Groundwater Application Review Summary Form

Application # G- <u>18760</u>

GW Reviewer <u>Grayson Fish</u> Date Review Completed: <u>8/11/2023</u>

Summary of GW Availability and Injury Review:

Groundwater for the proposed use is either over appropriated, will not likely be available in the amounts requested without injury to prior water rights, OR will not likely be available within the capacity of the groundwater resource per Section B of the attached review form.

Summary of Potential for Substantial Interference Review:

There is the potential for substantial interference per Section C of the attached review form.

Summary of Well Construction Assessment:

The well does not appear to meet current well construction standards per Section D of the attached review form. Route through Well Construction and Compliance Section.

This is only a summary. Documentation is attached and should be read thoroughly to understand the basis for determinations and for conditions that may be necessary for a permit (if one is issued).

WATER RESOURCES DEPARTMENT

MEMO

8/11/2023

TO: Application G-<u>18760</u>

FROM: GW: <u>Grayson Fish</u> (Reviewer's Name)

SUBJECT: Scenic Waterway Interference Evaluation

- ✓ YES The source of appropriation is hydraulically connected to a State Scenic Waterway or its tributaries
- ☑ YES☑ Use the Scenic Waterway Condition (Condition 7J)
- Per ORS 390.835, the Groundwater Section is **able** to calculate ground water interference with surface water that contributes to a Scenic Waterway. The calculated interference is distributed below
- □ Per ORS 390.835, the Groundwater Section is unable to calculate ground water interference with surface water that contributes to a scenic waterway; therefore, the Department is unable to find that there is a preponderance of evidence that the proposed use will measurably reduce the surface water flows necessary to maintain the free-flowing character of a scenic waterway

DISTRIBUTION OF INTERFERENCE

Calculate the percentage of consumptive use by month and fill in the table below. If interference cannot be calculated, per criteria in 390.835, do not fill in the table but check the "unable" option above, thus informing Water Rights that the Department is unable to make a Preponderance of Evidence finding.

Exercise of this permit is calculated to reduce monthly flows in <u>Klamath</u> Scenic Waterway by the following amounts expressed as a proportion of the consumptive use by which surface water flow is reduced.

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
See A	Attached	d Mem	o "An	alysis	of Gro	undwa	ter Pu	mping	Impact	s on	Scenic
Water	rway Fl	ows" da	ted: Fe	bruary	y 19, 20 1	13.			_		

PUBLIC INTEREST REVIEW FOR GROUNDWATER APPLICATIONS

TO: FROM:	Water Rights Section Groundwater Section	Date <u>8/11/2023</u> Grayson Fish	
SUBJECT:	Application G- <u>18760</u>	Reviewer's Name Supersedes review of <u>6/15/2020</u> Date of Review(s)	_
PUBLIC INTE OAR 690-310-1 welfare, safety a to determine what the presumption A. <u>GENERAL</u>	EREST PRESUMPTIO 30 (1) The Department shal nd health as described in O. ether the presumption is esta criteria. This review is bas INFORMATION:	4: GROUNDWATER presume that a proposed groundwater use will ensure the preservation of the public 2S 537.525. Department staff review groundwater applications under OAR 690-310-140 blished. OAR 690-310-140 allows the proposed use be modified or conditioned to meet ed upon available information and agency policies in place at the time of evaluation. Applicant's Name: Wallace Family Farms County: Klamath	

Applicant(s) seek(s) <u>1.32</u> cfs from <u>1</u> well(s) in the <u>Klamath</u> Basin, A1. Fourmile Creek subbasin

A2. Proposed use Irrigation (211.42 ac with a total volume limited to 317.13 acre feet) Seasonality: Apr. 1 – Oct. 31 (214 d)

A3. Well and aquifer data (attach and number logs for existing wells; mark proposed wells as such under logid):

Well	Logid	Applicant's Well #	Proposed Aquifer*	Proposed Rate(cfs)	Location (T/R-S QQ-Q)	Location, metes and bounds, e.g. 2250' N, 1200' E fr NW cor S 36
1	PROPOSED	1	Bedrock	1.32	36S/06E-17 SWSW	1236' N, 312' E of SW cor S 17
2						

* Alluvium, CRB, Bedrock

Well	Well Elev ft msl	First Water ft bls	SWL ft bls	SWL Date	Well Depth (ft)	Seal Interval (ft)	Casing Intervals (ft)	Liner Intervals (ft)	Perforations Or Screens (ft)	Well Yield (gpm)	Draw Down (ft)	Test Type
1	4172		30-70		350	0-18	+2-150					

Use data from application for proposed wells.

A4. Comments: The applicant's well is proposed but notes in the application mentioned that the well will be constructed to produce from "predominately basalt layers"; it is likely that the actual final depth will not be exactly 350 feet. SWL is estimated from nearby wells although there are no wells in the area close to the proposed depth. This rereview uses proposed rates and duties listed in the letter titled "Mitigation for Application G-18760" dated August 13, 2020 from Water Right Solutions, LLC.

A5. **Provisions of the** Klamath (OAR 690-0025) Basin rules relative to the development, classification and/or

management of groundwater hydraulically connected to surface water \Box are, or \boxtimes are not, activated by this application. (Not all basin rules contain such provisions.)

Comments: The rules listed in OAR 690-0025 are defunct and do not apply.

A6. Well(s) # _____, ____, ____, ____, tap(s) an aquifer limited by an administrative restriction.

Name of administrative area: Comments:

B. GROUNDWATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070

- B1. **Based upon available data**, I have determined that <u>groundwater</u>* for the proposed use:
 - a. is over appropriated, is not over appropriated, *or* cannot be determined to be over appropriated during any period of the proposed use. * This finding is limited to the groundwater portion of the over-appropriation determination as prescribed in OAR 690-310-130;
 - b. **will not** *or* **will** likely be available in the amounts requested without injury to prior water rights. * This finding is limited to the groundwater portion of the injury determination as prescribed in OAR 690-310-130;
 - c. \Box will not or \Box will likely to be available within the capacity of the groundwater resource; or
 - d. 🛛 will, if properly conditioned, avoid injury to existing groundwater rights or to the groundwater resource:
 - i. \square The permit should contain condition #(s)
 - 7N(Annual SWL); 7T(Measuring Tube); 7J; Large Water-Use Reporting:
 - ii. \Box The permit should be conditioned as indicated in item 2 below.
 - iii. \Box The permit should contain special condition(s) as indicated in item 3 below;
- B2. a. Condition to allow groundwater production from no deeper than ______ ft. below land surface;
 - b. Condition to allow groundwater production from no shallower than ______ ft. below land surface;
 - c. Condition to allow groundwater production only from the groundwater reservoir between approximately______ft. and______ft. below land surface;
 - d. **Well reconstruction** is necessary to accomplish one or more of the above conditions. The problems that are likely to occur with this use and without reconstructing are cited below. Without reconstruction, I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Groundwater Section.

Describe injury –as related to water availability– that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc):

B3. Groundwater availability remarks: The proposed well would produce water from "predominantly basalt layers" which would mean the well would likely extend to a depth deeper than 200'. The well log of KLAM 58670 drilled approximately 1 mile away at a similar elevation of the proposed well encountered water bearing "grey basalt & red cinder" starting at 179' bls and a static water level of 5' bls. Static water levels in any given well appears to be controlled by topography and is close to surface water elevation. Groundwater level data is limited in the area, however, KLAM 10521 is located approximately ¹/₄mile southwest of the POA and groundwater levels in that well have not excessively declined or shown an excessively declining trend. Therefore, a preponderance of evidence does not exist to say that groundwater is over-appropriated. The applicant's proposed well is located within 1 mile of a densely-developed neighborhood (several 1-acre lots) where most of the tax lots that have been developed have a domestic well associated with them (nearly 40 wells have been drilled in the Section which are concentrated in the southern part near the proposed POA). Approximately 20 tax lots are within ¹/₄ mile of the proposed POA. Many of the well logs for this area report total well depths around 100 to 150 feet and SWLs between 20 and 70 ft (the range of SWLs are more likely controlled by land surface elevation and not vertical changes in hydrogeologic characteristics). A Theis distance drawdown model along with the newly proposed rate of 1.32 cfs as listed in the proposed mitigation plan was used to estimate the magnitude of well-to-well interference that may result from the proposed uses (Theis). Drawdown from the proposed use at neighborhood wells within ¹/₄ mile may be over 5 feet by the end of the irrigation season. It should be noted that this is likely an overly conservative estimate as if the applicant was to exercise their full requested rate of 1.32 cfs they would fulfil their proposed duty of 317.13 ac/ft in 121 days, almost half the expected irrigation season. Regardless, even at the fully requested rate for the entirety of the irrigation season, a preponderance of evidence does not exist to determine injury is likely to occur. Permit conditions should be applied as referenced in B1(d)(i) of this form.

5

C. GROUNDWATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. 690-09-040 (1): Evaluation of aquifer confinement:

Well	Aquifer or Proposed Aquifer	Confined	Unconfined
1	Volcanic Rocks of the Late High Cascades	\boxtimes	

Basis for aquifer confinement evaluation: Well logs for the area typically report some variation of "clay" for 50+ feet near the surface before encountering "gravel" or "broken rock". The presence of a moderately thick, mixed-clay zone will likely add confinement to the deeper aquifer zones that the applicant's proposing to produce from.

C2. **690-09-040** (2) (3): Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¹/₄ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	GW Elev ft msl	SW Elev ft msl	Distance (ft)	YES	Hydraulically Connected? YES NO ASSUMED		Potentia Subst. In Assum YES	ll for terfer. ed? NO
1	1	Fourmile Creek	~4140	4160-4200	2330	Ø				Ø

Basis for aquifer hydraulic connection evaluation: Groundwater elevation was estimated mostly from well logs uphill from the proposed POA and likely represent deeper water level depths than would be encountered in the proposed well. Therefore, GW elevation in the proposed POA would likely be higher and closer to surface water elevations, implying that water is capable of moving easily between surface water and groundwater.

Water Availability Basin the well(s) are located within: Link R > Klamath R - AB Unn Str (ID# 31420305)

C3a. **690-09-040** (4): Evaluation of stream impacts for <u>each well</u> that has been determined or assumed to be **hydraulically** connected and less than 1 mile from a surface water (SW) source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that SW source, not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% *natural* flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked ⊠ box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < ¼ mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
1	1			KA 484	0.4	<mark>X</mark>	808		<10 %	<mark>N</mark>

C3b. **690-09-040** (**4**): Evaluation of stream impacts <u>by total appropriation</u> for all wells determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. **Complete only if Q is distributed among wells**. Otherwise same evaluation and limitations apply as in C3a above.

 			-					
SW #	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?

Comments: Instream Right KA 484 is located on Fourmile Cr. In the immediate vicinity and within 1 mile of the proposed POA and the proposed rate is greater than 1% of the instream water right.

Stream-depletion was estimated using the Hunt-2003 stream-depletion model using parameter values derived from aquifer tests in the area, extracted from Gannett et al., (2012), or representative of the geologic material in the vicinity of the proposed POA.

C4a. 690-09-040 (5): Estimated impacts on hydraulically connected surface water sources greater than one mile as a

percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

Non-D	istributed	Wells											
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	Q as CFS												
Interfer	ence CFS												
D' 4 'I	4 1 3 3 7 11	1											
Distrib Wall	SW#	IS Ion	Fab	Mor	Apr	Mov	Iun	In1	A 110	Son	Oct	Nov	Dec
wen	510#	Jall	reu	Iviai	Арі	Way	Juli	Jui	Aug	Sep	001	INUV	Dec
		%	%	%	%	%	%	%	%	%	%	%	%
Well (Q as CFS												
Interfer	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	Q as CFS												
Interfer	ence CFS												
		1	T	1	T	T		T	T	1	1	T	T
$(\mathbf{A}) = \mathbf{T}\mathbf{c}$	otal Interf.												
(B) = 80	% Nat. Q												
(C) = 1	% Nat. Q												
							-			-	-		
(D) =	(A) > (C)	\checkmark											
(E) = (A	/ B) x 100	%	%	%	%	%	%	%	%	%	%	%	%

 (\overline{A}) = total interference as CFS; (B) = WAB calculated natural flow at 80% exceed. as CFS; (C) = 1% of calculated natural flow at 80% exceed. as

CFS; (D) = highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage. **Basis for impact evaluation:**

C4b. 690-09-040 (5) (b) The potential to impair or detrimentally affect the public interest is to be determined by the Water Rights Section.

- C5. If properly conditioned, the surface water source(s) can be adequately protected from interference, and/or groundwater use under this permit can be regulated if it is found to substantially interfere with surface water:
 - i. \Box The permit should contain condition #(s)_
 - ii. \Box The permit should contain special condition(s) as indicated in "Remarks" below;
- C6. SW / GW Remarks and Conditions: <u>The applicant's proposed POA would be producing from an aquifer that has been found</u> to be hydraulically connected to surface water – specifically Fourmile Creek at a distance of less than 1 mile. <u>The proposed</u> maximum rate of appropriation is less than 1% of the pertinent adopted perennial streamflow for the WAB but is greater than 1% of the adopted instream water right for Fourmile Creek. **Per OAR 690-009-0040(4) the POA is assumed to have the Potential** for Substantial Interference.

The applicant has proposed mitigation as detailed in the letter titled "Mitigation for Application G-18760" dated August 13, 2020 from Water Right Solutions, LLC.

References Used:

- Gannett, M. W., B. J. Wagner, and K. E. Lite. 2012. Groundwater Simulation and Management Models for the Upper Klamath Basin, Oregon and California. USGS Scientific Investigations report 2012-5062.
- Gannett, M. W., K. E. Lite, J. L. LaMarche, B. J. Fisher, and D. J. Polette. 2007. Ground-water Hydrology of the Upper Klamath Basin, Oregon and California. USGS Scientific Investigations Report 2007-5050
- Hunt, B. 2003. Unsteady Stream Depletion when Pumping from a Semiconfined Aquifer. Journal of Hydrologic Engineering. Vol 8(1), pp 12-19
- Sherrod, D. R., and L. B. G. Pickthorn. 1992. *Geologic Map of the West Half of the Klamath Falls 1° by 2° Quadrangle, South-*<u>Central Oregon. USGS Miscellaneous Investigations Series Map I-2182.</u>

OWRD Well Log Database - Accessed 8/11/2023

Theis, C.V., 1935. The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using groundwater storage, Am. Geophys. Union Trans., vol. 16, pp. 519-524.

D. WELL CONSTRUCTION, OAR 690-200

D1.	Well #: Logid:	
D2.	THE WELL does not appear to meet current well construction standards based upon: a. □ review of the well log; b. □ field inspection by	;;
D3.	THE WELL construction deficiency or other comment is described as follows:	
D4. [\Box Route to the Well Construction and Compliance Section for a review of existing well construction.	

Water Availability Tables

		Water	Availability Ar Detailed Reports	nalysis		
		LII	NK R > KLAMATH R - AB UNN KLAMATH BASIN	STR		
Watershed ID # Date: 8/3/2023	έ 31420305 <u>(Map</u>)		Water Availability as of 8/3/202	3	Exce	edance Level: 80% 🗸 Time: 8:20 AM
Wat	ter Availability Calculation Wa	Consumptive Uses and Stor	lages	nstream Flow Requirements Wate	Reservatio	ns
		Wate Month Annual	er Availability Calcu ly Streamflow in Cubic Feet per Volume at 50% Exceedance in J	lation Second Acre-Feet		
Month	Natural Stream Flow	Consumptive Uses and Storages	Expected Stream Flow	Reserved Stream Flow	Instream Flow Requirement	Net Water Available
JAN	1,470.00	576.00	894.00	0.00	60.00	834.00
FEB	1,520.00	972.00	548.00	0.00	60.00	488.00
	2 220 00	1,040.00	1 100 00	0.00	80.00	1 020 00
MAY	2 100 00	1,120.00	815.00	0.00	83.00	732.00
JUN	1 670 00	1 510 00	160.00	0.00	74 00	86.10
JUL	1.180.00	1.370.00	-188.00	0.00	20.00	-208.00
AUG	914.00	1.060.00	-147.00	0.00	40.00	-187.00
SEP	830.00	827.00	3.06	0.00	30.00	-26.90
OCT	808.00	325.00	483.00	0.00	30.00	453.00
NOV	952.00	333.00	619.00	0.00	30.00	589.00
DEC	1,240.00	569.00	671.00	0.00	50.00	621.00
ANN	1,500,000.00	662,000.00	838,000.00	0.00	38,400.00	800,000.00

Well Location Map

G-18760



Service Layer Credits: Sources: Esri, HERE, Garmin, Intermap, increment P Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBase, IGN, Kadaster NL, Ordnance Survey, Esri Japan, METI, Esri

Service Layer Creans: Sources, Ean, HENE, Gammin, Internant, Internant, Roberts F, Octov, Hene, National Structures Community USGS The National Map: National Boundaries Dataset, 3DEP Elevation Program, Geographic Names Information System, National Hydrography Dataset, National Land Cover Database, National Structures Dataset, and National Transportation Dataset; USGS Global Ecosystems; U.S. Census Bureau TIGER/Line data; USFS Road Data; Natural Earth Data; U.S. Department of State

9

Observation Well Data KLAM 1122 KLAM 1747 4160 KLAM 10521 80 4155 Annual Precipitation (Inches per Year) ⁴¹¹⁰ GW elevation (ft AMSL) 60 40 20 4135 4130 Mean precipitation (1895-present) 0 1975 1985 1995 2005 2015 2025 Date (Water year for precipitation) Well Stats for 36S/6E -7, 8, 9 and 16 - 21 0.0 0.2 0.4 0.6 0.8 1.0 0.0 0.4 0.6 0.8 1.0 0.2 Well Compl Depth [ft] 00 00 00 00 00 40 0. 0.8 SWL [ft bls] 500 30 0.6 n = 115 med = 25.0 20 fied 0.4 10 0.2 n = 115 ned = 45.0 n = 115 med = 116.0 omitted vield="0": 1 SWL ic nth ia 300 0 0.0 0 150 200 2 Well Yield [gpm] 25 Ó 50 100 250 300 350 10 15 20 25 0 10 15 20 freq freq 40 0 0 Well Compl Depth [ft] [sl 100 200 SWL [ft bls] 30 200 20 freq 10 400 300 0 1990 2000 2010 2020 2030 Drill Date 1972 1982 1992 2002 2012 2022 1972 1982 1992 2002 2012 2022 1960 1970 1980 Drill Date Drill Date Well Compl Depth [ft] 00 00 00 00 00 Well Compl Depth [ft] WBZ [ft bls] 100 200 Depth to 300 400 150 200 250 300 350 50 150 250 300 50 100 Ó 100 200 0 50 100 150 200 250 300 350 400 Well Yield [gpm] SWL [ft bls] SWL [ft bls] 0 0 Includes Data from Water Wells only [100 SWL [ft bls] 200 200 [ft pls] 200 ŧ ₫ Well Logs per section exported to file: C:\Users\Public\found_trs_keys_RESULTS.txt Well Log Data exported to file: C:\Users\gwater\Desktop\Working Folder\well_data.txt 300 300 150 200 250 300 350 i ż 10 11 12 50 100 ż 4 9 5 6 7 8 0 Created 08/11/2023 Well Yield [gpm] Drill Month

Water-Level Measurements in Nearby Wells

Theis Distance-Drawdown

Theis Time-Drawdown Worksheet v.5.00

Calculates Theis nonequilibrium drawdown and recovery at any arbitrary radial distance, r, from a pumping well for 3 different T values and radial distance, r, from a pumping well for 3 different T values and 2 different S values. Written by Karl C. Wozniak September 1992. Last modified December 17, 2019

Input Data:	Var Name	Scenario 1	Scenario 2	Scenario 3	Units	
Total pumping time	t		214		d	
Radial distance from pumped well:	r		1320		ft	Q conversions
Pumping rate	Q		1.32		cfs	592.42 gpm
Hydraulic conductivity	K	10	40	60	ft/day	1.32 cfs
Aquifer thickness	b		300		ft	79.20 cfm
Storativity	S_1		0.0001			114,048.00 cfd
	S_2		0.001			2.62 af/d
Transmissivity Conversions	T_f2pd	3000	12000	18000	ft2/day	
	T_ft2pm	2.0833333	8.3333333	12.5	ft2/min	Recalculate
	T_gpdpft	22440	89760	134640	gpd/ft	



Use the Recalculate button if recalculation is set to manual

Hunt Streamflow Depletion

Application type:	G
Application number:	18760
Well number:	1
Stream Number:	1
Pumping rate (cfs):	1.32
Pumping duration (days):	214
Pumping start month number (3-March)	4.0

Parameter		Symbol	Scenario 1		Scenario 2		Scenario 3		Units			
Distance from well to stream			a	2330.0		2330.0		2330.0		ft		
Aquifer transmissivity			Т	5000.0		12000.0		20000.0		ft2/day		
Aquifer storativity			S	0.0006		0.0006		0.0006		-		
Aquitard vertical hydraulic conductivity			Kva	0.01		0.05		0.1		ft/day		
Aquitard saturated thickness			ba	10.0		10.0		10.0		ft		
Aquitard thickness below stream Aquitard specific yield			babs	8.0 0.2		5.0 0.1		2.0 0.05		ft -		
			Sya									
Stream width		ws	20.0		20.0		20.0		ft			
				St	ream dep	letion f	for Scen	ario 2:				
Days	10	300	330	360	30	60	90	120	150	180	210	240
Depletion (%)	0	2	2	2	1	1	2	2	2	3	3	3
Depletion (cfr)	0.01	0.03	0.03	0.03	0.01	0.02	0.02	0.03	0.03	0.04	0.04	0.03



Appendix Memo: Analysis of Groundwater Pumping Impacts on Scenic Waterway Flows



State of Oregon Water Resources Department

Memorandum

To: Barry Norris – Administrator, Technical Services Division Dwight French – Administrator, Waterights Division Tom Paul – Deputy Director Doug Woodcock – Administrator, Field Services Division

From: Ivan Gall – Manager, Groundwater Section //

Date: February 19, 2013

Subject: Analysis of Groundwater Pumping Impacts on Klamath Scenic Waterway Flows

In 1971 the Oregon Legislature created the Scenic Waterway Act, codified by Oregon Revised Statutes 390.805 to 390.925, to preserve for the benefit of the public Waldo Lake and selected parts of the state's free-flowing rivers. The Klamath Scenic Waterway was part of the Act and includes the Klamath River from the John Boyle Dam powerhouse downstream to the Oregon-California border. Under the Act, the Water Resources Commission is allowed to allocate small amounts of surface water for human consumption and livestock watering, as long as issuing the water right does not significantly impair the free-flowing character of these waters in quantities necessary for recreation, fish and wildlife, and the amount allocated may not exceed a cumulative total of one percent of the average daily flow or one cubic foot per second (cfs), whichever is less.

In 1995 the Scenic Waterway Act was modified to address the impact of groundwater uses that, based upon a preponderance of evidence, would measurably reduce the surface water flows within a scenic waterway. "Measurably reduce" means that the use authorized will individually or cumulatively reduce surface water flows within the scenic waterway in excess of a combined cumulative total of one percent of the average daily flow or one cfs, whichever is less.

In 2012 the United States Geological Survey (USGS), in cooperation with OWRD and the US Bureau of Reclamation, completed groundwater flow and management models for the Upper Klamath Basin. The 2012 groundwater flow model uses generally accepted hydrogeologic methods and the relevant field data to model the cumulative effects of groundwater pumping within the Klamath Scenic Waterway, and provides a comprehensive methodology for analyzing the relevant field data necessary to determine whether the cumulative use of groundwater in the Klamath Basin will measurably reduce the surface water flow necessary to maintain the freeflowing character of the Klamath Scenic Waterway.

In September 2012 the OWRD Groundwater Section conducted two model simulations. The two simulations used the 2012 USGS flow model, incorporating groundwater permits Issued (61.96 cfs) since adoption of the 1995 Scenic Waterway Act amendment up through 2004. Each simulation was run to steady-state, where inflows and outflows for that model run balanced. An evaluation of the water budgets showed that groundwater discharge to the Klamath Scenic Waterway decreased by 5.88 cfs as a result of the 61.96 cfs of groundwater uses issued between 1995 and 2004. These results indicate to the OWRD that a preponderance of evidence exists to establish that groundwater development occurring in the Upper Klamath Basin in Oregon since 1995 has "measurably reduced" surface water flows within the Klamath Scenic Waterway.

In January 2013 the OWRD Groundwater Section conducted flow model simulations to evaluate impacts to streams from pumping groundwater within the Lost River subbasin. Groundwater pumping was simulated by placing wells in the model that correspond to the center of 39 townships in the southeast part of the Klamath Basin in Oregon. Each of the simulations was run to steady-state, where inflows and outflows for that model run balanced. These results indicate that the scenic waterway is impacted by pumping groundwater in all of the townships evaluated in Oregon in the Lost River subbasin. In summary, a preponderance of evidence exists to establish that groundwater development occurring in Oregon since 1995 in the Upper Klamath Basin and Lost River subbasin has "measurably reduced" surface water flows within the Klamath Scenic Waterway.

References:

Gannett, M.W., Lite, K.E., Jr., La Marche, J.L., Fisher, B.J., and Polette, D.J., 2007. Ground-water hydrology of the upper Klamath Basin, Oregon and California: U.S. Geological Survey Scientific Investigations Report 2007-5050, 84p.

Gannett, M.W., Wagner, B.J., and Lite, K.E., Jr., 2012. Groundwater simulation and management models for the upper Klamath Basin, Oregon and California: U.S. Geological Survey Scientific Investigations Report 2012-5062, 92p. 14