Approved:

Мемо

To:	Kristopher Byrd, Well Construction Manager
From:	Tommy Laird, Well Construction Program Coordinator
Subject:	Re-Review of Water Right Application G-18840
Date:	May 23, 2024

The attached application was forwarded to the Well Construction Section by the Groundwater Section. Travis Brown reviewed the application. Please see Travis' Groundwater Review and the Well Report.

Applicant's Well #1 (MARI 68155): Based on a review of the Well Report, Applicant's Well #1 seems to protect the groundwater resource.

The construction of Well #1 may not satisfy hydraulic connection issues.

Applicant's Well #2 through Well #5 (Proposed): Well #2 through Well #5 are proposed wells, therefore they cannot be reviewed for construction. Construction of these proposed wells shall be completed in a manner that protects ground water resources as required under Oregon Administrative Rules 690-200 through 690-240. During construction of these wells, specific attention should be paid to ensure sealing requirements are met and that the wells do not commingle aquifers.

The construction of proposed Well #2 through Well #5 may not satisfy hydraulic connection issues.

STATE OF OREGON WATER SUPPLY WELL REPORT (as required by ORS 537.765 & OAR 690-205-0210)

MARI 68155

.....

WELL I.D. LABEL# L	
START CARD #	1039580
ORIGINAL LOG #	

.....

(1) LAND OWNER Owner Well I.D. 5904	- MARI 68155
First Name Last Name	(9) LOCATION OF WELL (legal description)
Company Mayfield Farms	
Address 18555 SW Teton Ave.	County MARION Twp 3 S N/S Range 1 W E/W WM
City Tualatin State OR Zip 97062	Sec <u>32</u> <u>SE</u> 1/4 of the <u>SE</u> 1/4 Tax Lot <u>1700</u>
	Tax Map Number Lot
	Tax Map Number Lot Lat ' OMS or DD
Alteration (complete 2a & 10) Abandonment(complete 5a)	Long o or DMS or DD
(2a) PRE-ALTERATION Dia + From To Gauge Stl Plstc Wid Thrd	Street address of well Nearest address
Casing:	(Sheet address of went (Nearest address
	11303 Arndt Rd. NE - Aurora, OR 97002
Seal: To Amt_sacks/lbs	
Seal: RECEIVED	
(3) DRILL METHOD	(10) STATIC WATER LEVEL
Rotary Air Rotary Mud Cable Auger Cable 19	Date SWL(psi) + SWL(ft)
Reverse Rotary Other DEF Z V 2010	Existing Well / Pre-Alteration
	Completed Well 08-24-2018 96
(4) PROPOSED USE X Domestic Irrigation Community	Flowing Artesian? Dry Hole?
Industrial/Commericial Livestock Dewatern QWRD	
	WATER BEARING ZONES Depth water was first found <u>185</u>
Thermal Injection Other	SWL Date From To Est Flow SWL(psi) + SWL(ft)
(5) BORE HOLE CONSTRUCTION Special Standard (Attach copy	08-24-2018 185 207 350 + 96
Depth of Completed Well 217 ft.	08-24-2018 185 207 350 + 96
Dia From To Material From To Amt Ibs	
16 0 217 Cement 20 120 84 S	
Calculated 47.8	
Bentonite 0 20 16 S	
Calculated 15.8	(11) WELL LOG Ground Elevation
How was seal placed: Method A B XC D E	Material From To
X Other Poured dry	Topsoil 0 2
	Brown clay 2 34
Backfill placed from <u>67</u> fl. to <u>197</u> fl. Material <u>\$/12</u> Filter pack from <u>120</u> fl to <u>197</u> fl. Material Colorado Size 10/20	Blue clay 34 54
Filter pack from 120 h. to 197 h. Material Colorado Size 10/20	Blue clay sandy 54 82
Explosives used Yes Type Amount	
(5a) ABANDONMENT USING UNHYDRATED BENTONITE	Blue sandy clay 112 182
Proposed Amount Pounds Actual Amount Pounds	Cemented gravel 182 187
(6) CASING/LINER	Black sand & gravel 187 202
Casing Liner Dia + From To Gauge Stl Plate Wid The	Cmeneted gravel 202 207
Casing Liner Dia + From To Gauge Stl Plstc Wld Thrd	Cmeneted gravel 202 207 Blue clay 207 217
Casing Liner Dia + From To Gauge Stl Plstc Wld Thrd	
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ORIGINAL - WATER RESOURCES DEPARTMENT THIS REPORT MUST BE SUBMITTED TO THE WATER RESOURCES DEPARTMENT WITHIN 30 DXYS OF COMPLETION OF WORK Form Version: 0.95

Groundwater Application Review Summary Form

Application # G- <u>18840 re-review</u>

GW Reviewer <u>Travis Brown</u> Date Review Completed: <u>6/20/2023</u>

Summary of GW Availability and Injury Review:

Groundwater for the proposed use is either over appropriated, will not likely be available in the amounts requested without injury to prior water rights, OR will not likely be available within the capacity of the groundwater resource per Section B of the attached review form.

Summary of Potential for Substantial Interference Review:

There is the potential for substantial interference per Section C of the attached review form.

Summary of Well Construction Assessment:

L The well does not appear to meet current well construction standards per Section D of the attached review form. Route through Well Construction and Compliance Section.

This is only a summary. Documentation is attached and should be read thoroughly to understand the basis for determinations and for conditions that may be necessary for a permit (if one is issued).

WATER RESOURCES DEPARTMENT

MEMO

June 20, 2023

TO: Application G- 18840 re-review

FROM: GW: <u>Travis Brown</u> (Reviewer's Name)

SUBJECT: Scenic Waterway Interference Evaluation

- □ YES The source of appropriation is hydraulically connected to a State Scenic Waterway or its tributaries
- □ YES
 □ Use the Scenic Waterway Condition (Condition 7J)
 □ NO
- Per ORS 390.835, the Groundwater Section is **able** to calculate ground water interference with surface water that contributes to a Scenic Waterway. The calculated interference is distributed below
- □ Per ORS 390.835, the Groundwater Section is unable to calculate ground water interference with surface water that contributes to a scenic waterway; therefore, the Department is unable to find that there is a preponderance of evidence that the proposed use will measurably reduce the surface water flows necessary to maintain the free-flowing character of a scenic waterway

DISTRIBUTION OF INTERFERENCE

Calculate the percentage of consumptive use by month and fill in the table below. If interference cannot be calculated, per criteria in 390.835, do not fill in the table but check the "unable" option above, thus informing Water Rights that the Department is unable to make a Preponderance of Evidence finding.

Exercise of this permit is calculated to reduce monthly flows in <u>[Enter]</u> Scenic Waterway by the following amounts expressed as a proportion of the consumptive use by which surface water flow is reduced.

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec

PUBLIC INTEREST REVIEW FOR GROUNDWATER APPLICATIONS

TO: FROM			Rights Se	ction		Travis E	Brown			Ι	Date <u>6/20</u>	0/2023
110000	•	0100010					ver's Name					
SUBJE	CT:	Applic	ation G- 1	8840 re-revi	ew	Supe	ersedes r	eview of <u>8/28</u>	/2019			
						~~r				Date of Revi	ew(s)	
		DECT	DDECIN			WATED						
OAR 69 welfare, to detern the pres	90-310-13 safety and mine whet umption c	0 (1) <i>Th</i> <i>d health</i> her the riteria.	e Departm as describ presumptio This revie	<i>ed in ORS 5</i> on is establis w is based u	esume that 37.525. De hed. OAR pon availa	<i>a proposea</i> epartment s 690-310-14 a ble inforn	<i>l groundw</i> staff revie 40 allows nation an	water use will en w groundwater the proposed us d agency polici	applications se be modifie ies in place a	under OAR ed or conditi at the time	690-310- ioned to n of evalua	-140 neet tion .
A. <u>GE</u>	NERAL	INFOF	RMATIO	<u>N</u> : App	olicant's N	ame: <u>N</u>	layfield l	Farms, LLC		County: <u>I</u>	MARION	1
A1.				cfs from				Willamette				Basin,
A2.	Proposed	use	Com	mercial		Seaso	nality: <u>`</u>	Year-round				
A3.	Well and	aquifer	data (atta	ch and num	ber logs fo	or existing	wells; m	ark proposed v	vells as such	under logi	d):	
Well	Logic	1	Applicant ⁷ Well #	s Propose	d Aquifer*	Propo Rate(c		Location (T/R-S QQ-Q		ation, metes a)' N, 1200' E		
1	MARI 68	3155	1	All	uvium	0.45	5	3S/1W-32 SE-5	SE 33	5' N, 1165' W	fr SE cor S	32
2	Propos	ed	2	All	uvium	0.45	5	3S/1W-32 SE-5		0' N, 930' W f		
3	Propos		3		uvium	0.45		3S/1W-32 SE-5		5' N, 765' W f		
4	Propos		4		uvium	0.45		3S/1W-32 SE-5		5' N, 565' W I		
5	Propos		5	All	uvium	0.45	5	3S/1W-32 SE-5	SE 9	50' N, 580' W	fr SE cor S	32
* Alluviu	ım, CRB, E	Bedrock										
Well	Well Elev	First Water ft bls	SWL ft bls	SWL Date	Well Depth	Seal Interval	Casing Interval	s Intervals	Perforation Or Screens	Yield	Draw Down	Test Type
1	ft msl ~196 ^a	185	96	8/24/2018	(ft) 217	(ft) 0-120	(ft) +2-167	(ft)	(ft) 167-207	(gpm) 175	(ft)	Air
1	~190	165	90	8/24/2018	217	0-120	207-217	,	(Screen)	175		AII
2	~192 ^a				220 ^b	0-120 ^b	0-220 ^b		(Screen) TBD ^b			
3	~193ª				220 ^b	0-120 ^b	0-220 ^b		TBD ^b			
4	~193ª				220 ^b	0-120 ^b	0-220 ^b		TBD ^b			
5	~189				220 ^b	0-120 ^b	0-220 ^b		TBD ^b			
		cation fo	r proposed	wells.	÷			1		I		
A4.	Commer	nts: <u>The</u>	e proposed				miles east	of the unincorp	orated comm	unity of But	teville, O	regon.

^a LIDAR elevation at existing/proposed well location (Watershed Sciences, 2009)

^b Proposed construction from application

A5. **Provisions of the** <u>Willamette</u> Basin rules relative to the development, classification and/or management of groundwater hydraulically connected to surface water **are**, *or* **are not**, activated by this application. (Not all basin rules contain such provisions.) Comments: <u>The proposed POA are greater than ¹/4 mile from the nearest surface water source; therefore, per OAR 690-502-0240 the relevant Willamette Basin rules (OAR 690-502-0050) do not apply.</u>

A6. Well(s) # _____, ____, ____, ____, ____, tap(s) an aquifer limited by an administrative restriction. Name of administrative area: N/A _______, _____, tap(s) an aquifer limited by an administrative restriction.

B. GROUNDWATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070

- B1. **Based upon available data**, I have determined that <u>groundwater</u>* for the proposed use:
 - a. **is** over appropriated, **is not** over appropriated, *or* **cannot be determined to be** over appropriated during any period of the proposed use. * This finding is limited to the groundwater portion of the over-appropriation determination as prescribed in OAR 690-310-130;
 - b. **will not** *or* **will** likely be available in the amounts requested without injury to prior water rights. * This finding is limited to the groundwater portion of the injury determination as prescribed in OAR 690-310-130;
 - c. **will not** *or* **will** likely to be available within the capacity of the groundwater resource; or
 - d. X will, if properly conditioned, avoid injury to existing groundwater rights or to the groundwater resource:
 i. X The permit should contain condition #(s) <u>7n (annual measurement condition), medium water use</u> reporting;
 - ii. \square The permit should be conditioned as indicated in item 2 below.
 - iii. The permit should contain special condition(s) as indicated in item 3 below;
- B2. a. Condition to allow groundwater production from no deeper than ______ ft. below land surface;
 - b. Condition to allow groundwater production from no shallower than ______ ft. below land surface;
 - c. Condition to allow groundwater production only from the <u>alluvial</u> groundwater reservoir between approximately_____ft. and_____ft. below land surface;
 - d. **Well reconstruction** is necessary to accomplish one or more of the above conditions. The problems that are likely to occur with this use and without reconstructing are cited below. Without reconstruction, I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Groundwater Section.

Describe injury –as related to water availability– that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc):

B3. **Groundwater availability remarks:** The proposed POA are or would be completed in sand and gravel of the Willamette Aquifer (Gannett and Caldwell, 1998). Proposed POA 1 (MARI 68155) produces from ~25 ft of black sand and gravel (some cemented) between ~185-207 ft below land surface (bls), which is overlain by fine-grained sediments to land surface (per the well log), generally classified as the Willamette Silt (Gannett and Caldwell, 1998). The other proposed POA, which have similar proposed construction to MARI 68155, are anticipated to produce water from the same or equivalent water-bearing zones. Some nearby wells (MARI 134 and MARI 304, for example) do produce relatively small quantities of water (<35 gpm) from thin (<10 ft thick) layers of sand within the Willamette Silt.

The nearest senior groundwater right producing from similar water-bearing zones as the proposed POA is MARI 143, authorized POA for Certificate 42114. MARI 143 is ~860 ft east of proposed POA 5. To assess the potential for injury to Certificate 42114 due to the proposed use, an analysis was conducted using the Theis (1935) equation for drawdown in a confined aquifer. Hydraulic parameters used for the analysis were derived from regional data and studies (Pumping Test Reports, Conlon et al., 2003, 2005; Iverson, 2002; McFarland and Morgan, 1996; Woodward et al., 1998) or are within a typical range of values for the given parameter within the hydrogeologic regime (Freeze and Cherry, 1979; Domenico and Mifflin, 1965). The applicant has noted in the Application that they have also submitted a Groundwater Registration Modification application (GR-MOD T-13221) which proposes to change the POA for Groundwater Registration GR-3351 to POA 1-5 as identified in this application. Per proposed GR-MOD T-13221, POA 1-5 would pump up to 0.25 cfs under GR-3351, in addition to the 0.45 cfs requested in this application. Therefore, the analysis used a combined rate of 0.7 cfs (~314 gpm) to assess potential injury to nearby senior users. Results indicate that the proposed use is not likely to interfere with MARI 143 such that a senior groundwater user would be prevented from receiving water to which they are legally entitled (see Theis Drawdown Analysis, attached).

Hydrographs of water levels in the nearby alluvial aquifer system over the past two decades do not indicate widespread or persistent declines (see Hydrograph - Spring, attached). However, there do appear to be substantial (~30 ft or more) seasonal fluctuations in water level based on observations from a nearby State Observation Well (see Hydrograph – MARI 308, attached). Additionally, well completion statistics from the area indicate slight trends of deeper well completions and lower initial reported static water levels over time (see Well Completion Statistics, attached). While there is not sufficient evidence

C. GROUNDWATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. 690-09-040 (1): Evaluation of aquifer confinement:

Well	Aquifer or Proposed Aquifer	Confined	Unconfined
1 – 5	Alluvium	\boxtimes	

Basis for aquifer confinement evaluation: <u>Reported static water level in MARI 68155 was greater than 80 ft above the noted</u> water-bearing zone, indicating confined conditions. Well completion statistics from this area indicate that most completed wells have initial reported static water levels above the first noted water-bearing zone, also indicating confined conditions (see Well Completion Statistics, attached). Based on the available evidence, the aquifer appears to be confined in this area.

C2. **690-09-040** (2) (3): Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¹/₄ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	GW Elev ft msl	SW Elev ft msl	Distance (ft)	Hydraulically Connected? YES NO ASSUMED	Potential for Subst. Interfer. Assumed? YES NO
1 – 5	1	Willamette River	~100-150	~63	~3,250 - 3,880		
1 – 5	2	Deer Creek	~100-150	~169-157	~2,840 - 3,510		

Basis for aquifer hydraulic connection evaluation: Water table maps of this area indicate that groundwater in the alluvial aquifer system is flowing toward and discharging into the Willamette River (SW 1) to the northwest of the proposed POA/POU (Woodward et al, 1998), an interpretation which is supported by the higher measured static groundwater elevations relative to the estimated surface water elevation for SW 1. SW 1 near this location may have incised into the water-bearing zone tapped by proposed POA 1 (MARI 68155) and which would be tapped by proposed POA 2-5. Based on the available evidence, the alluvial aquifer system in this area is hydraulically connected to SW 1 (Willamette River).

The proposed POA are also within 1 mile of Deer Creek (SW 2). Water table maps of this area indicate that static groundwater elevations in the alluvial aquifer system near SW 2 are within ~10 ft of the surface water elevations estimated for SW 2 (Woodward et al, 1998). Alluvial groundwater near SW 2 flows down-gradient to the northwest, through the area of the proposed POA, and into the Willamette River (SW 1). Although the reported static water elevation for proposed POA 1 (MARI 68155) is greater than 40 ft below the surface water elevations estimated for SW 2, the measurement reported for MARI 68155 was collected in August, when groundwater levels are anticipated to be temporarily depressed due to increased pumping and decreased recharge (see Hydrograph – MARI 308, attached). The preponderance of evidence indicates that SW 2 (Deer Creek) is hydraulically connected to the alluvial aquifer system.

Water Availability Basin the well(s) are located within: SW 1: WILLAMETTE R > COLUMBIA R - AB MOLALLA R SW 2: MILL CR > PUDDING R - AT MOUTH

C3a. **690-09-040** (4): Evaluation of stream impacts for <u>each well</u> that has been determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that surface water source, and not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% *natural* flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked 🖾 box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < ¼ mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
1 – 5	1			MF182	1,500		3,830		>25%	\square
1 – 5	2						1.88	\square	<<25%	\square

C3b. **690-09-040 (4):** Evaluation of stream impacts by total appropriation for all wells determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Complete only if Q is distributed among wells. Otherwise same evaluation and limitations apply as in C3a above.

SW #	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?

Comments: 3a: To assess the potential interference with surface water due to the proposed use, a stream depletion analysis was conducted using the Hunt (2003) analytical model. Hydraulic parameters used for the analysis were derived from regional data and studies (Pumping Test Reports, Conlon et al., 2003, 2005; Iverson, 2002; McFarland and Morgan, 1996; Woodward et al., 1998) or are within a typical range of values for the given parameter within the hydrogeologic regime (Freeze and Cherry, 1979; Domenico and Mifflin, 1965). Results of the analysis indicate that the proposed use will primarily impact SW 1 (Willamette River), with depletions of SW 1 most likely exceeding 25 percent of the rate of well discharge within 30 days of continuous use (see Stream Depletion Analysis, attached). The high relative rate of stream depletion is attributed primarily to the small intervening thickness of fine-grained sediments between the alluvial aquifer system and SW 1 (Willamette River) (i.e. a highly efficient hydraulic connection) and the confined nature of the alluvial aquifer. **Per OAR 690-009-0040(4)(d), the proposed use is assumed to have the potential to cause substantial interference (PSI) with SW 1 (Willamette River).**

Additionally, the maximum rate of withdrawal under the proposed use (0.45 cfs) is greater than 1 percent (0.0188 cfs) of the natural streamflow that is equaled or exceeded 80 percent of time (1.88 cfs) for SW 2 (Deer Creek). Per OAR 690-009-0040(4)(c), the proposed use is assumed to have PSI with SW 2 (Deer Creek).

C4a. **690-09-040 (5):** Estimated impacts on **hydraulically connected surface water sources greater than one mile** as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

Non-Di	stributed	Wells											
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
Interfere	ence CFS												
Distrib	uted Well	s											
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
Interfere	ence CFS												
(4)	4.1 .						-						
. ,	tal Interf.												
(B) = 80	% Nat. Q												
(C) = 1 ^c	% Nat. Q												
(D) = ($\lambda > (C)$												
	$\mathbf{A}) > (\mathbf{C})$										V	V	*
$(\mathbf{E}) = (\mathbf{A} / \mathbf{A})$	/ B) x 100	%	%	%	%	%	%	%	%	%	%	%	%

(A) = total interference as CFS; (B) = WAB calculated natural flow at 80% exceed. as CFS; (C) = 1% of calculated natural flow at 80% exceed. as CFS; (D) = highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage.
 Basis for impact evaluation: N/A

C4b. 690-09-040 (5) (b) The potential to impair or detrimentally affect the public interest is to be determined by the Water Rights Section.

C5. **If properly conditioned**, the surface water source(s) can be adequately protected from interference, and/or groundwater use under this permit can be regulated if it is found to substantially interfere with surface water:

i. \Box The permit should contain condition #(s)

ii. The permit should contain special condition(s) as indicated in "Remarks" below;

C6. SW / GW Remarks and Conditions:

References Used:

Application File: G-18840

Transfer File: T-13029

Certificate: 42114, 93743

Groundwater Claim: GR-3351

Groundwater Registration Modification File: T-13221

Pumping Test Reports: MARI 154, 160, 163, 172, 250, 348, 350, 358, 363, 53183, 53448, 54523

- Conlon, T.D., Lee, K.K., and Risley, J.R., 2003, Heat tracing in streams in the central Willamette Basin, Oregon, in Stonestrom, D.A. and Constantz, Jim, eds., Heat as a tool for studying the movement of groundwater near streams: U.S. Geological Survey Circular 1260, chapter 5, p. 29-34.
- Conlon, T.D., Wozniak, K.C., Woodcock, D., Herrera, N.B., Fisher, B.J., Morgan, D.S., Lee, K.K., and Hinkle, S.R., 2005, Groundwater hydrology of the Willamette Basin, Oregon, Scientific Investigations Report 2005-5168: U. S. Geological Survey, Reston, VA.
- Domenico, P.A. and Mifflin, 1965, Water from low-permeability sediments and land subsidence: Water Resource Research, v. 1, no. 4, p. 563-576.

Freeze, R.A. and Cherry, J.A., 1979, Groundwater, Prentice Hall, Englewood Cliffs, New Jersey, 604 p.

- Gannett, M.W. and Caldwell, R., 1998, Geologic framework of the Willamette Lowland aquifer system, Oregon and Washington, Professional Paper 1424-A, 32 p: U. S. Geological Survey, Reston, VA.
- Hunt, B., 2003, Unsteady stream depletion when pumping from semiconfined aquifer: Journal of Hydrologic Engineering, January/February, Vol 8, p. 12-19.
- Iverson, J., 2002, Investigation of the hydraulic, physical, and chemical buffering capacity of Missoula flood deposits for water quality and supply in the Willamette Valley of Oregon: Unpublished M.S. thesis, Oregon State University, 147 p.
- McFarland, W.D., and Morgan, D.S., 1996, Description of the Ground-Water Flow System in the Portland Basin, Oregon and Washington, Water Supply Paper 2470-A, 58 p: U. S. Geological Survey, Reston, VA.
- Theis, C.V., 1935. The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using groundwater storage, American Geophysical Union Transactions, vol. 16, p. 519-524.
- United States Geological Survey, 2017, Sherwood quadrangle, Oregon [map], 1:24,000, 7.5 minute topographic series, U.S. Department of the Interior, Reston, Virginia.
- Watershed Sciences, 2009, LIDAR remote sensing data collection, Department of Geology and Mineral Industries: Portland, OR, May 27.

Woodward, D.G., Gannett, M.W., and Vaccaro, J.J., 1998, Hydrogeologic framework of the Willamette Lowland aquifer system, Oregon and Washington: U.S. Geological Survey Professional Paper 1424-B, 82 p.

D. WELL CONSTRUCTION, OAR 690-200

D1. Well #: _____ Logid: _____

D2. THE WELL does not appear to meet current well construction standards based upon:

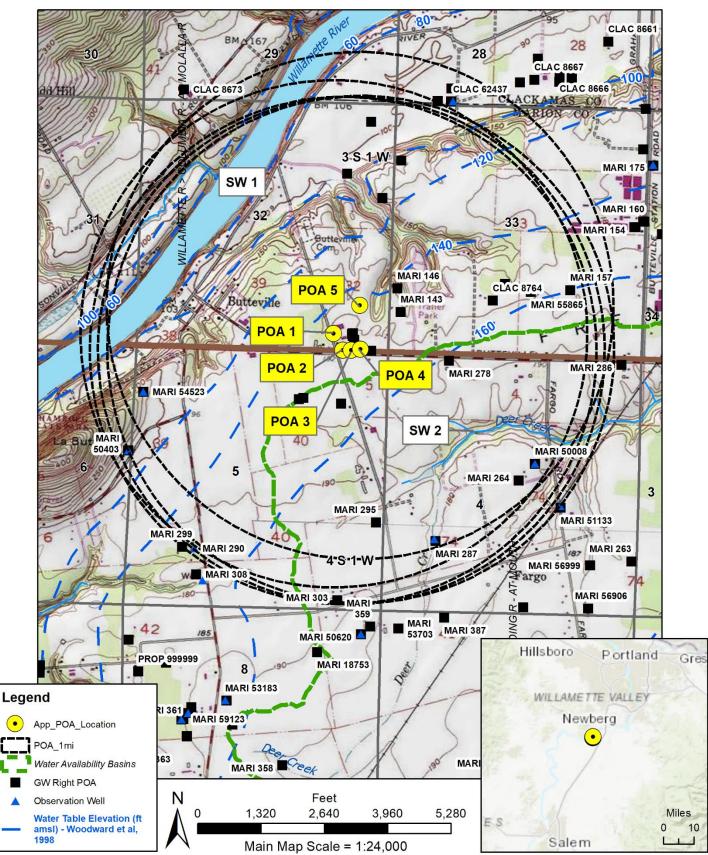
- a. \Box review of the well log;
- b. _____ field inspection by ______
- c. report of CWRE
- d. other: (specify)

D3. THE WELL construction deficiency or other comment is described as follows:

D4.
 Route to the Well Construction and Compliance Section for a review of existing well construction.

Well Location Map

G-18840 Mayfield Farms, LLC

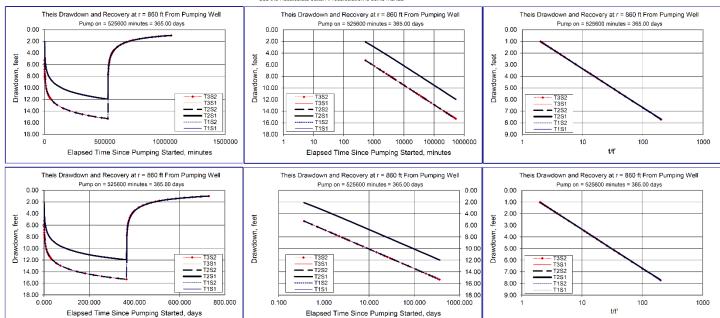


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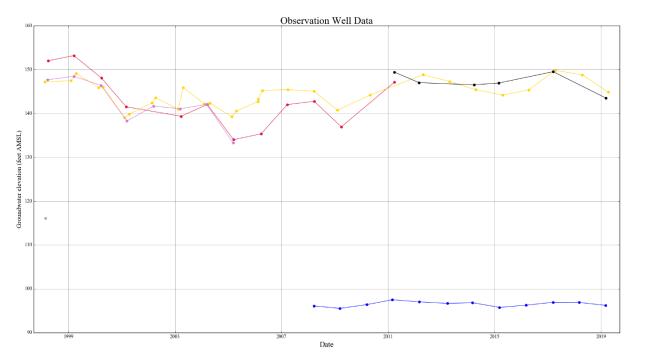
 Theis Time-Drawdown Worksheet
 v.3.00

 Calculates Theis nonequilibrium drawdown and recovery at any arbitrary radial distance, r, from a pumping well for 3 different T values and
 radial distance, r, from a pumping well for 3 different T values and 2 different S values Written by Karl C. Wozniak September 1992. Last modified December 30, 2014

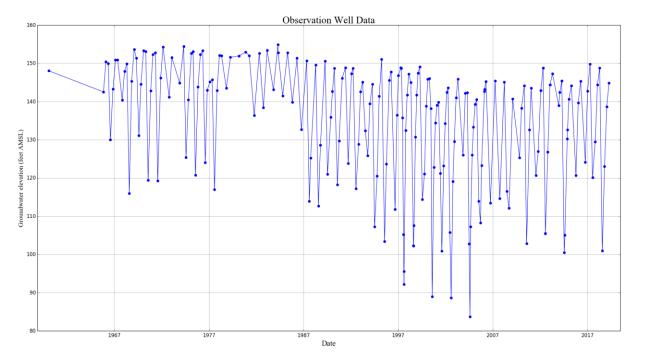
Input Data:	Var Name	Scenario 1	Scenario 2	Scenario 3	Units	
Total pumping time	t		365		d	
Radial distance from pumped well:	r		860.00		ft	Q conversions
Pumping rate	Q		314.0		gpm	314.00 gpm
Hydraulic conductivity	K	66.000	66.000	66.000	ft/day	0.70 cfs
Aquifer thickness	b		50		ft	41.98 cfm
Storativity	S_1		0.00100			60,449.20 cfd
	S_2		0.00010			1.39 af/d
Transmissivity Conversions	T_f2pd	3,300	3,300	3,300	ft2/day	
	T_ft2pm	2.2917	2.2917	2.2917	ft2/min]
	T_gpdpft	24,684	24,684	24,684	gpd/ft]
-				Use the Recalcu	late button if reca	culation is set to manual



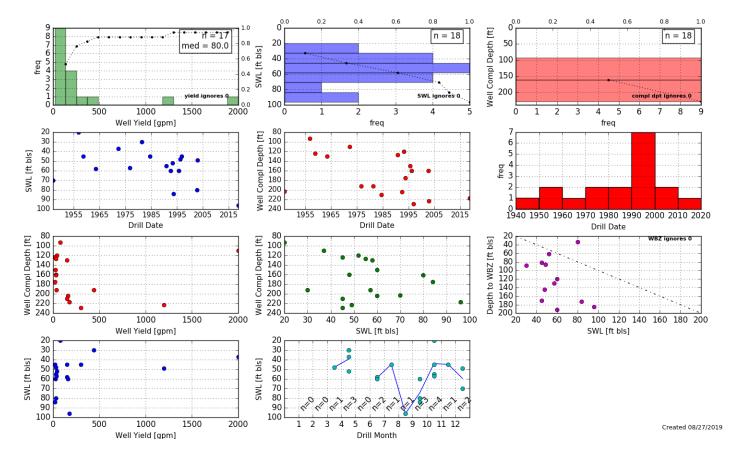
Hydrograph - Spring



Hydrograph – MARI 308



Well Completion Statistics - 3S/1W-32 & 33, 4S/1W-3 & 4



••• MARI 308

		D	etailed Reports			
		WILLAMETTE	R > COLUMBIA R - AB N WILLAMETTE BASIN	IOLALLA R		
		Wate	r Availability as of 8/27/20	19		
/atershe	d ID #: 182 (Map)				Exceedance	e Level: 80%
ate: 8/27	7/2019					Time: 1:36 P
Water	Availability Calculation	Consumptive Uses and S	itorages Instream	Flow Requirements	Reserva	tions
	Wa	ter Rights		Watershed C	haracteristics	
		Annual Volun	eamflow in Cubic Feet pe ne at 50% Exceedance in	Acre-Feet		
		mptive Uses and Storages Exp			Flow Requirement Ne	
JAN	21,400.00	2,300.00	19,100.00	0.00	1,500.00	17,600
FEB	23,200.00	7,490.00	15,700.00	0.00	1,500.00	14,200
MAR	22,400.00	7,260.00	15,100.00	0.00	1,500.00	13,600
APR MAY	19,900.00 16,600.00	6,920.00 4,260.00	13,000.00 12,300.00	0.00	1,500.00 1,500.00	11,500 10,800
JUN	8,740.00	1,980.00	6,760.00	0.00	1,500.00	5,260
JUL	4,980.00	1,810.00	3,170.00	0.00	1,500.00	1,670
AUG	3,830.00	1,650.00	2,180.00	0.00	1,500.00	677
SEP	3,890.00	1,400.00	2,490.00	0.00	1,500.00	992
ост	4,850.00	758.00	4,090.00	0.00	1,500.00	2,590
VOV	10,200.00	891.00	9,310.00	0.00	1,500.00	7,810
DEC	19,300.00	973.00	18,300.00	0.00	1,500.00	16,800
ANN	15,200,000.00	2,250,000.00	13,000,000.00	0.00	1,090,000.00	11,900,000
			vailability Ar etailed Reports	nalysis		
			R > PUDDING R - AT MOU WILLAMETTE BASIN	JTH		
		Water	Availability as of 8/27/201	19		
	d ID #: 30200901 <u>(Map)</u>				Exceedance	Level: 80% ~
atershee						Time: 1:36 PN

Water Availability Calculation

Monthly Streamflow in Cubic Feet per Second Annual Volume at 50% Exceedance in Acre-Feet

Month	Natural Stream Flow	Consumptive Uses and Storages	Expected Stream Flow	Reserved Stream Flow	Instream Flow Requirement	Net Water Available
JAN	39.20	9.74	29.50	0.00	0.00	29.50
FEB	53.90	9.89	44.00	0.00	0.00	44.00
MAR	38.40	9.47	28.90	0.00	0.00	28.90
APR	27.60	7.09	20.50	0.00	0.00	20.50
MAY	13.70	5.70	8.00	0.00	0.00	8.00
JUN	8.72	7.01	1.71	0.00	0.00	1.71
JUL	3.79	10.80	-6.96	0.00	0.00	-6.96
AUG	2.09	8.74	-6.65	0.00	0.00	-6.65
SEP	1.88	4.78	-2.90	0.00	0.00	-2.90
OCT	2.39	1.25	1.14	0.00	0.00	1.14
NOV	6.05	7.23	-1.18	0.00	0.00	-1.18
DEC	25.90	9.57	16.30	0.00	0.00	16.30
ANN	30,000.00	5,500.00	25,300.00	0.00	0.00	25,300.00

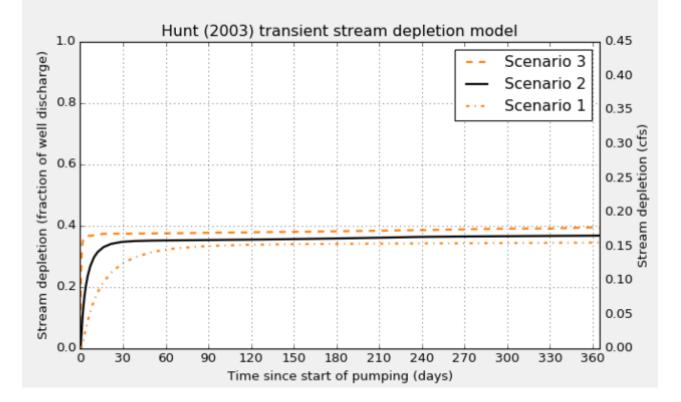
Stream Depletion Analysis – SW 1 (Willamette River)

Application type:	G
Application number:	18840
Well number:	1
Stream Number:	1
Pumping rate (cfs):	0.45
Pumping duration (days):	365.0
Pumping start month number (3=March)	1.0

Parameter	Symbol	Scenario 1	Scenario 2	Scenario 3	Units
Distance from well to stream	а	3880.0	3565	3250	ft
Aquifer transmissivity	Т	2000	3300.0	4300.0	ft2/day
Aquifer storativity	S	0.001	0.0005	0.0001	-
Aquitard vertical hydraulic conductivity	Kva	0.003	0.005	0.01	ft/day
Aquitard saturated thickness	ba	120.0	120.0	120.0	ft
Aquitard thickness below stream	babs	4.0	4.0	4.0	ft
Aquitard specific yield	Sya	0.2	0.2	0.2	-
Stream width	WS	650.0	650.0	650.0	ft

Stream d	leplet	tion f	or S	cenario	2:

Days	10	30	60	90	120	150	180	210	240	270	300	330	360
Depletion (%)	30	35	35	35	35	36	36	36	36	36	37	37	37
Depletion (cfs)	0.13	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.17



Stream Depletion Analysis – SW 2 (Deer Creek)

Application type:	G
Application number:	18840
Well number:	1
Stream Number:	2
Pumping rate (cfs):	0.45
Pumping duration (days):	365.0
Pumping start month number (3=March)	1.0

Parameter	Symbol	Scenario 1	Scenario 2	Scenario 3	Units	
Distance from well to stream	а	2840	2840	2840	ft	
Aquifer transmissivity	т	500.0	3300.0	4300.0	ft2/day	
Aquifer storativity	S	0.001	0.0003	0.0001	-	
Aquitard vertical hydraulic conductivity	Kva	0.01	0.005	0.001	ft/day	
Aquitard saturated thickness	ba	140.0	140.0	140.0	ft	
Aquitard thickness below stream	babs	140.0	140.0	140.0	ft	
Aquitard specific yield	Sya	0.2	0.2	0.2	-	
Stream width	WS	10.0	10.0	10.0	ft	

Stream depletion for Scenario 2:

Days	10	30	60	90	120	150	180	210	240	270	300	330	360
Depletion (%)	0	0	0	0	0	0	0	0	0	0	0	0	0
Depletion (cfs)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

