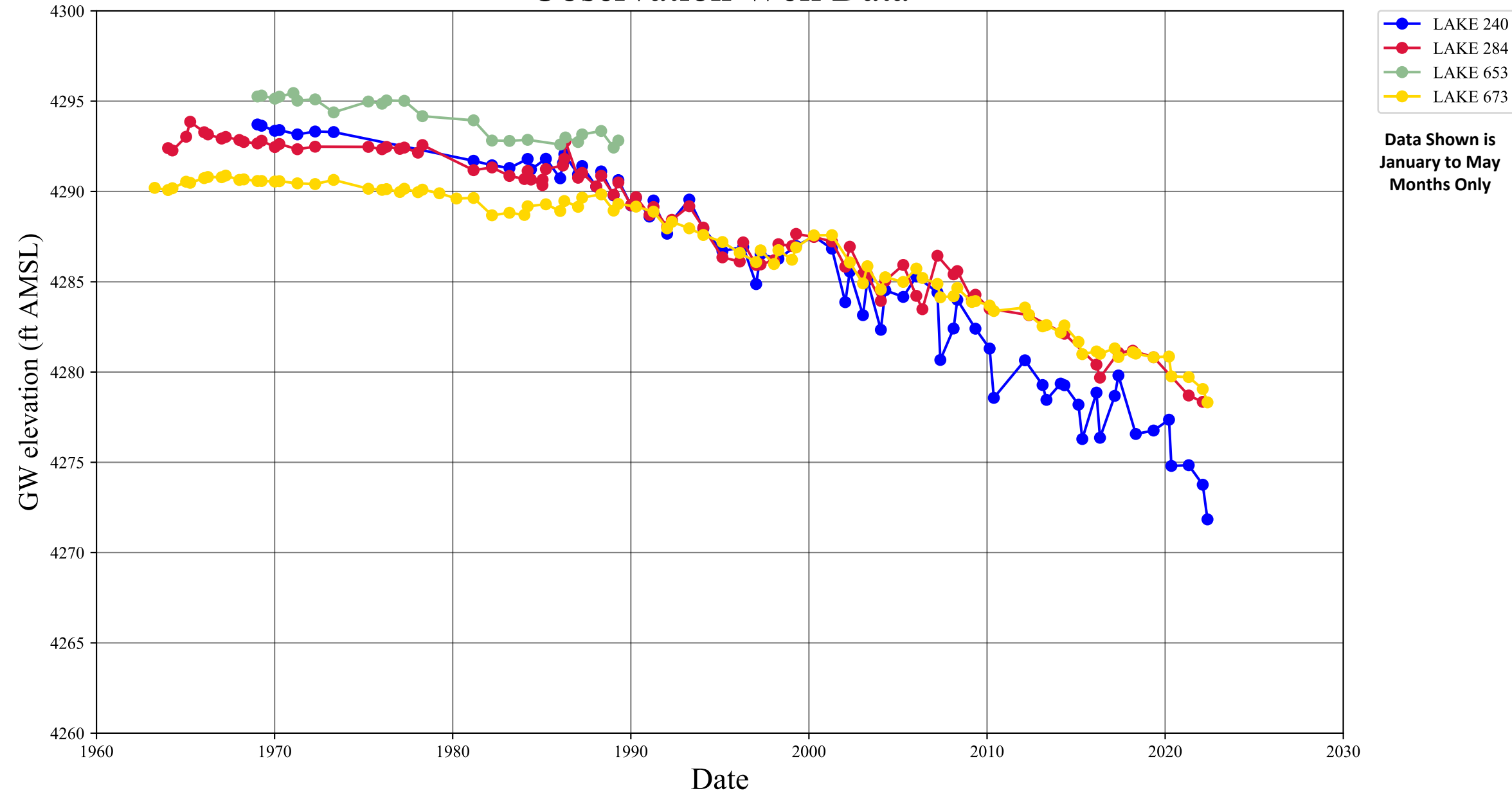
Note: this review identified LAKE 223 (owner well #7) as the original construction for LAKE 224 (deepening) and LAKE 4578 (subsequent deepening)

Note: the yellow highlights the proposed transfer for each certificate as specified in the T-13973 application

Observation Well Data



Observation Well Data



Theis Equation:

$$s = \frac{Q}{4\pi T} \sum_{n=1}^{\infty} \frac{W(u)}{n} \\ u = \frac{r^2 S}{4 T t} \\ W(u) = (-\ln u) - (0.5772157) + (u/1 \cdot 1!) - (u^2/2 \cdot 2!) + (u^3/3 \cdot 3!) - (u^4/4 \cdot 4!) + \dots$$

s = drawdown (L) r =
 T = transmissivity (L²/T) t =
 S = storage coefficient (dimensionless) u =
 π = 3.141592654 $W(u)$

Transmissivity T (gpd/ft)	Transmissivity T (ft ² /day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft ³ /sec)	Time t (days)	Distance r (feet)	pi	u	W(u) W(u)	Drawdown s (feet)	Drawdown Change s (feet)	Well	Comments
Note : W(u) calculation valid when u < 7.1													
Note: yellow grid areas are where values are calculated								7.0000	1.1545E-04				W(u) calculation test
"From" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	23,645.00	3.14	0.3106	0.8801	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	51.05	0.11	30.00	20,665.00	3.14	0.2372	1.0853	0.0566		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	21,055.00	3.14	0.2463	1.0560	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	28,555.00	3.14	0.4530	0.6211	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	23.00	0.05	30.00	5,995.00	3.14	0.0200	3.3563	0.0788		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	30.00	2,630.00	3.14	0.0038	4.9882	3.5268		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	3,750.00	3.14	0.0078	4.2826	0.0000		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						3.6622			
"To" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	23,645.00	3.14	0.3106	0.8801	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	20,665.00	3.14	0.2372	1.0853	0.0000		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	21,055.00	3.14	0.2463	1.0560	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	28,555.00	3.14	0.4530	0.6211	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	5,995.00	3.14	0.0200	3.3563	0.0000		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	74.06	0.16	30.00	2,630.00	3.14	0.0038	4.9882	0.3773		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	30.00	3,750.00	3.14	0.0078	4.2826	3.0279		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						3.4052	-0.2570		
"From" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	23,645.00	3.14	0.3106	0.8801	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	25.21	0.06	30.00	20,665.00	3.14	0.2372	1.0853	0.0279		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	21,055.00	3.14	0.2463	1.0560	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	28,555.00	3.14	0.4530	0.6211	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	11.36	0.03	30.00	5,995.00	3.14	0.0200	3.3563	0.0389		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	30.00	2,630.00	3.14	0.0038	4.9882	1.7418		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	3,750.00	3.14	0.0078	4.2826	0.0000		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						1.8087			
"To" POA wells													

Drawdown Calculations Using Theis Equation
Drawdown at Well LAKE 221 (T25S/R18E-sec 02, NE qtr)

Theis Equation: $s = [Q/(4\pi T \pi)] [W(u)]$
 $u = (r^2 S)/(4 T t)$
 $W(u) = (-\ln u) - (0.5772157) + (u/1!) - (u^2/2 \cdot 2!) + (u^3/3 \cdot 3!) - (u^4/4 \cdot 4!) + \dots$

s = drawdown (L)
 T = transmissivity (L²/T)
 S = storage coefficient (dimensionless)
 π = 3.141592654

r = radial distance (L)
 t = time (T)
 u = dimensionless
 $W(u)$ = well function

Transmissivity T (gpd/ft)	Transmissivity T (ft ² /day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft ³ /sec)	Time t (days)	Distance r (feet)	pi	u	W(u)	Drawdown s (feet)	Drawdown Change s (feet)	Well	Comments
Note : W(u) calculation valid when u < 7.1													
Note: yellow grid areas are where values are calculated								7.0000	1.1545E-04				W(u) calculation test
"From" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	23,645.00	3.14	0.0380	2.7298	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	51.05	0.11	245.00	20,665.00	3.14	0.0291	2.9903	0.1559		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	21,055.00	3.14	0.0302	2.9540	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	28,555.00	3.14	0.0555	2.3694	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	23.00	0.05	245.00	5,995.00	3.14	0.0024	5.4390	0.1278		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	2,630.00	3.14	0.0005	7.0849	5.0092		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	3,750.00	3.14	0.0010	6.3758	0.0000		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						5.2929			
"To" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	23,645.00	3.14	0.0380	2.7298	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	20,665.00	3.14	0.0291	2.9903	0.0000		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	21,055.00	3.14	0.0302	2.9540	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	28,555.00	3.14	0.0555	2.3694	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	5,995.00	3.14	0.0024	5.4390	0.0000		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	74.06	0.16	245.00	2,630.00	3.14	0.0005	7.0849	0.5358		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	3,750.00	3.14	0.0010	6.3758	4.5079		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						5.0437	-0.2492		
"From" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	23,645.00	3.14	0.0380	2.7298	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	25.21	0.06	245.00	20,665.00	3.14	0.0291	2.9903	0.0770		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	21,055.00	3.14	0.0302	2.9540	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	28,555.00	3.14	0.0555	2.3694	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	11.36	0.03	245.00	5,995.00	3.14	0.0024	5.4390	0.0631		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	2,630.00	3.14	0.0005	7.0849	2.4739		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	3,750.00	3.14	0.0010	6.3758	0.0000		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						2.6141			
"To" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	23,645.00	3.14	0.0380	2.7298	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	20,665.00	3.14	0.0291	2.9903	0.0000		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	21,055.00	3.14	0.0302	2.9540	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	28,555.00	3.14	0.0555	2.3694	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	5,995.00	3.14	0.0024	5.4390	0.0000		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	36.58	0.08	245.00	2,630.00	3.14	0.0005	7.0849	0.2646		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	3,750.00	3.14	0.0010	6.3758	2.2264		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						2.4910	-0.1231		

Drawdown at unidentified Well in T25S/R18E-sec 10, NE qtr

s = drawdown (L)	r = radial distance (L)
T = transmissivity (L^2/T)	t = time (T)
S = storage coefficient (dimensionless)	u = dimensionless
pi = 3.141592654	W(u) = well function

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Drawdown Calculations Using Theis Equation

Drawdown at unidentified Well in T25S/R18E-sec 10, NE qtr

Theis Equation: $s = [Q/(4 \cdot T \cdot \pi)] [W(u)]$

$u = (r^2 \cdot S)/(4 \cdot T \cdot t)$

$W(u) = (-\ln u) - (0.5772157) + (u/1 \cdot 1!) - (u^2/2 \cdot 2!) + (u^3/3 \cdot 3!) - (u^4/4 \cdot 4!) + \dots$

s = drawdown (L)

T = transmissivity (L²/T)

S = storage coefficient (dimensionless)

pi = 3.141592654

r = radial distance (L)

t = time (T)

u = dimensionless

W(u) = well function

Transmissivity T (gpd/ft)	Transmissivity T (ft ² /day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft ³ /sec)	Time t (days)	Distance r (feet)	pi	u	W(u)	Drawdown s (feet)	Drawdown Change s (feet)	Well	Comments
									Note : W(u) calculation valid when u < 7.1				
								7.0000	1.1545E-04				W(u) calculation test
"From" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	22,130.00	3.14	0.0333	2.8576	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	51.05	0.11	245.00	17,090.00	3.14	0.0199	3.3612	0.1752		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	18,490.00	3.14	0.0233	3.2070	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	27,540.00	3.14	0.0516	2.4380	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	23.00	0.05	245.00	5,060.00	3.14	0.0017	5.7774	0.1357		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	6,380.00	3.14	0.0028	5.3148	3.7577		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	3,900.00	3.14	0.0010	6.2975	0.0000		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						4.0687			
"To" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	22,130.00	3.14	0.0333	2.8576	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	17,090.00	3.14	0.0199	3.3612	0.0000		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	18,490.00	3.14	0.0233	3.2070	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	27,540.00	3.14	0.0516	2.4380	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	5,060.00	3.14	0.0017	5.7774	0.0000		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	74.06	0.16	245.00	6,380.00	3.14	0.0028	5.3148	0.4020		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	3,900.00	3.14	0.0010	6.2975	4.4525		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						4.8545	0.7858		
"From" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	22,130.00	3.14	0.0333	2.8576	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	25.21	0.06	245.00	17,090.00	3.14	0.0199	3.3612	0.0866		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	18,490.00	3.14	0.0233	3.2070	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	27,540.00	3.14	0.0516	2.4380	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	11.36	0.03	245.00	5,060.00	3.14	0.0017	5.7774	0.0670		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	6,380.00	3.14	0.0028	5.3148	1.8559		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	3,900.00	3.14	0.0010	6.2975	0.0000		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						2.0094			
"To" POA wells to Water Right Well closest to Proposed "To" Well (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	22,130.00	3.14	0.0333	2.8576	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	17,090.00	3.14	0.0199	3.3612	0.0000		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	18,490.00	3.14	0.0233	3.2070	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	27,540.00	3.14	0.0516	2.4380	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	5,060.00	3.14	0.0017	5.7774	0.0000		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	36.58	0.08	245.00	6,380.00	3.14	0.0028	5.3148	0.1985		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	3,900.00	3.14	0.0010	6.2975	2.1990		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						2.3975	0.3881		

Theis Equation: $s = [Q/(4 \cdot T \cdot \pi)] [W(u)]$
 $u = (r^2 r^2 S)/(4 \cdot T \cdot t)$
 $W(u) = (-\ln u) - (0.5772157) + (u/1 \cdot 1!) - (u^2/2 \cdot 2!) + (u^3/3 \cdot 3!) - (u^4/4 \cdot 4!) + \dots$

s = drawdown (L) r =
 T = transmissivity (L²/L/T) t =
 S = storage coefficient (dimensionless) u =
 π = 3.141592654 $W(u)$

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Drawdown Calculations Using Theis Equation

Theis Equation: $s = [Q/(4 \cdot T \cdot \pi)] [W(u)]$
 $u = (r^2 \cdot S)/(4 \cdot T \cdot t)$
 $W(u) = (-\ln u) - (0.5772157) + (u/1 \cdot 1!) - (u^2/2 \cdot 2!) + (u^3/3 \cdot 3!) - (u^4/4 \cdot 4!) + \dots$

 s = drawdown (L) r = radial distance (L)
 T = transmissivity (L²/T) t = time (T)
 S = storage coefficient (dimensionless) u = dimensionless
 π = 3.141592654 $W(u)$ = well function

Transmissivity T (gpd/ft)	Transmissivity T (ft ² /day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft ³ /sec)	Time t (days)	Distance r (feet)	pi	u	W(u)	Drawdown s (feet)	Drawdown Change s (feet)	Well	Comments
								Note : W(u) calculation valid when u < 7.1					
								7.0000	1.1545E-04				W(u) calculation test
"From" POA wells to Silver Lake (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	131,705.00	3.14	1.1800	0.1635	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	51.05	0.11	245.00	128,665.00	3.14	1.1262	0.1783	0.0093		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,430.00	3.14	1.1573	0.1696	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,170.00	3.14	1.1527	0.1708	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	23.00	0.05	245.00	141,185.00	3.14	1.3560	0.1243	0.0029		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	145,010.00	3.14	1.4305	0.1110	0.0785		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	142,870.00	3.14	1.3886	0.1183	0.0000		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						0.0907			
"To" POA wells to Silver Lake (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	131,705.00	3.14	1.1800	0.1635	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	128,665.00	3.14	1.1262	0.1783	0.0000		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,430.00	3.14	1.1573	0.1696	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,170.00	3.14	1.1527	0.1708	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	141,185.00	3.14	1.3560	0.1243	0.0000		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	74.06	0.16	245.00	145,010.00	3.14	1.4305	0.1110	0.0084		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	142,870.00	3.14	1.3886	0.1183	0.0836		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						0.0920	0.0013		
"From" POA wells to Silver Lake (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	131,705.00	3.14	1.1800	0.1635	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	25.21	0.06	245.00	128,665.00	3.14	1.1262	0.1783	0.0046		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,430.00	3.14	1.1573	0.1696	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,170.00	3.14	1.1527	0.1708	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	11.36	0.03	245.00	141,185.00	3.14	1.3560	0.1243	0.0014		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	145,010.00	3.14	1.4305	0.1110	0.0388		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	142,870.00	3.14	1.3886	0.1183	0.0000		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						0.0448			
"To" POA wells to Silver Lake (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	131,705.00	3.14	1.1800	0.1635	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	128,665.00	3.14	1.1262	0.1783	0.0000		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,430.00	3.14	1.1573	0.1696	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	130,170.00	3.14	1.1527	0.1708	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	141,185.00	3.14	1.3560	0.1243	0.0000		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	36.58	0.08	245.00	145,010.00	3.14	1.4305	0.1110	0.0041		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	142,870.00	3.14	1.3886	0.1183	0.0413		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						0.0454	0.0007		

Drawdown Calculations Using Theis Equation

Theis Equation: $s = [Q/(4 \cdot T \cdot \pi)] [W(u)]$
 $u = (r^2 \cdot S)/(4 \cdot T \cdot t)$
 $W(u) = (-\ln u) - (0.5772157) + (u/1 \cdot 1!) - (u^2/2 \cdot 2!) + (u^3/3 \cdot 3!) - (u^4/4 \cdot 4!) + \dots$

 s = drawdown (L) r = radial distance (L)
 T = transmissivity (L²/T) t = time (T)
 S = storage coefficient (dimensionless) u = dimensionless
 π = 3.141592654 $W(u)$ = well function

Transmissivity T (gpd/ft)	Transmissivity T (ft ² /day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft ³ /sec)	Time t (days)	Distance r (feet)	pi	u	W(u)	Drawdown s (feet)	Drawdown Change s (feet)	Well	Comments
								Note : W(u) calculation valid when u < 7.1					
								7.0000	1.1545E-04				W(u) calculation test
"From" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	127,555.00	3.14	9.0390	-0.0799	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	51.05	0.11	30.00	127,510.00	3.14	9.0327	-0.0788	-0.0041		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	128,050.00	3.14	9.1093	-0.0939	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	124,200.00	3.14	8.5698	-0.0265	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	23.00	0.05	30.00	141,935.00	3.14	11.1920	-6.6460	-0.1561		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	30.00	145,710.00	3.14	11.7952	-19.6616	-13.9014		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	144,200.00	3.14	11.5520	-12.7853	0.0000		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						-14.0616			Calculation not valid, U > 7.1
"To" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	127,555.00	3.14	9.0390	-0.0799	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	127,510.00	3.14	9.0327	-0.0788	0.0000		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	128,050.00	3.14	9.1093	-0.0939	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	124,200.00	3.14	8.5698	-0.0265	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	141,935.00	3.14	11.1920	-6.6460	0.0000		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	74.06	0.16	30.00	145,710.00	3.14	11.7952	-19.6616	-1.4870		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	30.00	144,200.00	3.14	11.5520	-12.7853	-9.0396		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						-10.5266	3.5350		Calculation not valid, U > 7.1
"From" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	127,555.00	3.14	9.0390	-0.0799	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	25.21	0.06	30.00	127,510.00	3.14	9.0327	-0.0788	-0.0020		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	128,050.00	3.14	9.1093	-0.0939	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	124,200.00	3.14	8.5698	-0.0265	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	11.36	0.03	30.00	141,935.00	3.14	11.1920	-6.6460	-0.0771		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	30.00	145,710.00	3.14	11.7952	-19.6616	-6.8656		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	144,200.00	3.14	11.5520	-12.7853	0.0000		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						-6.9447			Calculation not valid, U > 7.1
"To" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	127,555.00	3.14	9.0390	-0.0799	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	127,510.00	3.14	9.0327	-0.0788	0.0000		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	128,050.00	3.14	9.1093	-0.0939	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	124,200.00	3.14	8.5698	-0.0265	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	30.00	141,935.00	3.14	11.1920	-6.6460	0.0000		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	36.58	0.08	30.00	145,710.00	3.14	11.7952	-19.6616	-0.7344		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	30.00	144,200.00	3.14	11.5520	-12.7853	-4.4644		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						-5.1988	1.7459		Calculation not valid, U > 7.1

Drawdown Calculations Using Theis Equation

Theis Equation: $s = [Q/(4 \cdot T \cdot \pi)] [W(u)]$
 $u = (r^2 \cdot S)/(4 \cdot T \cdot t)$
 $W(u) = (-\ln u) - (0.5772157) + (u/1 \cdot 1!) - (u^2/2 \cdot 2!) + (u^3/3 \cdot 3!) - (u^4/4 \cdot 4!) + \dots$

 s = drawdown (L) r = radial distance (L)
 T = transmissivity (L²/T) t = time (T)
 S = storage coefficient (dimensionless) u = dimensionless
 π = 3.141592654 $W(u)$ = well function

Transmissivity T (gpd/ft)	Transmissivity T (ft ² /day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft ³ /sec)	Time t (days)	Distance r (feet)	pi	u	W(u)	Drawdown s (feet)	Drawdown Change s (feet)	Well	Comments
								Note : W(u) calculation valid when u < 7.1					
								7.0000	1.1545E-04				W(u) calculation test
Note: yellow grid areas are where values are calculated													
"From" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	127,555.00	3.14	1.1068	0.1839	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	51.05	0.11	245.00	127,510.00	3.14	1.1060	0.1842	0.0096		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	128,050.00	3.14	1.1154	0.1814	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	124,200.00	3.14	1.0494	0.2021	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	23.00	0.05	245.00	141,935.00	3.14	1.3704	0.1216	0.0029		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	145,710.00	3.14	1.4443	0.1087	0.0769		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	144,200.00	3.14	1.4145	0.1137	0.0000		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						0.0893			
"To" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	127,555.00	3.14	1.1068	0.1839	0.0000		LAKE 203	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	127,510.00	3.14	1.1060	0.1842	0.0000		LAKE 238	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	128,050.00	3.14	1.1154	0.1814	0.0000		LAKE 237	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	124,200.00	3.14	1.0494	0.2021	0.0000		LAKE 4372	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	141,935.00	3.14	1.3704	0.1216	0.0000		LAKE 223	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	74.06	0.16	245.00	145,710.00	3.14	1.4443	0.1087	0.0082		LAKE 225	Continuous Pumping at Full Rate
112,207.80	15,000.00	0.00100	692.32	1.54	245.00	144,200.00	3.14	1.4145	0.1137	0.0804		LAKE 51691	Continuous Pumping at Full Rate
			766.38	1.71						0.0886	-0.0007		
"From" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	127,555.00	3.14	1.1068	0.1839	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	25.21	0.06	245.00	127,510.00	3.14	1.1060	0.1842	0.0047		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	128,050.00	3.14	1.1154	0.1814	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	124,200.00	3.14	1.0494	0.2021	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	11.36	0.03	245.00	141,935.00	3.14	1.3704	0.1216	0.0014		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	145,710.00	3.14	1.4443	0.1087	0.0380		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	144,200.00	3.14	1.4145	0.1137	0.0000		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						0.0441			
"To" POA wells to Paulina Marsh (Transmissivity from Morgan (1988) and McFarland and Ryals (1991)): Used S = 0.001													
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	127,555.00	3.14	1.1068	0.1839	0.0000		LAKE 203	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	127,510.00	3.14	1.1060	0.1842	0.0000		LAKE 238	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	128,050.00	3.14	1.1154	0.1814	0.0000		LAKE 237	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	124,200.00	3.14	1.0494	0.2021	0.0000		LAKE 4372	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	0.00	0.00	245.00	141,935.00	3.14	1.3704	0.1216	0.0000		LAKE 223	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	36.58	0.08	245.00	145,710.00	3.14	1.4443	0.1087	0.0041		LAKE 225	Continuous Pro-Rated Pumping
112,207.80	15,000.00	0.00100	341.92	0.76	245.00	144,200.00	3.14	1.4145	0.1137	0.0397		LAKE 51691	Continuous Pro-Rated Pumping
			378.50	0.84						0.0438	-0.0004		

Vertical GW Flow Using Darcy Equation

Darcy Equation: $Q = K A [(h_1 - h_2) / (L_1 - L_2)]$

Q = volumetric GW flow
K = hydraulic conductivity
A = area

$h_1 - h_2$ = change in head at lake edge (head at lake vs. head of "main GW reservoir" potentiometric surface below lake)
 $L_1 - L_2$ = distance for change in head (distance from lake bed to "main GW reservoir" deposits below)
 $[(h_1 - h_2) / (L_1 - L_2)]$ = hydraulic gradient

Vertical GW Flow		Vertical GW Flow Change		Flow Change	Flow Change	Hydraulic Conductivity	Lake Area		Change in Head	Head Change Distance	Comments
Q	Q	Q	Q	Percent	Increase	$K_v = K_{xy} / 100$	A	A	$h_1 - h_2$	$L_1 - L_2$	
(ft ³ /day)	(acre-ft/day)	(ft ³ /day)	(acre-ft/day)	%		(ft/day)	(ft ²)	(acre)	(feet)	(feet)	
Vertical GW flow from full Silver Lake bed through lower permeability deposits to the higher permeability "main GW reservoir"											
27,188,431	624.16	---	---			0.30	455,265,086	10,451.45	30.00	150.00	Full lake, pre-transfer, well = off
27,270,631	626.05	82,200	1.89	0.30%		0.30	455,265,086	10,451.45	30.09	150.00	Full lake, pre-transfer, well = on 245 day full rate
27,229,032	625.09	40,601	0.93	0.15%		0.30	455,265,086	10,451.45	30.04	150.00	Full lake, pre-transfer, well = on 245 day pro-rated
Vertical GW flow from full Silver Lake bed through lower permeability deposits to the higher permeability "main GW reservoir"											
27,188,431	624.16	---	---			0.30	455,265,086	10,451.45	30.00	150.00	Full lake, post-transfer, well = off
27,271,809	626.07	83,378	1.91	0.31%	1.01	0.30	455,265,086	10,451.45	30.09	150.00	Full lake, post-transfer, well = on 245 day full rate
27,229,576	625.11	41,145	0.94	0.15%	1.01	0.30	455,265,086	10,451.45	30.05	150.00	Full lake, post-transfer, well = on 245 day pro-rated
Post-transfer rate minus pre-transfer rate											
1,178	0.03	1,178	0.03								Full lake, well = on 245 day full rate
544	0.01	544	0.01								Full lake, well = on 245 day pro-rated

NOTICE TO WATER WELL CONTRACTOR
The original and first copy of this report
are to be filed with the

WATER RESOURCES DEPARTMENT
SALEM, OREGON 97310
within 30 days from the date
of well completion.

WATER WELL REPORT

STATE OF OREGON

(Please type or print)

(Do not write above this line)

APR 18 1978

State Well No. 255/18E-3

State Permit No.

(1) OWNER:

Name G. B. Crawford
Address 1/2 Crawford Oil Co
Monroe Ore

(2) TYPE OF WORK (check):

New Well ☒ Deepening ☐ Reconditioning ☐ Abandon ☐

If abandonment, describe material and procedure in Item 12.

(3) TYPE OF WELL:

Rotary ☒ Driven ☐
Cable ☐ Jetted ☐
Dug ☐ Bored ☐

(4) PROPOSED USE (check):

Domestic ☒ Industrial ☐ Municipal ☐
Irrigation ☐ Test Well ☒ Other ☐

CASING INSTALLED:

Threaded ☐ Welded ☒
" Diam. from 0 ft. to 19 ft. Gage 250
" Diam. from ft. to ft. Gage
" Diam. from ft. to ft. Gage

PERFORATIONS:

Perforated? ☐ Yes ☒ No.

Type of perforator used

Size of perforations in. by in.
perforations from ft. to ft.
perforations from ft. to ft.
perforations from ft. to ft.

(7) SCREENS:

Well screen installed? ☐ Yes ☒ No

Manufacturer's Name

Type Model No.

Diam. Slot size Set from ft. to ft.

Diam. Slot size Set from ft. to ft.

(8) WELL TESTS:

Drawdown is amount water level is lowered below static level

Was a pump test made? ☐ Yes ☒ No If yes, by whom?

Yield: gal./min. with ft. drawdown after hrs.

" " "

"Tested w/air 1000 gpm"

Ball test gal./min. with ft. drawdown after 4 hrs.

Artesian flow g.p.m.

Temperature of water Depth artesian flow encountered ft.

(9) CONSTRUCTION:

Well seal—Material used Cement

Well sealed from land surface to ft.

Diameter of well bore to bottom of seal 17 1/2 in.

Diameter of well bore below seal 12 in.

Number of sacks of cement used in well seal 6 sacks

How was cement grout placed? poured

Was a drive shoe used? ☐ Yes ☒ No Plugs Size: location ft.

Did any strata contain unusable water? ☐ Yes ☒ No

Type of water? depth of strata

Method of sealing strata off

Was well gravel packed? ☐ Yes ☒ No Size of gravel: ft.

Gravel placed from ft. to ft.

(10) LOCATION OF WELL:

County Lake Driller's well number

1/4 1/4 Section 3 T. 25S R. 18E W.M.

Bearing and distance from section or subdivision corner

(11) WATER LEVEL: Completed well.

Depth at which water was first found 95 ft.

Static level 50 ft. below land surface. Date 2/23/78

Artesian pressure lbs. per square inch. Date

(12) WELL LOG:

Diameter of well below casing 12"

Depth drilled 285 ft. Depth of completed well 285 ft.

Formation: Describe color, texture, grain size and structure of materials; and show thickness and nature of each stratum and aquifer penetrated, with at least one entry for each change of formation. Report each change in position of Static Water Level and indicate principal water-bearing strata.

MATERIAL	From	To	SWL
Brown loam	0	2	
Blue volcanic rock	2	67	
Red volcanic rock	67	82	
Red cinders B. volcanic rock	82	135	
Red cinders	135	140	
Blue basalt	140	200	
Black volcanic rock	200	210	
Blue basalt	210	240	
Blue sand rock	240	275	
Blue basalt	275	285	

Work started 2/21/78 19 Completed 3/23 1978

Date well drilling machine moved off of well 3/23 1978

Drilling Machine Operator's Certification:

This well was constructed under my direct supervision. Materials used and information reported above are true to my best knowledge and belief.

[Signed] Robert Lester Date 3/10 1978
(Drilling Machine Operator)

Drilling Machine Operator's License No. 948

Water Well Contractor's Certification:

This well was drilled under my jurisdiction and this report is true to the best of my knowledge and belief.

Name But Jones
(Person, firm or corporation) (Type or print)

Address 29404 S. Linn Hwy Lebanon Ore

[Signed] But Jones
(Water Well Contractor)

Contractor's License No. 514 Date 3/10/78 19

The original and first copy of this report
are to be filed with the

WATER RESOURCES DEPARTMENT

SALEM, OREGON 97310

within 30 days from the date
of well completion.

RECEIVED

AUG 18 1980

WATER WELL REPORT

STATE OF OREGON

(Please type or print)

State Well No.

State Permit No.

WATER RESOURCES DEPT

write above this line

(1) OWNER:

SALEM, OREGON

Name Gilbert Crowson
Address Box 402 Christmas Valley, OR.

(2) TYPE OF WORK (check):

New Well ☒ Deepening ☐ Reconditioning ☐ Abandon ☐

If abandonment, describe material and procedure in Item 12.

(3) TYPE OF WELL:

Rotary ☒ Driven ☐
Cable ☐ Jetted ☐
☐ Bored ☐

(4) PROPOSED USE (check):

Domestic ☐ Industrial ☐ Municipal ☐
Irrigation ☒ Test Well ☐ Other ☐

(5) CASING INSTALLED:

14 " Diam. from 14 ft. to 20 ft. Gage 250
" Diam. from _____ ft. to _____ ft. Gage _____
" Diam. from _____ ft. to _____ ft. Gage _____

(6) PERFORATIONS:

Perforated? ☐ Yes ☒ No.

Type of perforator used _____

Size of perforations _____ in. by _____ in.
_____ perforations from _____ ft. to _____ ft.
_____ perforations from _____ ft. to _____ ft.
_____ perforations from _____ ft. to _____ ft.

(7) SCREENS:

Well screen installed? ☐ Yes ☒ No

Manufacturer's Name _____

Type _____ Model No. _____
Diam. _____ Slot size _____ Set from _____ ft. to _____ ft.
Diam. _____ Slot size _____ Set from _____ ft. to _____ ft.

(8) WELL TESTS:

Drawdown is amount water level is
lowered below static level

Is a pump test made? ☐ Yes ☒ No If yes, by whom?

Yield: _____ gal./min. with _____ ft. drawdown after _____ hrs.
" 150 lbs. Air " " "
" " " "

Boiler test 1000 gal./min. with _____ ft. drawdown after _____ hrs.

Artesian flow _____ g.p.m.

Temperature of water _____ Depth artesian flow encountered _____ ft.

(9) CONSTRUCTION:

Well seal—Material used Cement

Well sealed from land surface to _____ ft.

Diameter of well bore to bottom of seal 18 in.

Diameter of well bore below seal 8 in.

Number of sacks of cement used in well seal _____ sacks

How was cement grout placed? Cement was

mixed w. 1" pipe run down

along side & pressure grouted

in _____ in.

Was a drive shoe used? ☐ Yes ☒ No Plugs _____ Size: location _____ ft.

Did any strata contain unusable water? ☐ Yes ☒ No

Type of water? _____ depth of strata _____

Method of sealing strata off _____

Was well gravel packed? ☐ Yes ☒ No Size of gravel: _____

Gravel placed from _____ ft. to _____ ft.

(10) LOCATION OF WELL:

County Lake Driller's well number _____
_____ 1/4 Section 3 T. 25 R. 18 E. W.M.

Bearing and distance from section or subdivision corner _____

(11) WATER LEVEL: Completed well.

Depth at which water was first found 71 ft.

Static level 57 ft. below land surface. Date 5/7/80

Artesian pressure _____ lbs. per square inch. Date _____

(12) WELL LOG:

Diameter of well below casing 8 1/2

Depth drilled 370 ft. Depth of completed well 370 ft.

Formation: Describe color, texture, grain size and structure of materials;
and show thickness and nature of each stratum and aquifer penetrated,
with at least one entry for each change of formation. Report each change in
position of Static Water Level and indicate principal water-bearing strata.

MATERIAL	From	To	SWL
Brown Clay	0	4	
Black lava rock	4	67	
Red Cinders	67	74	
Brown Cinders	74	81	
Black lava Rock	81	121	
Amice Water Bearing	121	124	
Black lava Rock	124	136	
Brown Cinders	136	141	
Red lava Rock	141	153	
Black lava Rock	153	185	
Red lava Rock	185	197	
Black lava Rock	197	246	
Black sand	246	248	
Black lava Rock	248	320	
Black sand	320	350	
Gray Stone	350	370	

Work started 4/13 19 80 Completed 5/7 19 80

Date well drilling machine moved off of well 5/7 19 80

Drilling Machine Operator's Certification:

This well was constructed under my direct supervision.
Materials used and information reported above are true to my
best knowledge and belief.

[Signed] Mel Search Date 5/10, 19 80
(Drilling Machine Operator)

Drilling Machine Operator's License No. 699

Water Well Contractor's Certification:

This well was drilled under my jurisdiction and this report is
true to the best of my knowledge and belief.

Name Mel Search Well Drilling
(Person, firm or corporation) (Type or print)

Address 432 Lebanon, OR.

[Signed] Mel Search
(Water Well Contractor)

Contractor's License No. 567 Date 5/10, 19 80

STATE OF OREGON WATER SUPPLY WELL REPORT

(as required by ORS 537.765)

Instructions for completing this report are on the last page of this form.

WELL I.D. # L 47604
START CARD # 162617

LAKE 51503

(1) LAND OWNER
Name Conley 1st North Well Number _____
Address 10 Mon St
City Christmas Valley State OR Zip 97641

(2) TYPE OF WORK
☐ New Well ☒ Deepening ☐ Alteration (repair/recondition) ☐ Abandonment

(3) DRILL METHOD:
☒ Rotary Air ☐ Rotary Mud ☐ Cable ☐ Auger
☐ Other _____

(4) PROPOSED USE:
☐ Domestic ☐ Community ☐ Industrial ☒ Irrigation
☐ Thermal ☐ Injection ☐ Livestock ☐ Other _____

(5) BORE HOLE CONSTRUCTION:
Special Construction approval ☐ Yes ☒ No Depth of Completed Well 20' ft.
Explosives used ☐ Yes ☒ No Type _____ Amount _____

HOLE			SEAL			
Diameter	From	To	Material	From	To	Sacks or pounds
12"	140	200				

How was seal placed: Method ☐ A ☐ B ☐ C ☐ D ☐ E
☐ Other _____

Backfill placed from _____ ft. to _____ ft. Material _____
Gravel placed from _____ ft. to _____ ft. Size of gravel _____

(6) CASING/LINER:

Diameter	From	To	Gauge	Steel	Plastic	Welded	Threaded
Casing:				☐	☐	☐	☐
				☐	☐	☐	☐
				☐	☐	☐	☐
Liner:				☐	☐	☐	☐
				☐	☐	☐	☐

Drive Shoe used ☐ Inside ☐ Outside ☐ None
Final location of shoe(s) _____

(7) PERFORATIONS/SCREENS:

☐ Perforations Method _____
☐ Screens Type _____ Material _____

From	To	Slot size	Number	Diameter	Tele/pipe size	Casing	Liner
						☐	☐
						☐	☐
						☐	☐
						☐	☐

(8) WELL TESTS: Minimum testing time is 1 hour

☐ Pump ☐ Bailer ☒ Air ☐ Flowing
Yield gal/min _____ Drawdown _____ Drill stem at _____ Time _____

1500* 200' Dr.

Temperature of water 56' Depth Artesian Flow _____
Was a water analysis done? ☐ Yes By whom _____
Did any strata contain water not suitable for intake? ☐ Salty ☐ Muddy ☐ Odor ☐ Colored ☐ Other _____
Depth of strata: _____

(9) LOCATION OF WELL by legal description:
County LAKE Latitude _____ Longitude _____
Township 25 N or S Range 18 E or W. WM.
Section 7 SE 1/4 NW 1/4
Tax Lot 1900 Lot _____ Block _____ Subdivision _____
Street Address of Well (or nearest address) 89054 5th NW
Christmas Valley OR 97641

(10) STATIC WATER LEVEL: the same
69 ft. below land surface. Date 3-12-04
Artesian pressure _____ lb. per square inch Date _____

(11) WATER BEARING ZONES:

Depth at which water was first found _____

From	To	Estimated Flow Rate	SWL
140	200	1000+	

(12) WELL LOG:

'Ground Elevation _____

Material	From	To	SWL
Black Lava Rock	140'	163'	
Broken Lava Rock	163'	180'	
Red Lignite w/B	180'	185'	
Gray Basalt	185'	200'	
RECEIVED			
JUN 13 2005			
WATER RESOURCES DEPT. SALEM, OREGON			
RECEIVED			
JUN - 3 2004			
WATER RESOURCES DEPT. SALEM, OREGON			

Date started 1-27-04 Completed 3-12-04

(unbonded) Water Well Constructor Certification:

I certify that the work I performed on the construction, alteration, or abandonment of this well is in compliance with Oregon water supply well construction standards. Materials used and information reported above are true to the best of my knowledge and belief.

WWC Number _____
Signed _____ Date _____

(bonded) Water Well Constructor Certification:

I accept responsibility for the construction, alteration, or abandonment work performed on this well during the construction dates reported above. All work performed during this time is in compliance with Oregon water supply well construction standards. This report is true to the best of my knowledge and belief.

WWC Number 16541
Signed [Signature] Date 4-19-04

RECEIVED
LAKE 4372
 MAR 12 1981
 State Well No. 255/17E-2ac
 WATER RESOURCES DEPT.
 SALEM, OREGON
 State Permit No. LAKE 4372

Name Dave Roth
Address 7urbym Rd
City Sweet Home State Ore

If abandonment, describe material and procedure in Item 12.

Very Air	☒	Driven	☐	Domestic	☐	Industrial	☐	Municipal	☐
Water Mud	☐	Dug	☐	Irrigation	☒	Test Well	☐	Other	☐
Cable	☐	Bored	☐	Thermal:		Withdrawal	☐	Reinjection	☐

CASING INSTALLED: Steel ☒ Plastic ☐
Threaded ☐ Welded ☒
14" Diam. from 0 ft. to 67 ft. Gauge 3/2
" Diam. from ft. to ft. Gauge

....." Diam. from ft. to ft. Gauge

Size of perforations _____ in. by _____ in.

(8) WELL TESTS. Drawdown is amount water level is lowered

Temperature of water _____ Depth artesian flow encountered ft.

How was cement grout placed? Tramite

Gravel placed from ft. to ft.

Formation: Describe color, texture, grain size and structure of materials; and show thickness and nature of each stratum and aquifer penetrated, with at least one entry for each change of formation. Report each change in position of Static Water Level and indicate principal water-bearing strata.

[illegible]

Contractor's License No. 357 Date 2-25, 1981

SP*12658-690

STATE OF OREGON
WATER SUPPLY WELL REPORT
(as required by ORS 537.765)

LAKE 51691

WELL I.D. # L

76807

START CARD #

171718

Instructions for completing this report are on the last page of this form.

(1) LAND OWNER

Name Roth Farms Well Number _____
Address PO Box 358
City CHRISTIANBURG State OR Zip 97611

(2) TYPE OF WORK

☒ New Well
☐ Deepening ☐ Alteration (repair/recondition) ☐ Abandonment ☐ Conversion

(3) DRILL METHOD

☒ Rotary Air ☐ Rotary Mud ☐ Cable ☐ Auger ☐ Cable Mud
☐ Other _____

(4) PROPOSED USE

☐ Domestic ☐ Community ☐ Industrial ☒ Irrigation
☐ Thermal ☐ Injection ☐ Livestock ☐ Other _____

(5) BORE HOLE CONSTRUCTION

Special Construction: ☐ Yes ☒ No
Depth of Completed Well 220 ft.
Explosives used: ☐ Yes ☒ No Type _____ Amount _____

BORE HOLE

Diameter	From	To	Material	From	To	Sacks or Pounds
23 1/2"	0	19	Bmt	0	19	50 sack
16 1/2"	19	220				

SEAL

How was seal placed: Method ☐ A ☐ B ☐ C ☐ D ☐ E

☒ Other 3/8 Hole Plug

Backfill placed from _____ ft. to _____ ft. Material _____

Gravel placed from _____ ft. to _____ ft. Size of gravel _____

(6) CASING/LINER

Diameter	From	To	Gauge	Steel	Plastic	Welded	Threaded
Casing: 18"	1	19	250	☒	☐	☒	☐
Liner:				☐	☐	☐	☐

Drive Shoe used ☐ Inside ☐ Outside ☐ Nonc

Final location of shoe(s) _____

(7) PERFORATIONS/SCREENS

☐ Perforations Method _____
☐ Screens Type _____ Material _____

From	To	Slot Size	Number	Diameter	Tele/pipe size	Casing	Liner
						☐	☐
						☐	☐
						☐	☐
						☐	☐

(8) WELL TESTS: Minimum testing time is 1 hour

☐ Pump ☐ Bailer ☒ Air ☐ Flowing Artesian

Yield gal/mip	Drawdown	Drill stem at	Time
2000 gal		220	1 hr

Temperature of water 53° Depth Artesian Flow Found _____

Was a water analysis done? ☐ Yes By whom _____

Did any strata contain water not suitable for intended use? ☐ Too little

☐ Salty ☐ Muddy ☐ Odor ☐ Colored ☐ Other _____

Depth of strata: _____

(9) LOCATION OF WELL (legal description)

County Lake
Tax Lot 300 Lot _____
Township 25 N or S Range 18 E or W WM
Section 3 SE 1/4 SE 1/4

Lat _____° _____' _____" or _____ (degrees or decimal)
Long _____° _____' _____" or _____ (degrees or decimal)

Street Address of Well (or nearest address) NO ADDRESS
assigned

(10) STATIC WATER LEVEL

61' ft. below land surface. Date 8-15-05
_____ ft. below land surface. Date same
Artesian pressure _____ lb. per square inch Date _____

(11) WATER BEARING ZONES

From	To	Estimated Flow Rate	SWL
105	220	2000 gal	

(12) WELL LOG

Ground Elevation _____

Material	From	To	SWL
76P Soil	0	2	
Gravel Basalt	2	4 1/2	
Red Lava Rock	4 1/2	60	
Black Lava Rock	60	80	
Black Lava Rock	80	105	
Gravel Lava Rock	105	145	
Black Lava Rock	145	189	
Gravel Lava Rock	189	200	
Black RECEIVED	200	220	

SEP 27 2005

WATER RESOURCES DEPT
SALEM, OREGON

RECEIVED

DEC 30 2005

WATER RESOURCES DEPT
SALEM, OREGON

Date Started 4-27-05 Completed 5-15-05

(unbonded) Water Well Constructor Certification

I certify that the work I performed on the construction, deepening, alteration, or abandonment of this well is in compliance with Oregon water supply well construction standards. Materials used and information reported above are true to the best of my knowledge and belief.

WWC Number _____ Date _____

Signed _____

(bonded) Water Well Constructor Certification

I accept responsibility for the construction, deepening, alteration, or abandonment work performed on this well during the construction dates reported above. All work performed during this time is in compliance with Oregon water supply well construction standards. This report is true to the best of my knowledge and belief.

WWC Number 165-1 Date 6-15-05

Signed [Signature]