| -  |  |                |           |              |                |                               |            |
|--|--|----------------|-----------|--------------|----------------|-------------------------------|------------|
| Name OR Dept. of Fish & Wildlife<br>By Randy Fisher, Director<br>Address PO Box 59 or 2901 SW First Avenue<br>Portland, OR 97207 | Applicat<br>Per<br>Certifica<br>Strear | tion No        | FW        | Date<br><br> | FEES I<br>Amou | PAID<br>int F<br>Fee<br>UNDEI | eceipt No. |
| Date filedMarch.21, 1990   |  |                |           | Date         | Amou           | int C                         | neck No.   |
| Priority<br>Action suspended until   | Date                                   | ASS<br>To Whom | SIGNMENTS | Address      |                | Volume                        | Page       |
| Return to applicant  |  |                | -         |              | ••••           |                               |            |
| Date of approval   |  |                |           |              |                |                               |            |
| CONSTRUCTION   |  |                | REMARKS   |              |                |                               |            |
| Date for beginning   |  |                |           |              |                |                               |            |
| Date for completion  |  |                |           |              |                |                               |            |
| Extended to  |  |                |           |              |                |                               |            |
| Date for application of water  |  |                |           |              |                |                               |            |
| Extended to  |  |                |           |              |                |                               |            |
|  |  |                |           |              |                |                               |            |
| PROSECUTION OF WORK  |  |                |           |              |                |                               |            |
| Form "A" filed   |  |                |           |              |                |                               |            |
| Form "B" filed   |  |                |           | ••••••       | ••••••         |                               |            |
| Form "C" filed   |  |                |           |              |                | ••••••                        |            |
| FINAL PROOF  |  |                |           |              |                |                               |            |
| Blank mailed   |  |                |           |              |                |                               |            |
| Proof received   |  |                |           |              |                |                               |            |
| Date certificate issued  |  |                |           |              |                |                               |            |

INST

-

SP\*70900-119

1025 Certificate No. Instream Apolication No - N STATE OF OREGON 12821 1993 WATER RESOURCES DEPARTMENT Application for Instream Water Right OREGC ti .eeu oldud to vien by a State Agency TR-AR There is no fee required for this application. A. Applicant: \_\_\_\_\_ Randy Fisher \_\_\_\_\_ for Oregon Dept. of Fish & Wildlife (Agency) (Director) Mailing Address: 2501 S.W. First Ave., P. O. Box 59 229-5400 Ext. 438 97207 OR Portland State Phone No. Zip City for \_\_\_\_\_ B. Applicant: (Agency) (Director) Mailing Address: \_ Zp Phone No. State City

| C. Applicant:    | for      |
|------------------|----------|
| (Director)       | (Agency) |
| Mailing Address: |          |

State

Zip

Phone No.

a tributary or source (if lake) of \_\_\_\_\_\_ John Day River\_\_\_\_\_\_

City

2. The public use(s) this instream water right is based upon include:

Upstream passage of adult and juvenile fish including summer steelhead and resident rainbow trout.

Instream Application No. \_

7025

Certificate No. \_

3. The amount of water needed by month and/or year for each category of public use. If more space is needed, use a separate sheet of paper.

| List      | quantiti | ies in ei | ther c | fs, acr | e-feet, o | r lake | elevati  | on abo     | ve Mea     | an Sea | Level   | 31 5%  |
|-----------|----------|-----------|--------|---------|-----------|--------|----------|------------|------------|--------|---------|--------|
| Use(s)    | Jan      | Feb       | Mar    | Apr     | May       | Jun    | Jul      | Aug        | Sept       | Oct    | Nov     | Dec    |
| Migration | of Anac  | iromous   | fish   | and r   | esident   | fish   | vo en en | e bipo i v | all starts |        | •       |        |
|           |          |           |        |         |           |        |          | Chi and    |            |        | WIRE T  |        |
|           | 34       | 57        | 57     | 57      | 57        | 34     | 34       | 34         | 34         | 34     | 34      | 34     |
|           |          | - Stand P | 1      |         |           |        |          | PARA       | 1          |        |         |        |
|           |          |           |        |         |           |        |          |            |            |        |         | -      |
|           |          |           |        |         |           |        |          |            |            | 82910  | OV CIUT | 1.24.1 |
| ·         |          |           |        | 1000    |           |        |          | -          |            |        |         |        |
|           |          |           |        |         |           |        | -        |            |            |        |         |        |

4. The reach of the stream identified for an instream water right is from the:

| upstream end at        | USGS Guaging  | station     | @ White | Park (Statio                           | on #14047390) |
|------------------------|---------------|-------------|---------|--|---------------|
| River Mile (if known   | ) _RM 40.0    |             |         |  |               |
| within the <u>NE</u>   | _ 1/4 of the  | SW          | 1/4 of  |  |               |
| Section36              | _ Township _  | 3S          | Ra      | nge22                                  | 2E W.M.,      |
| CountyGillia           | m             |             |         |  |               |
|                        |               |             |         | · ···································· |               |
| downstream end a       | atThe_m       | outh        |         |  |               |
| River Mile (if known)  | 0.0           |             |         |  |               |
| within theNE           | 1/4 of the    | SW          | 1/4 of  |  |               |
| Section                | _ Township _  | 1N          | Ran     | nge198                                 | W.M.,         |
| CountyGilli            | am            |             |         | mithad                                 | 1             |
| Lake identified for ar | instream wate | er right is |         | allound                                | 'ly           |
| within the             | 1/4 of the    |             | 1/4 of  | Rech 635                               | -             |
| Section                | Township _    |             | Rai     | 400-015                                | (9) V.M.,     |
| County                 |               | <u> </u>    |         | nu                                     | 1             |
|                        |               |             |         |  |               |

5. Method(s) used to determine the requested amounts: <u>Flow required to operate proposed fish passage facilities during migration</u> <u>period for adults and juveniles.</u> <u>Required flows are based on engineering determinations</u> <u>using USGS data and passage facility design.</u> Instream Application No. \_

Certificate No.

6. When were the following state agencies notified of the intent to file for the instream water right?

Department of Environmental Quality D Department of Fish and Wildlife D Parks and Recreation Division D

0251

| Date | 2-7-90 |   |  |
|------|--------|---|--|
| Date |        |   |  |
| Date | 2-7-90 | i min vinion of a su  |  |
|      |        | and the second se |  |

7. If possible, include recommendations for measuring locations or methods:

Measure @ USGS station 14047390 and by staff gauge @ the mouth RM 0.0

 If possible, include recommendations for assisting the Water Resources Department (WRD) in measuring and monitoring procedures:

Local watermaster will measure w/ periodic assistance from ODEW. Monitoring plan to be developed.

 If possible, include other recommendations for methods or conditions necessary for managing the water right to protect the public uses (see OAR 690-77-020 (5)(c)): Monitoring plan to be developed.

Remarks: <u>The Department of Fish and Wildlife is aggressively persuing the</u> <u>completion of a series of passage facilities at eight existing irrigation diversion</u> <u>structures. Once adult steelhead have access to the upper reaches of Rock Creek</u> <u>we expect an annual return of 1000 adults. Upstream passage of juvenile fish will be</u> a critical component of the passage facilities function.

This application must be accompanied by a basin map with the applicable lake or stream reach identified.

An instream water right may be allowed for an instream beneficial use of water subject to existing water rights with an effective date prior to the filing date of this application.

This type of beneficial use is for the benefit of the public and a certificate issued confirming an instream water right shall be held in trust by the Water Resources Department for the people of the State of Oregon, pursuant to ORS 537.341.

3/21/90 Date

Oregon Dept. of Fish & Wildlife Agency

Mancy M. Machush Signature

Assistant Director Title

| Instrume Acator is Al                             | 20251   | Company A marine  |
|---|---|---|
| Instream Application No.                          |   | Certificate No  |
|   | Date  | doint?<br>Department of Environmental Quality                                   |
| This is to certify ting maps and da               | that I have examined the fore<br>ta, and return them for: | going application, together with the accompany-                                 |
|   | abadian na anita. I palaga                                | win tot en utolitie managen obukeni jeldiset ett. "T                            |
| In order to retain<br>Department with             | n its priority, this application corrections on or before | on must be returned to the Water Resources, 19                                  |
| Date:   | , 19  |   |
|   |   | Water Resources Department  |
|   |   | Title   |
|   |   |   |
|   |   |   |
| · · ·   |   | Auntone Auntone A   |
|   |   |   |
|   |   |   |
| This document wa<br>the <u>21<sup>51</sup></u> da | as first received at the Water<br>ay of                   | Resources Department in Salem, Oregon, on _, 19 $20$ , at $2:50$ o'clock $2$ M. |
|   |   |   |
|   |   |   |
|   | WATER RESOURCE<br>3850 Portian<br>SALEM, OREC             | S DEPARTINE<br>d Road NE<br>SON 97310   |

Date: November 25, 1995

## **OREGON WATER RESOURCES DEPARTMENT**

SATISFACTORY REPORT OF TECHNICAL REVIEW

#### FOR AN INSTREAM WATER RIGHT APPLICATION

OBJECTIONS TO THE PROPOSED WATER INSTREAM WATER RIGHT TECHNICAL REVIEW REPORT, AS DESCRIBED BELOW, MUST BE RECEIVED IN WRITING BY THE OREGON WATER RESOURCES DEPARTMENT, 158 12th ST NE, SALEM, OREGON 97310, ON OR BEFORE 5 PM: February 1, 1995

1. APPLICATION FILE NUMBER - IS 70251

2. APPLICATION INFORMATION

Application name/address/phone:

Oregon Department of Fish and Wildlife P.O. Box 59 Portland, Oregon 97207 503-229-5400

Date application received for filing and/or tentative date of priority: 3/21/1990

Source: ROCK CR tributary to JOHN DAY R

County: GILLIAM

Purpose: UPSTREAM PASSAGE OF ADULT AND JUVENILE FISH INCLUDING SUMMER STEELHEAD AND RESIDENT RAINBOW TROUT.

The amount of water (in cubic feet per second) requested by month:

JANFEBMARAPRMAYJUNJULAUGSEPOCTNOVDEC1st1/234.057.057.057.034.034.034.034.034.034.034.034.034.02nd1/234.057.057.057.057.034.034.034.034.034.034.034.034.0

To be maintained in:

ROCK CREEK FROM USGS GAGING STATION AT WHITE PARK RM 40.0 (NESW, SECTION 36, T3S, R22E); TO THE MOUTH OF ROCK CREEK RM 0.0 (NESW, SECTION 11, T1N, R19E)

#### 3. TECHNICAL REVIEW

The application is complete and free of defects.

The proposed use is not restricted or prohibited by statute.

The following supporting data has been submitted by the applicant:

- (a) Fish and Wildlife Resources of the John Day Basin, Oregon, and Their Water Requirements; September, 1979.
- (b) Determining Minimum Flow Requirements for Fish, ODFW Report January 20, 1984.
- (c) Developing and Application of Spawning Velocity and Depth Criteria for Oregon Salmonids, Alan K. Smith, Transactions of the American Fisheries Society, April 1973.
- (d) Determining Stream Flows for Fish Life, Oregon State Game Commission Report, March 1972.

An assessment with respect to conditions previously imposed on other instream water rights granted for the same source has been completed.

An assessment with respect to other Commission administrative rules, including but not limited to the applicable basin program has been completed.

An evaluation of the information received from the local government(s) regarding the compatibility of the proposed instream water use with land use plans and regulations has been completed.

The level of instream flow requested is based on the methods of determining instream flow needs that have been approved administrative rule of the agency submitting this application.

The evaluation of the estimated average natural flow available from the proposed source during the time(s) and in the amounts requested in the application is described below. The recommended flows take into consideration planned uses and reasonably anticipated future demands for water from the source for agricultural and other uses as required by the standards for public interest review:

|                                 | JAN  | FEB  | MAR  | APR  | MAY  | JUN  | JUL  | AUG  | SEP  | OCT  | NOV  | DEC            |
|---------------------------------|------|------|------|------|------|------|------|------|------|------|------|----------------|
| 1sty                            | 34.0 | 57.0 | 57.0 | 57.0 | 57.0 | 34.0 | 34.0 | 34.0 | 34.0 | 34.0 | 34.0 | 34.0           |
| 2nd <sup>1</sup> <sub>2</sub>   | 34.0 | 57.0 | 57.0 | 57.0 | 57.0 | 34.0 | 34.0 | 34.0 | 34.0 | 34.0 | 34.0 | 34.0 REQUESTED |
|                                 | 36.0 | 77.7 | 125  | 116  | 32.0 | 11.0 | 4.7  | 3.09 | 2.47 | 2.72 | 6.67 | 21.8 AVG FLOW  |
| 1st1/2                          | 35.0 | 35.0 | 50.0 | 50.0 | 50.0 | 35.0 | 20.0 | 10.0 | 10.0 | 10.0 | 20.0 | 35.0           |
| 2nd <sup>1</sup> / <sub>2</sub> | 35.0 | 50.0 | 50.0 | 50.0 | 50.0 | 35.0 | 10.0 | 10.0 | 10.0 | 10.0 | 20.0 | 35.0 MIN FLOW  |

### 4. REPORT CONCLUSIONS

The proposed water use, as conditioned, passed this technical review. The information contained in the application along with the supporting data submitted by the applicant indicate that the flow levels set out in this report are necessary to protect the public use.

The supporting data states that the recommended flows are necessary to meet the biological requirements for spawning and rearing of salmonids and resident game fish. Consideration of habitat type, stream depth and water velocity were considered by the applicant in development of the flow levels. (See Determining Minimum Flow Requirements for Fish, ODFW Report January 20, 1984.) The recommended flow volumes are necessary to ensure appropriate levels of dissolved oxygen, turbidity, pH and temperature.

The listed flows would provide desirable levels of natural fish production for fishery management purposes.

#### 5. PROPOSED CERTIFICATE CONDITIONS

[The following proposed conditions will apply to water use and will appear on the face of the certificate.]

 The right is limited to not more than the amounts, in cubic feet per second, during the time periods listed below:

| JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG  | SEP  | OCT  | NOV  | DEC  |
|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|------|
| 34  | 57  | 57  | 57  | 32  | 11  | 4.7 | 3.09 | 2.47 | 2.72 | 6.67 | 21.8 |

- The water right holder shall measure and report the in-stream flow along the reach of the stream or river described in the certificate as may be required by the standards for in-stream water right reporting of the Water Resources Commission.
- This instream right shall not apply to permits for appropriation for domestic or livestock use or to use of water legally stored or legally released from storage.
- The instream flow allocated pursuant to this water right is not in addition to other instream flows created by a prior water right or designated minimum perennial stream flow.



## Oregon Water Resources Department Water Rights/Adjudication Section

Water Right Application Number: IS 70251

1-12

#### Proposed Final Order

Summary of Recommendation: The Department recommends that the attached draft certificate be issued with conditions.

#### Application History

On 3/21/90, the Oregon Department of Fish and Wildlife submitted an application to the Department for the following instream water right certificate.

Source: ROCK CR tributary to JOHN DAY R

County: GILLIAM

Purpose: UPSTREAM PASSAGE OF ADULT AND JUVENILE FISH INCLUDING SUMMER STEELHEAD AND RESIDENT RAINBOW TROUT

The amount of water (in cubic feet per second) requested by month:

JANFEBMARAPRMAYJUNJULAUGSEPOCTNOVDEC1st½34.057.057.057.034.034.034.034.034.034.034.02nd½34.057.057.057.034.034.034.034.034.034.034.034.0

To be maintained in:

ROCK CREEK FROM USGS GAGING STATION AT WHITE PARK RM 40.0 (NESW, SECTION 36, T3S, R22E); TO THE MOUTH OF ROCK CREEK RM 0.0 (NESW, SECTION 11, T1N, R19E)

The Department mailed the applicant notice of its Technical Review on November 25, 1995, determining that the requested flows exceeded the estimated average natural flow during some months but that flows at a reduced amount, with exceptions for human and livestock consumption, are appropriate. The objection period closed February 1, 1995. Objections and comments were received (from A DAVID CHILDS, OREGON DEPT OF FISH AND WILDLIFE, WATER FOR LIFE, WATERWATCH OF OREGON).

The following supporting data was submitted by the applicant:

- Engineering determined by using USGS data and passage facility design.
- (b) A letter dated April 5, 1996, stating that the flows requested in this application are the minimum amount necessary to restore, protect and enhance populations and habitats of native wildlife species at self-sustaining levels

In reviewing applications, the Department may consider any relevant sources of information, including the following:

- comments by or consultation with another state agency
- any applicable basin program
- any applicable comprehensive plan or zoning ordinance
- the amount of water available
- the proposed rate of use
- pending senior applications and existing water rights of record
- the Scenic Waterway requirements of ORS 390.835
- applicable statutes, administrative rules, and case law '
- any comments received

An assessment with respect to conditions previously imposed on other instream water rights granted for the same source has been completed.

An evaluation of the information received from the local government(s) regarding the compatibility of the proposed instream water use with land use plans and regulations has been completed.

The level of instream flow requested is based on the methods of determining instream flow needs that have been approved by administrative rule of the agency submitting this application.

#### Findings of Fact

The John Day Basin Program allows the proposed use.

Senior water rights exist on this source or on downstream waters.

The source of water is not above a State Scenic Waterway.

The source of water is not withdrawn from appropriation by order of the State Engineer or legislatively withdrawn by ORS 538.

The estimated average natural flow for the lower end of the requested reach is as follows (in cubic feet per second):

JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC 36.0 77.7 125 116 32.0 11.0 4.7 3.09 2.47 2.72 6.67 21.8

Water is NOT available for further appropriation (at a 50 percent exceedance probability) for the period May, June, July, August, September, October, November and December.

The flows available for further appropriation are shown below:

JANFEBMARAPRMAYJUNJULAUGSEPOCTNOVDEC35.8277.5123.8110.824.221.53-8.0-7.41-4.57-0.436.482L62

#### Conclusions of Law

· · · · · ·

Under the provisions of ORS 537.153, the Department must

presume that a proposed use will not impair or be detrimental to the public interest if the proposed use is allowed in the applicable basin program established pursuant to ORS 536.300 and 536.340 or given a preference under ORS 536.310(12), if water is available, if the proposed use will not injure other water rights and if the proposed use complied with rules of the Water Resources Commission.

The proposed use requested in this application is allowed in the John Day Basin Plan.

No preference for this use is granted under the provisions of ORS 536.310(12).

The proposed use will not injure other water rights.

The proposed use complies with rules of the Water Resources Commission.

The proposed use complies with the State Agency Agreement for land use.

The proposed instream flows do not fully appropriate this source of water year round. Water is available for additional storage.

While the proposed use meets the other tests, the full amount of water requested is not available during some months of the year.

Water is not available for the proposed use at the amount requested during May, June, July, August, September, October, November and December because the unappropriated water available is less than the amounts requested during these months.

For these reasons, the presumption set forth in ORS 537.153, as discussed above, has not been established. The application therefore has been processed without the statutory presumption.

"When instream water rights are set at levels which exceed current unappropriated water available the water right not only protects remaining supplies from future appropriation but establishes a management objective for achieving the amounts of instream flows necessary to support the identified public uses." OAR 690-77-015(2).

"The amount of appropriation for out-of-stream purposes shall not be a factor in determining the amount of an instream water right." "The amount allowed during any time period for the water right shall not exceed the estimated average natural flow ..." (excerpted from OAR 690-77-015 (3) and (4)).

Because the proposed use exceeds the available water, it can not be presumed to be in the public interest. However, under the direction of OAR 690-77-015 (2)(3) and(4), the proposed use is in the public interest up to the limits of the estimated average natural flow.

Oregon law allows certain uses of water to take precedence over other uses in certain circumstances. When proposed uses of water are insufficient for all who desire to use them, preference shall be given to human consumption purposes over all other uses and for livestock consumption over any other use (excerpted from ORS 536.310 (12)).

The Department therefore concludes that

- the proposed use, as limited in the draft certificate, will not result in injury to other water rights,
- the proposed use, as limited in the draft certificate, will not impair or be detrimental to the public interest as provided in ORS 537.170.
- the proposed use, as limited in the draft certificate, for purposes of water distribution, this instream right shall not have priority over human or livestock consumption.
- the flows are to be measured at the lower end of the stream reach to protect necessary flows throughout the reach.
- the stream flows listed below represent the minimum flows necessary to support the public use.

N JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC taken from IR 34 57 57 57 57 57 11 4.7 3.09 2.47 2.72 6.67 21.8-taken from IR N 1996 37.50 74.20 120 120 124 39.5 14 3.13 1.56 1.61 2.74 8.92 20.60 new 50% exceedence

The Department recommends that the attached draft certificate be issued with conditions.

DATED AUGUST 20, 1996

Steven P. Applegate Administrator Water Rights and Adjudications Division

#### Protest Rights

Under the provisions of ORS 537.153(6) or 537.621(7), you have the right to submit a protest against this proposed final order. Your protest must be in writing, and must include the following:

- Your name, address, and telephone number;
- A description of your interest in the proposed final order, and, if you claim to represent the public interest, a precise statement of the public interest represented;
- A detailed description of how the action proposed in this proposed final order would impair or be detrimental to your interest;
- A detailed description of how the proposed final order is in error or deficient, and how to correct the alleged error or deficiency;

- Any citation of legal authority to support your protest, if known; and
- If you are not the applicant, the \$200 protest fee required by ORS 536.050.
- Proof of service of the protest upon the applicant.

· · · ·

Your protest must be received in the Water Resources Department no later than October 4, 1996.

After the protest period has ended, the Director will either issue a final order or schedule a contested case hearing. The contested case hearing will be scheduled *only* if a protest has been submitted *and* if

- upon review of the issues the director finds that there are significant disputes related to the proposed use of water, or
- the applicant requests a contested case hearing within 30 days after the close of the protest period.

#### DRAFT STATE OF OREGON

· · · · ·

#### CERTIFICATE OF WATER RIGHT

THIS CERTIFICATE ISSUED TO

STATE OF OREGON WATER RESOURCES DEPARTMENT SALEM, OREGON 97310

The specific limits for the use are listed below along with conditions of use.

Source: ROCK CR tributary to JOHN DAY R

County: GILLIAM

Purpose: UPSTREAM PASSAGE OF ADULT AND JUVENILE FISH INCLUDING SUMMER STEELHEAD AND RESIDENT RAINBOW TROUT

To be maintained in:

ROCK CREEK FROM USGS GAGING STATION AT WHITE PARK RM 40.0 (NESW, SECTION 36, T3S, R22E); TO THE MOUTH OF ROCK CREEK RM 0.0 (NESW, SECTION 11, T1N, R19E)

The right is established under Oregon Revised Statutes 537.341.

The date of priority is 3/21/90.

The following conditions apply to the use of water under this certificate:

 The right is limited to not more than the amounts, in cubic feet per second, during the time periods listed below:

 JAN
 FEB
 MAR
 APR
 MAY
 JUN
 JUL
 AUG
 SEP
 OCT
 NOV
 DEC

 34
 57
 57
 57
 57
 11
 4.7
 3.09
 2.47
 2.72
 6.67
 21.8

- The water right holder shall measure and report the in-stream flow along the reach of the stream or river described in the certificate as may be required by the standards for in-stream water right reporting of the Water Resources Commission.
- For purposes of water distribution, this instream right shall not have priority over human or livestock consumption.
- The instream flow allocated pursuant to this water right is not in addition to other instream flows created by a prior water right or designated minimum perennial stream flow.
- The flows are to be measured at the lower end of the stream reach to protect necessary flows throughout the reach.

Witness the signature of the Water Resources Director affixed this 1st day of \_\_\_\_\_, 19\_\_\_\_

Water Resources Director

Recorded in State Record of Water Right Certificate number \_\_\_\_\_.

IS70863

## BEFORE THE WATER RESOURCES DEPARTMENT OF OREGON WATER RIGHTS DIVISION

| In the Matter of Surface Water Application )<br>IS 70251 in the Name of Oregon Water Resources ) | PROTEST TO     |
|--|----------------|
| Department for Instream Water Use, )   | PROPOSED FINAL |
| Gilliam County   | ORDER          |

Protestant A. David Childs, in accordance with ORS 537.153 (6) and OAR 690-77-043, submits the following Protest to Proposed Final Order for Application IS 70251.

#### I. INTRODUCTION

Protestant's address is 1806 Thompson Street, The Dalles, Oregon 970558; phone number (541) 298-1499. Protestant is a landowner in the Rock Creek subbasin, where the instream water right has been applied for.

Protestant asserts that the Proposed Final Order ("PFO") by the Water Resources Department ("WRD" or "Department") is defective and in error and that there are elements of the water right as approved that will impair or be detrimental to the public interest, based on the facts and issues set forth below. The action proposed in the Proposed Final Order if not modified will result in excessive and unrealistic instream flows, set at quantities that do not and have not historically flowed in Rock Creek to the detriment of the Protestant.

The Protestant's interest as a landowner and user of Rock Creek for recreational and aesthetic purposes would be impaired by instream water rights granted in excessive amounts unrelated to the true flows of the stream. The Protestant is interested in the restoration of Rock Creek and possible upstream reservoir development for stream enhancement. In order for restoration work to be carried forward for Rock Creek, instream water rights must reflect the true conditions in the stream and actual flows available. If excessive quantities are granted that are not attainable, the restoration of Rock Creek will suffer as a result and flows would not be available for possible storage projects for stream enhancement.

## II. ODFW'S APPLICATION IS DEFECTIVE AND SHOULD BE REJECTED

The application filed by the Oregon Department of Fish & Wildlife ("ODFW") should be rejected by the WRD due to the deficiencies set forth below.

## A. METHOD USED BY ODFW IS UNACCEPTABLE METHODOLOGY FOR INSTREAM WATER RIGHT APPLICATION

ODFW's application under part 5. as to the "Method(s) used to determine the requested amounts" states: "Flow required to operate proposed fish passage facilities during migration period for adults and juveniles. Required flows are based on engineering determi (sp) using USGS data and passage facility design." (emphasis added). The flows requested are not based on any acceptable methodology for determining a flow rate for an instream water right application under the rules of the applicant agency, the Oregon Department of Fish & Wildlife. See OAR 635-400-015 for the "Instream Flow Measurement Methodologies" that are acceptable.

The Water Resources Department's rules governing instream applications require that "all applications for instream water rights shall be based on methods of determining instream flows needs that have been approved by administrative rule of the agencies submitting the applications." OAR 690-77-020 (3). Therefore the application submitted is defective and should be rejected by the Department since the application is based on a *proposed* fish passage facility.

Any assertion that ODFW's request represents a methodology acceptable under OAR 635-400-015 (9) is not valid. First, there is no information or data in the WRD file to indicate that ODFW conducted any "Site-specific studies...to determine flows necessary for...maintaining passage for fish migration or other specific requirements." The only information in support of ODFW's specific request is a letter from Al Mirati of ODFW to Michael Mattick of WRD dated November 15, 1994 with attached material regarding a proposed fishway in response to a WRD information request (Exhibit 1). That Exhibit reveals that the sole basis for the requested flows is a <u>proposed</u> "functional design for the Harper Dam Fishway on Rock Creek" (Exhibit 1 at 2). A design for a proposed fishway is not the same as a site-specific study, it is simply a proposed design for a fishway and nothing more.

Secondly, the information submitted on the proposed design shows that "the fishway is designed to accommodate passage" when adult steelhead are expected to be present "during the months of February through May..." (Exhibit 1 at 5). Therefore, at most, the requested flows are only valid for the months of February through May and there is <u>no supporting data whatsoever for the months of June through</u> <u>January</u>. Moreover, the design information makes it clear that 34 cubic feet per second is the "minimum" flow supposedly needed for the fishway to function. Since ORS 537.332 (2) sets forth that the standard for instream water rights is the "minimum quantity of water necessary to support the public use requested by an agency", 34 cfs is the highest amount that should be granted.

The requested flows are also obviously defective and the "methodology" is flawed, however, since the <u>"proposed" fish passage</u> <u>facility was never constructed</u>. Instead of the designed fishway on which the instream water right application is based, the fish ladder constructed at Harper Dam (aka Baird Dam) is of a different design. The fishway actually constructed does not require flows anywhere near even the 34 cfs minimum requested by ODFW. See Exhibit 2, Photocopy of picture of Harper fish ladder taken on August 31, 1996 by the Protestant.

## B. BASIN INVESTIGATION FLOW REQUIREMENT NOT FOLLOWED BY ODFW

As noted above, ODFW's application is based solely on proposed design flows of a fishway that was not constructed. The flow requests were not based on the John Day River Basin Investigation. ODFW's own rules require that "Instream flow requirements in the OSGC Environmental Basin Investigation Reports <u>shall be used</u> to apply for instream water rights for waterways listed in the reports." (emphasis added; OAR 635-400-015 (13)). This mandatory requirement was not followed by ODFW. The failure by ODFW to follow the requirement contained in its rules to use the Basin Investigation Reports again results in a application whereby the agency failed to follow the "methods of determining instream flow needs that have been approved by administrative rule of the agencies submitting the applications." OAR 690-77-020 (3). The application should be rejected on this basis.

If the Department chooses instead to modify the instream water right allowed, the flow rates granted should at least be reduced for January through April to the minimum flows recommended by ODFW's predecessor in the Basin Investigation for the John Day River Basin. These amounts are as follows: January - 35 cfs; February - 35/50 cfs; March - 50 cfs; April - 50 cfs.

### C. ODFW FAILED TO COMPARE FLOWS REQUESTED WITH EXISTING GAGING DATA

ODFW failed to compare the flows it requested with existing gaging data, as required by OAR 635-400-015 (10). Subsection (a) of that same administrative rule requires ODFW to further evaluate their instream flow requests: "Instream flow requirements greater than 70 percent or less than 30 percent of the naturally occurring stream flows...for any given time period shall be evaluated for appropriateness of the requirement in relation to naturally occurring stream flows or water surface elevations."

Despite the availability of gaging data at both the Whyte Park gage (#14047390) and the Cayuse Canyon gage (#14047400) ODFW failed to gather the information and make any comparisons or evaluations. This additional failure by ODFW to follow its own rules on instream applications results in submission of a defective application to the WRD.

## D. NO TECHNICAL DATA OR SUPPORTING INFORMATION SUBMITTED BY ODFW

Where applicable, ODFW must also submit supporting data to show that the standards and criteria contained in their rules has been followed. OAR 690-77-020 (4)(g). No such submission was made to the WRD in this case, with the possible exception of the information on the "proposed" fishway and design flows for it. Therefore, Application IS-70251 failed to include sufficient technical data or information to support the flow rates requested by said agency, as required by OAR 690-77-020 and ORS 537.336. OAR 690-77-020 (4)(g) requires an application to include at a minimum "a description of the <u>technical data</u> and methods used to determine the requested amounts;" (emphasis added). The only information submitted in support of the application was the flow rate amounts set forth in ODFW's application. ODFW later submitted information regarding the proposed fish ladder, including designed flows rates for that specific fishway. Since the proposed fishway was never constructed, it is obvious that there is no validity as to the "technical data" submitted. Even if the fishway had been constructed, the design flows were only applicable to the months of February through May (Exhibit 1 at 5). No technical data or supporting information whatsoever was submitted for the months of June through January.

In this case, the Department under OAR 690-77-020 (7) requested "additional information needed to complete the review". The additional information submitted by ODFW (Exhibit 1) was still defective and incomplete as noted above. Therefore, ODFW's application is defective and incomplete and should be returned to them for resubmission in accordance with OAR 690-77-027 (1): "If the Department determines that the application is incomplete or defective, the Department shall return the application."

### II. "EANF" CALCULATIONS ARE DEFECTIVE and INCOMPLETE

....

# A. LACK OF INFORMATION IN WRD FILE TO SUPPORT "EANF" CALCULATIONS

There are no calculations or information in the WRD file to show what "ratios" were used or how adjustments were made to any gaged flows to determine the estimated average natural flows ("EANF"). See OAR 690-77-010 (11) . Particularly where the "EANF" review under OAR 690-77-015 (4) is literally the only analysis of the requested flows by the WRD, it is critical that the basis for the "EANF" calculations be available for review. The only information available are the *conclusions* of what the WRD has determined the "EANF" flows are. There is also no information in the WRD file or the Technical Review to show the type of statistics or model used, the actual figures used to calculate "EANF", or any adjustments that were made (see "Methods for Determining Streamflows and Water Availability in Oregon", <u>Robison</u>, p. 22 and 23). The Protestant maintains that the EANF calculations are defective, resulting in high EANF levels and thus allowing excessive recommended flows by the WRD.

#### B. REVISED "EANF" CALCULATIONS NOT USED IN WRD'S ANALYSIS

The "EANF" flows calculated by WRD and used in the PFO review were revised by WRD staff. Nevertheless, the revised "EANF" calculations were not used to analyze the application and prepare the PFO (Personal communication with Rick Cooper, WRD, October 1, 1996). The Protestant asserts that the latest, revised "EANF" calculations must be used as required by OAR 690-77-015 (4). Protestant also requests that a copy of the revised "EANF" flows and the basis thereof be provided to counsel, since no such information was included in the WRD file.

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## C. GAGED INFORMATION and MISCELLANEOUS MEASUREMENTS NOT UTILIZED FOR "EANF" REVIEW: HIGHLIGHT ZERO STREAMFLOWS IN SUMMER MONTHS

The "EANF" calculations done by WRD staff utilized gaged flow information for Rock Creek from the Whyte Park gage at river mile 40.8 (#14047390); the review did not, however, utilize additional gaged flow information from the Cayuse Canyon gage (#14047400), approximately 5 miles downstream from Whyte Park (Personal communication with Rick Cooper, WRD, October 1, 1996). There is no Cayuse Canyon gage information in the WRD file.

The 13 years of information from the Cayuse Canyon gage is important to the determination of "EANF" because it provides a clear picture of Rock Creek flows and the behavior of the stream without any out-of-stream diversions. A review of the Cayuse Canyon gage information shows a clear pattern of <u>zero flow during significant</u> <u>stretches of time and mean flows that are much lower than the "EANF"</u> <u>calculations for most months.</u> For example, the mean flows in July, August and September are well below the "EANF" figures for 12 out of the 13 years of record; for June, 11 out of the 13 years are lower than "EANF" and for May 9 out of 13 years are lower. See Exhibit 3, Cayuse Canyon Gage #14147400, State Engineer-Water Resources Department, 1966-1978. These gaged flows establish that the "EANF" figures used in the PFO are higher than the actual flows in Rock Creek and therefore must be adjusted.

A comparison of the gaged flows from the two gages also shows that during the summer months, stream flow downstream is equal to or <u>lower</u> than the flow upstream (Exhibit 3). Thus, the normal assumption of increasing flow as one proceeds downstream with added flow from tributaries is shown not to be true for Rock Creek.

The Cayuse Canyon gage fall within the "base period" of 1958-1987 used by the WRD to calculate "EANF" and overlaps with the Whyte Park gage for comparison purposes. The Cayuse Canyon gage also meets the criteria noted by the WRD in its "Water Availability File" dated January 25, 1994 (Memo on "A Methodology for Estimating Water Availability Based on Mean Daily Flows", January 26, 1994 in that it measured "unregulated streamflow", was "unaffected by large diversions" and had "at least three years of record (mean daily flows)".

That Rock Creek flows do not necessarily increase from tributaries as it flows downstream, is further buttressed by documentation in the John Day River Basin Report, Water Resources Department, November 1986, at page 193: "The Lower Subbasin can be characterized as an area that receives water, as opposed to one that produces it. Most streams in the subbasin are nearly ephemeral, almost ceasing to flow in summer." (Exhibit 4 at 5). Note the statement that "Generally, streams tributary to the John Day are already dry or nearly dry by the time regulation for minimum flows is required." (Exhibit 4 at 6). For other information regarding "tributary streams" which "dry up in summer months" see <u>Rock Creek</u>

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Watershed Improvement Plan, Soil and Water Conservation District of Gilliam Morrow and Wheeler Counties, (May 22, 1991), Exhibit 8 at 7.

These general statements regarding streamflow in Rock Creek's subbasin are also supported by the Protestant's personal knowledge from diary entries which, for example, note that during the years 1959 through 1974 Rock Creek went dry every year (ranch location below French Charlie). The earliest date the creek went dry during that period was April 2nd and the latest was June 27th (diary entries not submitted at this time).

A comparison of flow at the two gages clearly highlights the fact that the flow of Rock Creek in the summer does not increase as it flows downstream. See <u>Water Availability for Oregon's Rivers and Streams: Volume 2; Technical Guide and Appendixes</u>, E. George Robison, May 1991, Appendix B, Table 5, page 23 and Appendix F, Table 5, page 16 (Exhibit 5), which shows comparisons of the Whyte Park and Cayuse Canyon gaged flows.

WRD's file for Application IS-70251 does contain miscellaneous flow measurements of the flow of Rock Creek, most of which are within the "base period" of 1958-1987 used for "EANF" calculations (see Exhibit 6, Miscellaneous Measurements, Rock Creek). Apparently these flow measurements were not used to calculate or adjust the "EANF" A comparison of the miscellaneous flows with WRD's figures. calculations of "estimated average natural flow" ("EANF") provides evidence that the EANF calculations are too high. A substantial number of these actual miscellaneous flows recorded are significantly lower than the EANF flows eventually used by the Department to analyze the application. Since the EANF flows are the only analysis or review conducted by the Department to determine whether requested flows meet the criteria for instream water rights, it is critical that EANF flows not be calculated at excessive levels. The Protestant maintains that these miscellaneous measurements should have been used to adjust the "EANF" calculations.

The other pattern that is abundantly clear when one scrutinizes all the gage records is that sudden heavy rainstorms will often drastically skew the averages higher. "Sudden severe convectional storms in summer months can lead to extreme localized flood peaks." <u>Rock Creek Watershed Improvement Plan</u>, Soil and Water Conservation District of Gilliam Morrow and Wheeler Counties, (May 22, 1991), Exhibit 8 at 4. A perfect example of this is shown by the miscellaneous gage readings for gage #14047480 (not in WRD file) for the year 1965 (Exhibit 9 at 7). The flow of Rock Creek, having just gone through nearly two months of zero flow in July and August, spikes up to 148 cfs on August 22nd and 128 cfs on August 23rd. The next day the flow drops all the way to 4.7 cfs. The result is a mean flow of 9.39 cfs for the month of August, despite the fact that 24 out of 31 days had zero flow.

The unmistakable pattern of flows *lower* than the "EANF" calculations, especially in the summer months, plus periods of zero streamflow is also shown in Exhibit 9. That exhibit contains twelve

sets of gage flow readings from various locations in the proposed 40 mile reach, for five different years. See also Exhibit 10 at 2, John Day Project, Department of the Interior, U.S. Reclamation Service (February 1916) for discharge readings in 1905 and 1911. These readings along with all the other gaged information should be taken into account when the WRD attempts to determine "EANF" figures.

## D. ADDITIONAL INFORMATION - ACTUAL FLOWS ARE LOWER THAN "EANF"

The John Day River Basin Report, Water Resources Department, November 1986 provides further evidence that the "EANF" flows as calculated are too high and need to be adjusted. Section IX on the Lower Subbasin of the John Day River, which includes Rock Creek, furnishes important information on climate, land cover and surface water that apparently were not considered when the "EANF" flows were calculated. In particular, information contained on page 193 regarding surface water flows in Rock Creek notes that Rock Creek's "mean monthly flows range from 120 cfs in March to <u>less than 1 cfs in</u> <u>September</u>." (emphasis added; Exhibit 4 at 5). By contrast, "EANF" for September was calculated at 2.47 cfs (PFO at 2).

Another area of concern is the use of an irrigation add-back utilized by the WRD staff to calculate "EANF" in this case (Personal communication, Rick Cooper, WRD, October 1, 1996). Part of the "EANF" flow figure was generated by adding to the gaged flows from the Whyte Park gage, in order to arrive at the estimate of the "EANF" flows at the mouth of Rock Creek. In most streams, such an add-back for irrigation use makes sense. For Rock Creek, however, one must be extremely cautious in utilizing an add-back for irrigation use since regulation of water use in Rock Creek "normally begins in May and June." (John Day River Basin Report, Exhibit 4 at 6).

Exhibit 7, Watermaster's Compilation for Rock Creek, shows normal cut-off dates for irrigation water rights in Rock Creek. Since no specific information regarding the irrigation add-back amounts was contained in the WRD file, it is impossible for the Protestant to ascertain if the add-back accurately reflects the true situation in Rock Creek. It is clear, however, from the Watermaster's Compilation that there should be little or no add-back for the months of July through October, since the regulation of even the earliest right on the stream (1868 priority) begins by August 1st (Exhibit 7). In fact, the John Day River Basin Report at page 193 states that "Rock Creek's flow stopped at some point nine years of the same period [13 year period]....Generally, no-flow conditions last from August through September." (Exhibit 4 at 5).

The <u>Final Environmental Impact Statement</u>, Rock Creek Watershed Project, Soil Conservation Service, U.S. Dept. of Agriculture (April 1975), contained the following information regarding Rock Creek flows:

"It [Rock Creek] is an unmodified perennial stream for approximately 20 miles in its upper reaches, an <u>unmodified</u> <u>intermittent stream</u> for 21 miles, and a modified intermittent stream for 30.7 miles in its lower reaches where it passes through cropland... Rock Creek has a typical snowmelt runoff pattern of high spring flows and low to nonexistent surface flows during the summer and fall... Rock Creek averages no flow for 30 days each year in the vicinity of Cayuse Canyon. In the seven years of record at this location the dry period ranged from 0 to 80 days. (17) In the lower reaches of Rock Creek the <u>stream</u> is essentially dry from June through November on the average."

(emphasis added; Exhibit 11 at 2, 3). The EIS also includes a table of average monthly stream discharges at three locations which shows zero flow during several months at two of the locations, including the mouth of Rock Creek (Exhibit 11 at 3).

The <u>Rock Creek Watershed Improvement Plan</u>, Soil and Water Conservation Districts of Gilliam, Morrow and Wheeler Counties, (May 22, 1991) also provides evidence that "[L]ate season baseflow has become unreliable and, in fact, is nonexistent through much of the summer." (Exhibit 8 at 2). "Summer flows for irrigation and instream use is minimal to nonexistent. Stream hydrographs shown in Appendix A reinforce what irrigators know: during much of the summer, there is no water available in Rock Creek." (Exhibit 8 at 5; see also page 6).

The Water Resources Department itself noted the problem with "late season water shortages. This situation is most serious along smaller tributaries [to the John Day River] because late summer flows are often extremely low or nonexistent." John Day River Basin, State Water Resources Board, March 1962, page 35 (Exhibit 12 at 2).

#### E. POTENTIAL PROBLEMS WITH REVISED EANF CALCULATIONS

As noted above, no specific information regarding the basis for the "EANF" calculations is contained in the WRD's file. Thus, it is not possible to adequately review the "EANF" calculations and determine their accuracy for Rock Creek. One of the problems for Rock Creek is that the stream flow is heavily dependent, if not entirely based, on large spring flows in the summer months. As noted in the WRD report discussing poor performance of regression models at page 24, "The Water Availability Program - A Progress Report - 1993" (April 1993): "The reason for much of the poor performance apparently is related to hydrologic processes (i.e. large spring flow) that cannot be accounted for in the existing models." Therefore, if a regression model is used for Rock Creek, problems can be expected due to the makeup of summer flows.

## III. FLOW PROPOSED FOR MAY INADVERTENTLY EXCEEDS "EANF" FLOW

Although the WRD calculated in May the "estimated average natural flow" for Rock Creek was 32 cubic feet per second, the PFO failed to limit the flow for May to that amount. In accordance with OAR 690-77-015 (3) and (4), the flow rate for May should be reduced to 32 cfs. The Technical Review dated November 25, 1995 did comply with the "EANF" limitation and proposed a flow in May of 32 cfs.

# IV. PROPOSED FLOW RATES ARE IN EXCESS OF MINIMUM QUANTITY NECESSARY

The instream water right flow rates proposed are excessive and unnecessary for the use applied for. The flow rates proposed are higher than the <u>minimum quantity of water necessary</u> for the public use of the instream water right, and are, therefore, contrary to the definition of "In-stream flow" of ORS 537.332 (2) and OAR 690-77-010 (14). Water use of the instream right, if approved, would adversely affect the Protestant and potential water users from the stream by appropriating excess quantities of water and preventing any other new appropriations of water.

The flow rates granted must be reduced to the minimum quantity of water necessary for the fishery purpose of the application. At the very least, the flow rates should be reduced to the lesser of: (1) the revised "EANF" flow rates (see part II.B. above); or (2) the minimum flows recommended in the John Day River Basin Investigation (see part I.B. above).

#### V. WRD FAILED TO ANALYZE FLOW NEEDS

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The flow levels approved by the Proposed Final Order are not based on any analysis of the need for the flows requested. ORS 537.332 (2) sets out the definition of "In-stream flow" which the Department is supposed to follow when determining instream water rights: the "minimum quantity of water necessary to support the public use requested by an agency". The Proposed Final Order does not address the minimum quantity of water or flow levels necessary to support the uses applied for: fishery needs. Fish passage was the sole basis for the ODFW application; the WRD unfortunately relied on a "proposed" fishway design that never was built.

A review of the WRD file shows that no analysis of any kind regarding flow needs occurred. The only review undertaken by the WRD was a check to see if the requested flows are less than the average estimate natural flow ("EANF"; OAR 690-77-015 (4)).

#### VI. REACH PROBLEMS - INTERMITTENT FLOW IN SUMMER MONTHS

The fact that spring flows at limited locations provide all of the flow of Rock Creek and that a dry streambed exists for the great majority of Rock Creek during low flow season must be taken into account by the WRD. Granting instream water rights for a 40 mile reach of stream, when the only flow in summer is provided in short stretches fed by springs, fails to account for the actual streamflow that exists. A detailed discussion and documentation of facts regarding the reach of the application and the variance of stream flows from upstream to downstream locations is set forth above under part II. C. and D.

OAR 690-77-015 (9) contains the requirement that the "amount, timing and location" of the instream water right shall serve a public use or uses. The specific circumstances regarding Rock Creek need to be viewed in light of this requirement. A 40 mile reach has been proposed. In the summer, evidence exists to show that the surface flow of Rock Creek often ceases for the majority of the stream (see above); the only flow exists in small sections of Rock Creek where water from springs feeds the streambed. This variance of surface flow at different locations in Rock Creek was also measured and noted by Watermaster Bob Main in a letter to Walter N. Perry of the State Engineer's Office on June 6, 1975 (Exhibit 13). As noted in the Rock Creek Watershed Improvement Plan, Soil and Water Conservation District of Gilliam Morrow and Wheeler Counties, (May 22, 1991), "near the mouth of Rock Creek a spring in the streambed produces flow continuously, whereas except for several springs, no water may be found upstream until above the town of Olex." (Exhibit 8 at 3). Any instream right granted for Rock Creek should be limited accordingly and note the likelihood of dry streambed throughout most of the reach.

#### CONCLUSION

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This Protest is filed in accordance with OAR 690-77-043. The issues raised should be considered as part of a contested case hearing. The WRD's Proposed Final Order is inadequate and defective and has failed to follow applicable rules. A thorough review of the application is necessary to determine the minimum quantity of water necessary to support the public uses applied for.

For the reasons set forth above, the protestant asserts that the application is defective and should be returned to the applicants. The flow levels requested are excessive and are not necessary to support the public uses proposed. Flow levels set at the rates proposed will interfere with future maximum economic development of the waters of the State of Oregon. Excessive flow rates for instream water rights represent a wasteful and unreasonable use of the water involved (ORS 537.170 (8)(e)).

Based on the points discussed above, the Proposed Final Order should deny the application for a permit or modify the Proposed Final Order accordingly.

Respectfully submitted this 4th day of October, 1996.

By: Dovid C. Moon

David C. Moon Attorney for Protestant

#### CERTIFICATE OF FILING AND SERVICE

I hereby certify that on the 4th day of October, 1996 I filed the original of the foregoing Protest to the Proposed Final Order on the Water Resources Department by causing said original to be personally delivered to the Water Resources Department at the address set forth below. I further certify that on the 4th day of October, 1996 I served a true and accurate copy of the foregoing Protest to the Proposed Final Order on the applicant by mailing said copy by first class mail, postage prepaid, by depositing said copy in the United States Post Office in Eugene, Oregon, addressed as set forth below:

Oregon Water Resources Department Commerce Building 158 12th Street N.E. Salem, Oregon 97310-0210

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Oregon Department of Fish & Wildlife 2501 SW First Avenue P.O. Box 59 Portland, Oregon 97207

By:

David C. Moon Attorney for Protestant

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# 50% Exceedance Streamflows for Some Watersheds in the John Day Basin

Natural streamflows and water availability for the John Day basin were first calculated in late 1994. At that time 5 watersheds with ISWR applications were analyzed: 69960, 70250, 70251, 70263, and 70648. The natural streamflows for these ungaged watersheds were estimated by an area - precipitation ratio with similar gaged watersheds. Estimates for these five watersheds were revised in 1996. A regression analysis was used to make these new estimates. At that time, additional streamflow data for Bridge Creek were incorporated. Streamflows for all other watersheds with ISWR applications in the John Day basin also were estimated in 1996.

Natural streamflows for 5 original watersheds calculated from area - precipitation ratio (Late 1994)

| 69960    | 654.00 | 1250.00 | 1850.00 | 3200.00 | 3460.00 | 1630.00 | 346.00 | 157.00 | 140.00 | 168.00 | 243.00 | 494.00 |
|----------|--------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|
| 1 _70250 | 6.23   | 13.50   | 21.60   | 20.10   | 5.54    | 1.90    | 0.81   | 0.54   | 0.43   | 0.47   | 1.16   | 3.77   |
| 0 70251  | 36.00  | 77.70   | 125.00  | 116.00  | 32.00   | 11.00   | 4.70   | 3.09   | 2.47   | 2.72   | 6.67   | 21.80  |
| -70263   | 5.08   | 11.00   | 17.60   | 16.40   | 4.52    | 1.55    | 0.66   | 0.44   | 0.35   | 0.38   | 0.94   | 3.07   |
| 70648    | 93.40  | 138.00  | 166.00  | 385.00  | 891.00  | 697.00  | 128.00 | 56.00  | 49.30  | 53.70  | 65.80  | 75.30  |

Natural streamflows for 5 original watersheds calculated from regression analysis and incorporating additional gage information for Bridge Creek (Early 1996)

|       | 69960   | 652.00 | 1250.00 | 1830.00 | 3180.00 | 3480.00 | 1640.00 | 359.00 | 164.00 | 144.00 | 171.00 | 243.00 | 492.00 |
|-------|---------|--------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|
| Cert  | - 10250 | 7.25   | 6.23    | 10.00   | 20.80   | 31.50   | 28.80   | 6.41   | 2.95   | 4.69   | 4.45   | 4.80   | 5.05   |
|       | 70251   | 38.50  | 79.20   | 120.00  | 88.40   | 39.50   | 24.00   | 3.13   | 1.56   | 1.61   | 2.74   | 8.92   | 20.60  |
| CENT  |         | 6.41   | 6.02    | 9.94    | 16.80   | 15.90   | 12.30   | 2.75   | 1.36   | 2.00   | 2.02   | 3.13   | 4.48   |
| ier T | 70648   | 112.00 | 135.00  | 163.00  | 547.00  | 1310.00 | 701.00  | 155.00 | 69.60  | 58.60  | 67.60  | 86.30  | 105.00 |

Natural streamflows for remaining watersheds with ISWR applications (Early 1996)

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| 69949 | 11.60 | 11.70 | 15.90 | 32.30 | 47.80  | 28.20  | 13.20 | 7.62  | 8.18  | 10.40 | 12.20 | 11.50 |
|-------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|-------|-------|
| 69951 | 8.08  | 7.84  | 10.40 | 21.40 | 34.40  | 21.70  | 10.50 | 5.97  | 6.33  | 7.92  | 8.91  | 8.18  |
| 69958 | 13.10 | 15.40 | 19.10 | 76.80 | 194.00 | 70.90  | 13.10 | 4.10  | 4.00  | 5.57  | 9.26  | 12.10 |
| 69959 | 7.10  | 8.90  | 11.40 | 43.70 | 92.80  | 37.90  | 6.38  | 2.31  | 2.04  | 2.95  | 4.09  | 6.39  |
| 69961 | 4.40  | 4.70  | 0.31  | 20.50 | 33.40  | 26.00  | 4.82  | 3.38  | 3.01  | 3.49  | 4.25  | 3.99  |
| 69963 | 4.47  | 5.41  | 9.51  | 14.80 | 12.80  | 8.19   | 2.33  | 0.55  | 0.37  | 1.74  | 3.31  | 4.03  |
| 70640 | 9.92  | 8.95  | 10.59 | 19.40 | 36.20  | 28.40  | 16.60 | 9.20  | 9.57  | 11.50 | 11.90 | 10.30 |
| 70641 | 5.11  | 4.45  | 5.28  | 10.00 | 20.20  | 16.00  | 9.07  | 5.10  | 5.18  | 6.18  | 6.33  | 5.38  |
| 70642 | 3.76  | 3.34  | 4.19  | 8.31  | 16.10  | 11.60  | 5.97  | 3.46  | 3.47  | 4.24  | 4.53  | 3.91  |
| 70643 | 2.47  | 3.10  | 6.32  | 15.60 | 20.40  | 11.10  | 2.88  | 1.32  | 1.06  | 1.38  | 2.05  | 2.43  |
| 70644 | 4.76  | 5.83  | 11.90 | 29.40 | 41.90  | 24.60  | 6.63  | 2.55  | 2.10  | 2.73  | 4.11  | 4.65  |
| 70645 | 7.03  | 10.10 | 20.30 | 45.10 | 50.20  | 25.10  | 6.77  | 3.02  | 2.45  | 3.23  | 4.92  | 6.78  |
| 70646 | 2.93  | 3.14  | 3.76  | 5.54  | 7.15   | 9.85   | 2.63  | 1.88  | 1.24  | 1.48  | 2.01  | 2.60  |
| 70647 | 16.70 | 15.40 | 15.80 | 32.70 | 210.00 | 260.00 | 72.60 | 36.30 | 28.60 | 28.20 | 23.50 | 15.70 |
| 70649 | 2.88  | 3.19  | 4.25  | 18.20 | 45.00  | 19.10  | 3.11  | 0.97  | 0.83  | 1.21  | 1.81  | 2.59  |
| 70650 | 6.06  | 6.00  | 7.29  | 19.60 | 109.00 | 97.20  | 20.30 | 10.20 | 8.27  | 8.46  | 7.80  | 5.60  |
| 70651 | 3.79  | 8.26  | 18.00 | 29.00 | 17.30  | 7.94   | 1.53  | 0.78  | 0.55  | 0.76  | 1.07  | 2.72  |
| 70652 | 5.91  | 7.50  | 12.80 | 29.60 | 43.80  | 27.60  | 5.50  | 3.97  | 3.73  | 4.30  | 5.09  | 5.24  |
| 70653 | 7.76  | 11.30 | 19.50 | 42.30 | 57.00  | 36.40  | 7.47  | 4.56  | 4.27  | 5.06  | 5.41  | 6.52  |
| 70654 | 3.77  | 5.01  | 8.65  | 18.20 | 24.40  | 11.20  | 2.79  | 0.69  | 0.76  | 0.91  | 2.15  | 2.94  |
| 70655 | 1.96  | 2.82  | 4.93  | 7.98  | 7.04   | 2.49   | 0.85  | 0.13  | 0.09  | 0.45  | 1.24  | 1.69  |

4-30-13 NEWLOT EANE for These are the best latest numbers quailable Send little t g/2 +/s w/ duft FO MM

Water Availability Analysis

http://apps.wrd.state.or.us/apps/wars/wars\_display\_wa\_tables/display\_wa\_details.aspx?ws\_...

# Water Availability Analysis Detailed Reports

ROCK CR > JOHN DAY R - AT MOUTH JOHN DAY BASIN Water Availability as of 4/29/2013

Watershed ID #: 70251 Date: 4/29/2013 Exceedance Level: 50% Time: 11:16 AM

| Natur Availa siller Caleniadon | Consumptive Uses and Storages | Instream Flow Requirements | Reservations |  |  |  |
|--------------------------------|-------------------------------|----------------------------|--------------|--|--|--|
| Water                          | Rights                        | Watershed Characteristics  |              |  |  |  |

# Water Availability Calculation

Monthly Streamflow in Cubic Feet per Second

Annual Volume at 50% Exceedance in Acre-Feet

| Month | Natural Stream Flow   | Consumptive Uses and Storages | Expected Stream Flow | Reserved Stream Flow | Instream Flow Requirement | t Net Water Available |
|-------|-----------------------|-------------------------------|----------------------|----------------------|---------------------------|-----------------------|
| JAN   | 3 <mark>6.</mark> 10  | 0.01                          | 36.10                | 10.00                | 34.0                      | 0. \ -7.95            |
| FEB   | 7 <mark>8.</mark> 00  | 0.02                          | 78.00                | 21.70                | 57.0                      | -0.71                 |
| MAR   | 12 <mark>3.</mark> 00 | 5.29                          | 118.00               | 33.60                | 57.0                      | 27.10                 |
| APR   | 75.60                 | 8.10                          | 67.50                | 18.80                | 57.0                      | 0 -8.27               |
| MAY   | 33.10                 | 20.70                         | 12.40                | 3.45                 | 33.1 57.0                 | -48.00 - 24.15        |
| JUN   | 12.60                 | 16.70                         | -4.13                | 0.00                 | 11.0                      | 0 -15.10              |
| JUL   | <mark>3.6</mark> 9    | 5.58                          | -1.89                | 0.00                 | 4.7                       | 0 -6.59               |
| AUG   | 2.29                  | 2.23                          | 0.06                 | 0.00                 | 3.0                       | 9 -3.03               |
| SEP   | 2.24                  | 1.15                          | 1.09                 | 0.00                 | 2.4                       | 7 -1.38               |
| OCT   | 3. <mark>2</mark> 6   | 0.56                          | 2.70                 | 0.00                 | 2.7                       | 2 -0.02               |
| NOV   | 8. <mark>6</mark> 1   | 0.01                          | 8.60                 | 2.39                 | 6.6                       | 7 -0.46               |
| DEC   | 19. <mark>1</mark> 0  | 0.00                          | 19.10                | 5.31                 | 21.8                      | 0 -8.01               |
| ANN   | 23,800.00             | 3,660.00                      | 20,500.00            | 5,700.00             | 18,900.0                  | 0 1,660.00            |

# **Patricia McCarty**

From: Sent: To: Subject: Patricia McCarty Thursday, August 29, 2013 3:35 PM 'Pagel, Martha' RE: Instream Water Right Applications

Any time after 8 is fine.

Patricia

From: Pagel, Martha [mailto:MPagel@SCHWABE.com] Sent: Thursday, August 29, 2013 3:02 PM To: Patricia McCarty Subject: RE: Instream Water Right Applications

Patricia,

Can I call you tomorrow morning to talk more about this? I'm still trying to develop a proposal for Mr. Childs as to what I might be able to help him achieve, and I will also need to have a follow-up conversation with John Sample at PacifiCorp.

What would be a good time to call you? Thanks.

MARTHA O. PAGEL | Attorney at Law SCHWABE, WILLIAMSON & WYATT Direct: 503-540-4260 | Fax: 503-796-2900 | Cell: 503-507-7293 | Email: mpagel@schwabe.com

From: Patricia McCarty [mailto:patricia.e.mccarty@state.or.us] Sent: Thursday, August 29, 2013 9:21 AM To: Pagel, Martha Subject: Instream Water Right Applications

#### Martha,

I've discussed your question to the department regarding instream water right applications and the impacts on storage opportunities. Dwight and Tim have informed me that the department is not currently contemplating a change to the water availability exceedance value used in processing instream water right applications.

I also discussed your proposal to the department to bring interested parties together to have a policy exploration/discussion about the same topic. A settlement discussion between the department, ODFW and protestants for the purpose of resolving a protest on an application is something I will be able to arrange, but the broader policy discussion is beyond the protest program's reach. Let me know if you would like for me to work on setting up a meeting with ODFW on either the Rock Creek application or on the applications protested by PacifiCorp.

Also, thank you for the reference to ORS 537.352 and Div. 77. Tim, Dwight and I are looking at that now, and will welcome your input on how it can be applied. We will need to look at the legislative history, as it is not entirely clear to us how it fits in with a Division 33 recommendation from ODFW, among other things.

I will be out of the office September 2<sup>nd</sup> through the 13<sup>th</sup>. I will be back in September 16<sup>th</sup>. I look forward to talking with you then.

Patricia

From: Pagel, Martha [mailto:MPagel@SCHWABE.com] Sent: Monday, August 26, 2013 11:53 AM To: Patricia McCarty Subject: RE: Instream Water Right Applications

Thank you.

FYI – I spent some time reviewing the statutes and rules and was reminded of ORS 537.352, which could help address the concern about preserving the ability to approve new storage in the future. However, I was surprised to see OAR 690-077—0100, which seems to be contrary to the statute in allowing discretion for the Water Resources Commission to deny a request for "precedence." It could go a long way to address protest concerns if instream water right certificates were issued with reference to the statutory requirement of 537.352, but I'm worried about the rule provision...

Martha

MARTHA O. PAGEL | Attorney at Law SCHWABE, WILLIAMSON & WYATT Direct: 503-540-4260 | Fax: 503-796-2900 | Cell: 503-507-7293 | Email: mpagel@schwabe.com

From: Patricia McCarty [<u>mailto:patricia.e.mccarty@state.or.us</u>] Sent: Monday, August 26, 2013 11:35 AM To: Pagel, Martha Subject: RE: Instream Water Right Applications

Here is the list

Patricia

From: Pagel, Martha [mailto:MPagel@SCHWABE.com] Sent: Monday, August 26, 2013 9:41 AM To: Patricia McCarty Subject: Instream Water Right Applications

Hi Patricia,

Do you have a list of all the pending instream water right applications that were protested? Could I get a copy?

Thanks, Martha

MARTHA O. PAGEL | Attorney at Law SCHWABE, WILLIAMSON & WYATT 530 Center St. NE, Ste. 400, Salem, OR 97301 Direct: 503-540-4260 | Fax: 503-796-2900 | Cell: 503-507-7293 | Email: <u>mpagel@schwabe.com</u> Assistant: Karen Donohue| Direct: 503-540-4262 | <u>kdonohue@schwabe.com</u> Legal advisors for the future of your business@ www.schwabe.com

| 70251                 |             |             |             |      |      |      |      |      |              |
|-----------------------|-------------|-------------|-------------|------|------|------|------|------|--------------|
| 1994 EANF -used in IR |             |             |             |      |      |      |      |      |              |
| J                     | F           | М           | А           | М    | J    | J    | А    | S    | 0            |
| 36                    | 77.7        | 125         | 116         | 32   | 11   | 4.7  | 3.09 | 2.47 | 2.72         |
| 1996 EANF             |             |             |             |      |      |      |      |      |              |
| J                     | F           | М           | А           | М    | J    | J    | А    | S    | 0            |
| 38.5                  | 79.2        | 120         | 88.4        | 39.5 | 14   | 3.13 | 1.56 | 1.61 | 2.74         |
| Current EA            | NF-should   | use for Cer | t on 70251  |      |      |      |      |      |              |
| J                     | F           | М           | А           | М    | J    | J    | А    | S    | 0            |
| 36.1                  | 78          | 123         | 75.6        | 33.1 | 12.6 | 3.69 | 2.29 | 2.24 | 3.26         |
| IS70251 ar            | nount appl  | ied for     |             |      |      |      |      |      |              |
| J                     | F           | M           | A           | М    | J    | J    | A    | S    | 0            |
| 34                    | 57          | 57          | 57          | 57   | 34   | 34   | 34   | 34   | 34           |
| Max allow             | ed for cert | based amo   | unt applied | for  |      |      |      |      |              |
| J                     | F           | М           | А           | М    | J    | J    | A    | S    | 0            |
| 34                    | 57          | 57          | 57          | 33.1 | 12.6 | 3.69 | 2.29 | 2.24 | 3.26         |
|                       |             |             |             |      |      |      |      |      | and a second |

| N    | D    |  |  |  |  |
|------|------|--|--|--|--|
| 6.67 | 21.8 |  |  |  |  |
|      |      |  |  |  |  |
|      |      |  |  |  |  |
| N    | D    |  |  |  |  |
| 8.92 | 20.6 |  |  |  |  |
|      |      |  |  |  |  |
| N    | D    |  |  |  |  |
| 8.61 | 19.1 |  |  |  |  |
|      |      |  |  |  |  |
|      |      |  |  |  |  |
| N    | D    |  |  |  |  |
| . 34 | 34   |  |  |  |  |
|      |      |  |  |  |  |
|      |      |  |  |  |  |
| N    | D    |  |  |  |  |
| 8.61 | 19.1 |  |  |  |  |
|      |      |  |  |  |  |





Water Resources Department North Mall Office Building 725 Summer Street NE, Suite A Salem, OR 97301-1271 503-986-0900 FAX 503-986-0904

August 5, 2013 - via first class mail

David Childs 1806 Thompson St. The Dalles, OR 97058

Re: Protest to ODFW Instream Water Right Application S-70251

Dear Mr. Childs,

The Oregon Department of Fish and Wildlife filed numerous applications for instream water rights in 1990 on various streams across Oregon. You protested Application # 70251 for Rock Creek.

After a review of the issues raised in the protest Water Resources has determined that a certificate should be issued. The estimated average natural flow in Rock Creek has been revised since 1996 and the proposed certificate reflects those changes. The instream certificate priority date is March 21, 1990, junior to all other existing surface water rights on Rock Creek and its tributaries in the vicinity of the instream reach.

You will receive a copy of the Final Order on the application. Enclosed is a draft of the final order and certificate. If you still have concerns regarding the proposed order and certificate please let me know by contacting me directly at the number or email below.

Sincerely,

Patricia Mc Carty

Patricia McCarty Protest Program Coordinator Water Right Services Division 503-986-0820

Oregon Water Resources Department Water Right Services Division

> Instream Water Right Application Number IS 70251

## **Final Order**

## Application History

On March 21, 1990, the Oregon Department of Fish and Wildlife submitted an application to the Department for an instream water right. On August 20, 1996, the Department issued a Proposed Final Order proposing to issue the certificate with conditions. The amount requested in the application exceeds the estimated average natural flow. Pursuant to OAR 690-077-0015(4) the amounts allowed during any time period were reduced to amounts not exceeding the estimated average natural flow occurring from the drainage basin.

On October 4, 1996, David Childs submitted a protest to the Proposed Final Order.

The findings of fact and conclusions of law in the Proposed Final Order are incorporated into this Final Order. After the issuance of the Proposed Final Order the Department updated the values for the estimated average natural flow for the reach of Rock Creek in which this right is to be maintained. The right as described in the certificate is therefore limited to the amount requested, further limited to an amount not exceeding the current estimated average natural flow.

The proposed use would not impair or be detrimental to the public interest.

## NOTICE OF RIGHT TO PETITION FOR RECONSIDERATION OR JUDICIAL REVIEW

This is an order in other than a contested case. This order is subject to judicial review under ORS 183.484. Any petition for judicial review must be filed within the 60-day time period specified by ORS 183.484(2). Pursuant to ORS 183.484, ORS 536.075 and OAR 137-004-0080, you may petition for judicial review or petition the Director for reconsideration of this order. A petition for reconsideration may be granted or denied by the Director, and if no action is taken within 60 days following the date the petition was filed, the petition shall be deemed denied.

Application IS 70251

Page 1 of 2

# Order

IT IS HEREBY ORDERED that Application IS 70251 be approved as provided in the attached certificate.

Issued \_\_\_\_\_

Dwight W. French Water Right Services Administrator, for Phillip C. Ward Director

Application IS 70251

Page 2 of 2
# STATE OF OREGON

# CERTIFICATE OF WATER RIGHT

# THIS CERTIFICATE ISSUED TO

# OREGON WATER RESOURCES DEPARTMENT 725 SUMMER ST NE, STE A SALEM, OREGON 97301

The specific limits for the use are listed below along with conditions of use.

Source: ROCK CREEK TRIBUTARY TO JOHN DAY RIVER

County: GILLIAM

# Purpose: UPSTREAM PASSAGE OF ADULT AND JUVENILE FISH INCLUDING SUMMER STEELHEAD AND RESIDENT RAINBOW TROUT

To be maintained in:

ROCK CREEK FROM USGS GAGING STATION AT WHYTE PARK RM 40.0 (NESW, SECTION 36, T3S, R22E); TO THE MOUTH OF ROCK CREEK RM 0.0 (NESW, SECTION 11, T1N, R19E)

The right is established under Oregon Revised Statutes 537.341.

The date of priority is MARCH 21, 1990.

The following conditions apply to the use of water under this certificate:

- 1. The right is limited to not more than the amounts, in cubic feet per second, during the time periods listed below:
- JAN
   FEB
   MAR
   APR
   MAY
   JUN
   JUL
   AUG
   SEP
   OCT
   NOV
   DEC

   34
   57
   57
   57
   33.10
   12.6
   3.69
   2.29
   2.24
   3.26
   8.61
   19.10

Application IS 70251

Page 1 of 2

Certificate 87XXX

- The water right holder shall measure and report the in-stream flow along the reach of the stream or river described in the certificate as may be required by the standards for in-stream water right reporting of the Water Resources Commission.
- For purposes of water distribution, this instream right shall not have priority over human or livestock consumption.
- 4. The instream flow allocated pursuant to this water right is not in addition to other instream flows created by a prior water right or designated minimum perennial stream flow.
- 5. The flows are to be measured at the lower end of the stream reach to protect necessary flows throughout the reach.

Issued \_

Dwight W. French Water Right Services Administrator, for Phillip C. Ward Director

Application IS 70251

Page 2 of 2 Recorded in State Record of Water Right Certificates numbered 87XXX



WATER

RESOURCES

DEPARTMENT

August 30, 1996

DAVID CHILDS 1806 THOMPSON ST THE DALLES OR 97058

RE: Instream Water Right Application IS-70251

Dear Mr. Childs,

Thank you for your interest in the above referenced application.

After a careful review of the situation regarding the mailing of the notice and the protest date we have decided not to extend the protest deadline which is 5:00 pm, Friday, October 4, 1996, for this application.

However, we will accept comments up to 5:00, October 14, 1996. Further, if you file a protest by the deadline (October 4, 1996), we will allow you to file supplementary information until 5:00, October 14, 1996.

I'm sorry for any inconvienience this may have caused you. It is our intent to give concerned citizens a fair opportunity to participate in the water rights review process.

If you have any more questions regarding the water rights review process or this application in particular, please give Mike Mattick or myself a call. I can be reached toll free from within Oregon at 1 (800) 624-3199 extension 268. Mike's extension is 276.

Sincerely

Dwight French Water Rights Section Manager

cc: file



Commerce Building 158 12th Street NE Salem, OR 97310-0210 (503) 378-3739 FAX (503) 378-8130 COPY CHECK-OFF SHEET FOR PROPOSED FINAL ORDERS

CC: FILE # IS 70251

WATERMASTER # KELLY RISE

REGIONAL MANAGER: KENT SEARLES

ODF&W - County: GILLIAM

DEQ

PARKS

OTHER STATE AGENCY IF NECESSARY:

DIVISION 33 LIST: \_\_\_\_ COLUMBIA RIVER INTERTRIBAL FISH COMMISSION; U.S. FISH & WILDLIFE; (CHECK ONLY IF APPLICABLE) NORTHWEST POWER PLANNING COUNCIL & NATIONAL MARINE FISHERIES

POWER BUILDER UPDATER; FRONT COUNTER

WATER FOR LIFE (TODD HEIDGERKEN)

OTHER ADDRESSES OF PEOPLE WHO PAID THE \$10 FEE:

PEOPLE WITH OBJECTIONS, COMMENTS OR REQUESTED COPY W/O \$10 (SEND THE \$10 LETTER):

CASEWORKER : CINDY SMITH

PFO AND FO NOTIFICATION LIST FOR FILE NUMBER:

IS-70251 BASIN # 6

| A DAVID CHILDS ,1806 T             | HOMPSON ST    | THE DALLES | ,OR,97058   |
|------------------------------------|---------------|------------|-------------|
| GILLIAM COUNTY SOIL AND WA, PO BOX | 206           | CONDON     | ,OR,97823   |
| MORROW COUNTY SOIL AND WAT, PO BOX | 127           | HEPPNER    | ,OR,97823   |
| OREGON DEPT OF FISH AND WI, PO BOX | 59            | PORTLAND   | , OR, 97207 |
| WATER FOR LIFE , PO BOX            | 12248         | SALEM      | , OR, 97309 |
| WATERWATCH OF OREGON , 213 SW      | ASH SUITE 208 | PORTLAND   | , OR, 97204 |

For some with long names or addresses, the complete name and address are located in the file. Those who receive the Departments weekly public notice do not receive additional notice.

# RECEIVED

FEB -1 1995

WATER RESOURCES DEPT. SALEM, OREGON

A David Childs 1806 Thompson St The Dalles, OR 97058 January 31 1995 503/ 298/1499

Mr Mike Mattick Instream Water Rights Water Resources Department Commerce Building 158 12 th Street NE Salem, Oregon, 97310-0210

Dear Mike.

The proposed instream water right, (application No. 70251) for Rock Creek Gilliam County is seriously flawed.

1 / The forty mile stream-reach described for the Instream Water Right is dry for much of its distance during August, September, and October.

2 / The stream reach above The Gage Station is also dry for much of its distance up to the divide during this period.

3./ The period of summer dry-up with no water was about 30 days at our former ranch below French Charlie In the era of 1900.

Interview (1976) and visit with Ethel Sprinkel. She was born on the ranch in 1888, and lived there until 1906. I asked, "When you were here, the creek never went dry did it?" She responded, " It went dry every August for about a month.

My father came to Rock Creek in 1903, lived with his mentor-family, Tip and Mrs Mobley, until 1910. Tip settled on Rock Creek near Olex in 1867. Father ranched In the community until his death in 1946. I was born in 1923 and started fishing with my Dad in 1927. I rode horseback for 3 miles and forded the creek twice each day riding to school at Olex. My mother, myself, and children went to grade school at Olex. My grandfather came to the area in 1881 and retired in his "new" home along its banks in 1898. (Earl Weatherford ranch 2 miles below Olex bridge.)

Rock Creek now is dry for long reaches every year with no water for any use. see notes and Photos.

Rock Creek reaches go dry every year:

From Wolf Hollow to near the Harper fish ladder (Mile 29 to mile 25)

From Olex bridge to a mile below French Charlie. (Mile 17 to mile 9)

From Rock Creek Station to Welp's Spring, about a mile above the mouth, the stream is dry annually . (Mile 7 to Mile 1)

Rock Creek goes nearly dry to dry every year in the five mile Reach between Whyte Park Gage, mile 40, and former Cayuse Gage station, mile 35, downstream. There are no out-of-stream withdrawals between these gage locations Both gages were in operation at the same time for the years 1976 to 1978. The Cayuse gage was installed in cooperation with the State Engineer in 1965 and operated through 13 years. It was taken out after the gage was operating at Whyte park.

Enclosed are copies and synopsis of the Cayuse records showing months that flows were not met. I've also included miscellaneous data and pictures.

My thinking and reasons for submitting objections to using the proposed flows for instream rights are:

First; these flows haven't existed in the last 60 years, if ever.

Second; I believe Rock Creek can again become a viable Trout and Steelhead rearing stream, but in order to get the cooperative effort, in the magnitude necessary, we will have to truly picture conditions as they are.

I would be happy to discuss the instream or additional proposals further.

Sincerely, Nauf Sale

| Rock Creek | stopped flowing        | Rock Creek started flowing |
|------------|------------------------|----------------------------|
| Year       |                        |                            |
| 1957       |                        | Prior to Dec 6             |
| 1959       | June 21                | Dec 12                     |
| 1960       | June 23                |                            |
| 1961       | June 16                | Dec 25                     |
| 1962       | June 20                |                            |
| 1963       | June 15                |                            |
| 1964       | June 22                | Dec 10                     |
| 1965       | June 10                | Nov 3                      |
| 1966       | May 4                  | Nov 18                     |
| 1967       | June 12                | Last week Jan 1968         |
| 1968       | April 2                | Nov 19                     |
| 1969       | June 27                | Dec 3                      |
| 1970       | May 20                 |                            |
| 1971       | June 24                |                            |
| 1972       | June 8<br>'waterspout' | After Nov 24               |
|            | June 15                |                            |
| 1973       | May 10                 |                            |
| 1974       | June 12                |                            |

David Childs' ranch below French Charlie: Notes from diary

# MAP OF THE LOWER SUBBASIN



Environmental Considerations.

· · · · · · ·

51

Rock Creek is intermittently dry in its lower reaches for several months during the summer and fall. Conversely, large fluctuations in runoff occur during the winter and early spring. During the dry period, water supplies for wildlife become very limited, and there is little available fish habitat either due to high water temperatures or the lack of flowing water.

From: Rock Creek Watershed Work Plan 1974 Gilliam and Morrow Counties, Oregon U.S. Department of Agriculture Soil Conservation Service

in the second Work Sheet

ž

Table indicates number of days per month proposed flows were met at Cayuse gage five miles downstream from Whyte gage within the 40 mile reach.

| D 658 | Propose              | μ0 m.       |             |              |             |    | / |
|-------|----------------------|-------------|-------------|--------------|-------------|----|---|
| (     | Mile<br>407<br>Flows | 4.7<br>July | 3.09<br>Aug | 2.47<br>SEDT | 2.72<br>Oct |    |   |
|       | 1966                 | 2           | 0           | 0            | 0           |    |   |
|       | 1967                 | 0           | 0           | 0            | 0           |    |   |
|       | 1968                 | 0           | 0           | 0            | 0           |    |   |
|       | 1969                 | 0           | .0          | 0            | 0           |    |   |
|       | 1970                 | 0           | 0           | 0            | 0           |    |   |
| (     | 1971                 | 4           | 0           | 0            | 0           | τ. |   |
|       | 1972                 | D           | D .         | 0            | 0           |    |   |
|       | 1973                 | 0           | 0           | 0            | 0           |    |   |
|       | 1974                 | 0           | 0           | 0            | 0           |    |   |
|       | 1975                 | Cu.         | 0           | 0            | 0           |    |   |
|       | 1976                 | 0           | 25          | 25           | 0           |    |   |
| (     | 1977                 | 0           | 1           | 0            | 0           |    |   |
|       | 1978                 | 0           | /           | 0            | 0           |    |   |

5-1

#### STATE OF OREGON

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

14-0474." Rock Creek above Cayuse Canyon, near Condon, Oreg.

Location .-- Lat 45°20'15", long 120°03'40", in MM4SW4 sec.3, T.3 S., R.22 E., on left bank about 200 ft below

county road bridge, 15 miles northeast of Condon, Gilliam County.

Records available .- April 12, 1965, to Sept. 30, 1966.

Gage. -- Water-stage recorder.

Extremes. -- Maximum discharge, 364 cfs Mar. 14 (gage height, 2.48 ft); no flow at times.

1965, 1966: Maximum discharge, that of Mar. 14, 1966; no flow at times.

Remarks .- Records good except for period of no gage-height record, which are poor.

CAYUSE 66-78

Discharge, in cubic feet per second for the year ending September, 30, 19..66

| Day               | Oct.    | Nov.    | Dec.    | Jan.    | Feb.  | Mar.   | April  | May     | June    | July  | Aug.  | Sept. |
|-------------------|---------|---------|---------|---------|-------|--------|--------|---------|---------|---|-------|-------|
| 1                 | 2.9     | 3.9     | 8.3     | 6.1     | 12    | 19     | 174    | 9.7     | 3.3     | 1.9   | . 0.2 | 0     |
| 2                 | 2.9     | 4.1     | 8.0     | 9.7     | 11    | 17     | 158    | 9.3     | 3.8     | 4.1   | :1    | 0     |
| 3                 | 2.9     | 4.3     | 0.9     | 12      | 12    | 14     | 121    |         | 3.8     | 3.8   | 0     | 0     |
|                   | 2.9     | i 5.1   | 0.9     | 12      | 11    | 14     | 98     | 1 ( 8.2 | 5.8     | 2.8   | Ō     | 0     |
| 5                 | 3.2     | 5.1     | 8.0     | 16      | 11    | 14     | 63     | 1 20    | 3.0     | 2.1   | 0     | 0     |
| 6                 | 2.8     | 5.1     | 8.3     | 26      | 11    | 16     | 74     | 7.1     | 3.8     | 1.6   | 0     | 0     |
| 7                 | 3.1     | 5.1     | 8.3     | 33      | 12    | 4 16   | 65     | 7.1     | 4.1     | 1.9   | 0     | 0     |
| 8                 | 3.1     | 5.3     | 5.1     | 29      | 12    | * 21   | 58     | 6.7     | 4.1     | 1.6   | 0     | 0     |
| 9                 | 3.1     | 5.5     | a 5.5   | 30      | 11    | 64     | 52     | 6.4     | 4.1     | 1.4   | C     | 0     |
| 10                | 3.1     | # 5.5   | a 5.5   | 23      | 11    | #2.02  | - 51   | 5.5     | 3.8     | 1.3   | 0     | 0     |
| 11                | 3.1     | 5.5     | a 5.5   | 21      | 10    | 114    | - 50   | 5.5     | 3.8     | 1.3   | 0     | 0     |
| 12                | * 3.2   | 5.8     | a 5.5   | 19      | 10    | 109    | * # 45 | 5.2     | 3.8     | 1.1   | 0     | 0     |
| 13                | 3.4     | 6.9     | a 5.5   | 18      | 10    | 217    | • 41   | - 5.0   | 3.6,    | 1.3   | .1    | 0     |
| 14                | 3.4     | 8.6     | a 5.5   | 17      | 10    | 266    | . 58   | 5.0     | 3.3     | 11  | .1    | 0     |
| 15                | 3.5     | 8.3     | a 5.5   | 17      | 10    | * 234  | - 20   | 5.0     | 2.5     | 6.7   | .1    | .4    |
| 16                | 3.5     | 8.6     | a 5.5   | 17      | 9.7   | 165    | · 29   | 5.0     | 2.4     | a 4   | * .1  | .6    |
| 17                | 3.5     | 8.3     | a 5.5   | 15      | # 10  | 104    | . 27   | 5.0     | 1.9     | a 3   | .1    | .6    |
| 18                | 3.7     | 8.3     | a 6     | 14      | 10    | 94     | - 26   | 4.4     | 1.9     | a 2   | 0     | .6    |
| 19                | 3.9     | 7.6     | a 6     | 14      | 10    | 89     | . 23   | # 4.1   | 1.9     | a 1   | C     | .6    |
| 20                | 3.9     | 7.2     | a 6.5   | # 13    | 11    | 81     | . # 22 | 3.8     | 1.6     | a 1   | 0     | .6    |
| 21                | 3.9     | 7.2     | * 6.7   | 13      | 11    | 69     | - 21   | 3.6     | 1.6     | a .5  | 0     | .4    |
| 22                | 3.9     | 7.2     | 5.5     | 14      | 12    | 58     | - 21   | 3.3     | 1.6     | a .5  | 0     | .4    |
| 23                | 3.9     | 7.6     | 4.7     | 13      | 14    | 58     | . 20   | 3.3     | 1.6     | a .5  | 0     | .2    |
| 24                | 3.9     | 8.6     | 7.8     | 13      | 16    | 59     | · 18   | 3.3     | 1.9     | a .4  | 0     | .2    |
| 25                | 3.9     | 10      | 6.4     | 13      | 18    | 87     | - 16   | 3.1     | 1.9     | a .4  | 0     | .2    |
| 26                | 3.9     | 10      | 6.7     | 13      | 21    | 144    | • 14   | 2.6     | 1.6     | a .2  | 0     | .2    |
| 27                | 3.9     | 9.6     | 7.1     | 13      | 20    | 198    | - 13   | 2.6     | # 1.4   | a .2  | .1    | .2    |
| 28                | 3.9     | 8.6     | 7.4     | 13      | 20    | 230    | . 12   | 2.6     | 1.3     | * .1  | .1    | .2    |
| 29                | 3.9     | 0.9     | 7.4     | 13      |       | 2 34   | . 11   | 2.6     | 1.1     | .2  | .1    | .2    |
| 20 1              | 3.91    | 0.3     | 1.4     | 13      |       | 2 30   | - 10   | 2.8     | 1.1     | .6  | * .1  | = .2  |
| 31                | 3.9     |         | 7.8     | 13      | -     | 195    |        | + 3.3   |         | .5  | .1    |       |
|                   | 1 080   |         | 2 C 4 9 |         | 346.7 |        | 1.4 C1 |         | 80.5    | and the second se | 1.3   |       |
|                   | Tech    | 5 C 8.9 |         | 5 C 5.P |       | 3.4 32 |        | 1 5 7.4 |         | 59.0  |       | 5.8   |
| Mean              | 3.48    | 6.96    | 6.61    | 16.3    | 12.4  | 111    | 46.7   | 5.08    | 2.68    | 1.90  | 0.04  | 0.19  |
| Acre              | 21/1    | 414     | 406     | 1,000   | 688   | 6,810  | 2,780  | 312     | 160     | 117   | 2.6   | 12    |
| Calend            | ar year | 1965    | Max     | -       | Min   | -      | Mean   | -       | Acre-ft | -   |       |       |
| Period<br>Water : | rear    | 1965-66 | Max     | 266     | Min   | 0      | Moan   | 17.8    | Acre-ft | 12,910  |       |       |

. Discharge measurement made on this day.

a No gage-height record.

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

JOHN DAY RIVER BASIN

5-2

14-0474. Rock Creek above Cayuse Canyon, near Condon, Creg.

Location .-- Lat 45°20'15", long 120"03'40", in Nw1SW1 sec. 3, T.3 S., R.22 E., on left bank about 200 ft downstream

from county bridge, 15 miles northeast of Condon, Gilliam County.

Records available .-- April 12, 1962, to Sept. 30, 1967.

Gage .-- Water-stage recorder.

84 

Extremes .-- Maximum discharge during year, 832 cfs Jan. 28 (gage height, 3.27 ft); no flow at times.

1965-67: Maximum discharge, that of Jan. 28, 1967; no flow at times.

Remarks .-- Records good except for period of no gage-height record, which are poor.

| Day    | Oct.  | Nov.    | Dec.  | Jan.    | Feb.    | Mar.  | April  | May   | June    | July  | Aug.  | Sept. |
|--------|-------|---------|-------|---------|---------|-------|--------|-------|---------|-------|-------|-------|
| 1      | 0.4   | 1.4     | 25    | 32      | * 2 3 6 | 48    | 63     | 240   | 21      | 2.0   | 0.2   | 0     |
| 2      | .4    | 1.4     | 58    | 32      | 195     | 51    | 89     | 240   | 19      | 1.9   | 2. 44 | C     |
| 3      | .4    | 1.4     | 51    | * 30    | 169     | 47    | 1 C 4  | SCE   | 16      | 1.6   |       | C     |
| 4      | .4    | 1.6     | 47    | 29      | 156     | 39    | 117    | 179   | 13      | 1.2   |       | 0     |
| 5      | .4    | 1.0     | 52    | 35      | 142     | 39    | 119    | 153   | 12      | a 1.2 | .1    | 0     |
| 6      | .4    | 2.4     | * 52  | 36      | 119     | 41    | 125    | 1 38  | 5.5     | 1 1 1 | .1    | č     |
| 7      | .4    | 2.4     | 50    | 25      | 110     | 30    | 1 50   | 1 2 3 | 5.5     | 1 1   | 1     | õ     |
| 8      | .4    | 2.4     | 46    | 22      | 100     | 30    | 1 2 1  | 1 1 4 | 22      | 11    | .1    | õ     |
| 9      | .2    | 2.4     | 40    | 30      | 95      | 42    | 1 10   | 112   | 6.4     | 1.1   | .1    | C     |
| 10     | .4    | 2.0     | 4 1   | 31      | E 3     | 42    | 140    | 112   | 45      | 0     | .1    | 0     |
| 11     | .4    | 2.5     | 70    | 36      | 71      | 38    | 125    | 9.9   | EI      | £     | .1    | C     |
| 12     | .4    | a 7     | 256   | 30      | 70      | 42    | 110    | 94    | 9       | .5    | .1    | 0     |
| 1.3    |       | a1 C    | 290   | 81      | 66      | 38    | 104    | 80    | 5.7     | .5    | .1    | .1    |
| 15     | , o   | a15     | 142   | 142     | 59      | 34    | 1 C O  | 70    | 5.0     | .5    | .1    | .1    |
| 16     | 9     | aze     | 100   | 181     | 54      | 34    | 96     | 62    | 4.7     | .4    | 1     | .1    |
| 17     |       | a15     | 79    | 123     | 54      | 91    | 91     | 54    | 4.1     | .4    | 0     | .1    |
| 18     | 1.0   | alC     | 67    | 94      | 66      | 100   | 94     | 49    | 3.4     | .4    | 0     | .1    |
| 19     | 9     | 240     | 61    | 76      | 58      | 87    | 69     | 45    | 3.1     | .4    | 0     | -1    |
| 20     | .0    | a1 50   | 57    | 69      | 46      | 60    | 78     | 40    | 2.5     | .4    | 0     | .1.   |
| 21     | 1.3   | a 70    | 57    | 1 06    | 51      | 95    | 71     | 3 30  | 2.4     | -4    | č     | -1    |
| 22     | 1.6   | a 50    | 46    | 19      | 44      | 110   | 60     |       | 10      | 4     | ö     | .1    |
| 23     | 1.6   | a 40    | 35    | 64      | * 51    | 1 04  | 75     | 15    | 76      | .3    | č     | .1    |
| 24     | 1.6   | asc     | 37    | 65      | 51      | 87    | 145    | 23    | 57      | .3    | č     | .1    |
| 25     | 1.6   | azo     | 51    | 62      | 51      | 76    | #153   | 21    | 4.7     | .2    | C     | .1    |
| 26     | * 1.6 | a 20    | 26    | 70      | 43      | 71    | 166    | 18    | 4.1     | .2    | 0     | .1    |
| 21     | 1.4   | - 15    | 25    | 368     | 45      | 68    | 175    | 18    | 3.8     | .2    | C     | .1    |
| 20     | 1.4   | # 19    | 32    | 731     |         | 75    | 148    | 21    | 3.1     | .2    | 0     | .1    |
| 20     | 1.4   | 24      | 35    | 483     |         | 78    | 145    | 22    | 2.5     | .2    | 0     | .2    |
| 31     | 1.4   |         | 32    | 3 C 5   |         | *76   |        | 21    |         | .2    | 0     |       |
| Total  | 27.4  |         | 2.033 |         | 2.4 1 1 |       | 3.3 56 |       | 2 1 9.9 |       | 2.0   |       |
|        |       | 6 C 6.2 |       | 3.6 1 0 |         | 1.943 |        | 2.576 |         | 21.6  |       | 1.8   |
| Mean   | 0.88  | 20.2    | 65.6  | 116     | 86.1    | 62.7  | 112    | 83.1  | 7.33    | 0.70  | 0.06  | 0.06  |
| Max    | 1.6   | 150     | 290   | 731     | 236     | 110   | 175    | 240   | 21      | 2.0   | .2    | 0.2   |
| Min    | 0.2   | 1.4     | 25    | 29      | 43      | 34    | 68     | 16    | 2.5     | 0.2   | 0     | 0     |
| Ac-ft  | 54    | 1,200   | 4,030 | 7,160   | L,780   | 3,850 | 6,660  | 5,110 | L36     | 43    | 4.0   | 3.6   |
| Cal yr | 1966  | Mean    | 23.7  | Max     | 290     | Min   | 0      | Ac-ft | 17,170  |       |       |       |
| ktr yr | 1967  | Hean    | 46.0  | Max     | 290     | Min   | 0      | Ac-ft | 33,340  |       |       |       |

Discharge, in cubic feet per second for the year ending September, 30, 1967 ...

Discharge measurement made on this day. \*\* Field estimated made on this day. a No gage-height record.

#### JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

Location -- Lat h5\*20'15", long 120\*03'h0", in NW4SW4 sec.3, T.3 S., R.22 E., on left bank about 200 ft downstream from

county bridge, 15 miles northeast of Condon, Gilliam County.

Records available .-- April 12, 1965, to Sept. 30, 1968.

Gage .--- Water-stage recorder.

·, · · · · 90

Extremes .-- Maximum discharge during year not determined; no flow at times.

1965-68: Maximum recorded discharge, 832 cfs Jan. 28, 1967; no flow at times.

Remarks .- Records good except for periods of ice effect or no gage-height record, which are poor.

Revisions .-- The maximum daily discharge for water year 1967 is corrected to 731 cfs.

| Day  | Oct.   | Nov.  | Dec.  | Jan.   | Feb.   | Mar.   | April   | May  | June  | July  | Aug.                                    | Sept.                                   |
|--|--|---|---|--|--|--|---|--|---|---|---|---|
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13                            | е е е е е е е е е е е е е е е е е е е  | a 0.9<br>a 9<br>a 9<br>a 9<br>a 9<br>a 9<br>a 9<br>a 10<br>a 10<br>a 111<br>a 112<br>a 12<br>a 12 | a 1.4<br>a 1.6<br>a 2.0<br>a 2.3<br>* 2.8<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 1.5<br>a 1.5<br>a 1.4<br>a 1.2 | a 7<br>a 6<br>*b 5<br>a 4<br>*b 25<br>b 3.0<br>b 3.0<br>b 3.0<br>b 3.5<br>b 4.0<br>b 4.5<br>b 4.5<br>6.3 | 165<br>* 157<br>290<br>225<br>225<br>225<br>225<br>225<br>225<br>225<br>23<br>24<br>29<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25 | 374<br>29<br>* 275<br>224<br>221<br>221<br>221<br>221<br>221<br>221<br>221<br>221<br>221                 | * 9.6<br>10<br>9.6<br>10<br>9.6<br>9.6<br>9.2<br>8.0<br>7.1<br>6.3<br>6.3<br>6.3                      | 4.2<br>3.8<br>3.4<br>3.1<br>3.4<br>3.4<br>3.1<br>2.8<br>2.4<br>2.4<br>2.4<br>2.4   | 3.1<br>3.1<br>3.1<br>* 2.8<br>2.4<br>2.2<br>2.4<br>2.0<br>2.0<br>2.0<br>1.7<br>1.9<br>2.0<br>1.9        | * 0.6<br>a a 3<br>a a 2<br>a a 1<br>a a 1<br>a a 1<br>a a 0 |   |   |
| 14<br>15   | a 2<br>a 2   | a 1.2<br>a 1.2  | a 1.0   | . 18   | a 11<br>a 11   | 18   | 5.9   | / 2.4  | 1.7   | a 0 /   |   |   |
| 16<br>17<br>18<br>19<br>20<br>21<br>22<br>23<br>24<br>25<br>26<br>27<br>28<br>29<br>30<br>31 | a 22<br>a 22<br>a 22<br>a 22<br>a 23<br>a 24<br>a 5<br>a 5<br>a 5<br>a 6<br>a 6<br>a 6<br>a 15<br>a 15<br>a 11 | a 13<br>a 13<br>a 13<br>a 13<br>a 13<br>a 13<br>a 13<br>a 13                                      | a 8<br>a 8<br>a 9<br>a 10<br>a 13<br>a 16<br>a 22<br>a 26<br>a 40<br>a 17<br>a 25<br>a 15<br>a 10<br>a 90         | 49<br>31<br>22<br>19<br>16<br>25<br>70<br>46<br>36<br>30<br>b12<br>b 9<br>b10<br>b12<br>b14              | a 11<br>a 12<br>a 14<br>a 17<br>a 25<br>a 120<br>a 280<br>a 90<br>a 280<br>a 90<br>a 60<br>a 55<br>a 50<br>a 45<br>a 40  | 16<br>b 14<br>b 13<br>b 13<br>15<br>14<br>14<br>13<br>12<br>12<br>14<br>14<br>16<br>14<br>13<br>12<br>14 | 5.9<br>5.9<br>5.6<br>5.6<br>5.6<br>5.6<br>5.6<br>5.9<br>5.6<br>5.6<br>5.6<br>5.6<br>5.6<br>4.8<br>4.5 | 2.0<br>2.0<br>1.9<br>5.2<br>4.2<br>4.5<br>3.8<br>4.2<br>4.8<br>4.8<br>4.8<br>4.8<br>4.8<br>4.8<br>4.8<br>4.8<br>4.8<br>4.8 | 15<br>15<br>13<br>13<br>13<br>13<br>11<br>10<br>11<br>11<br>11<br>11<br>13<br>6<br>.5<br>.5<br>.6<br>.6 |   |   |   |
| Total<br>Mean<br>Max<br>Min<br>Ac-ft   | 12.2<br>0.39<br>1.5<br>0.2<br>24   | 34.8<br>1.16<br>1.3<br>0.9<br>69  | 1 2 6.0<br>4.06<br>25<br>0.8<br>250   | 4 9 1.8<br>15.9<br>70<br>2.5<br>975  | 1.162<br>li0.1<br>280<br>11<br>2,300   | 5 6 8<br>18.3<br>37<br>10<br>1,130   | 2 0 5.9<br>6.86<br>10<br>4.5<br>408   | 1 0 5.6<br>3.41<br>5.2<br>1.9<br>209   | 4 8.6<br>1.62<br>3.1<br>0.5<br>96   | 3.0<br>0.10<br>0.6<br>0<br>6.0                              | 000000000000000000000000000000000000000 | 000000000000000000000000000000000000000 |
| Cal 77<br>Wir 77   | 1967 : 1<br>1968 : 1   | Mean 39.2<br>Mean 7.5   | 2 Max   | 731<br>280   | M<br>M   | a 0<br>a 0   | Ac-   | n 28,<br>n 5,  | 390<br>470  |   |   |   |

Discharge, in cubic feet per second for the year ending September 30, 1968.

\* Discharge measurement made on this day.

a No gage-height record.

#### STATE OF OREGON OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

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#### JOHN DAY RIVER BASIN

# 14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION.--Lat 45°20'15", long 120°03'40", in NWESWE sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

PERIOD OF RECORD. -- April 12, 1965, to current year.

GAGE.--Water-stage recorder.

EXTREMES.--Current year: Maximum discharge, 1,010 cfs June 10 (gage height, 3.69 ft); minimum observed, 0.1 cfs Oct. 2 (gage height, 0.67 ft); and may have been no flow sometime Oct. 1.

Period of record: Maximum recorded discharge, 1,010 cfs June 10, 1969 (gage height, 3.69 ft); no flow at times. REMARKS .-- Records good except for periods of no gage height record, which are poor.

Discharge, in cubic feet per second for the year ending September 30, 1969

| Day    | Uct.        | Nov.         | Dec.   | Jan.   | Feb.  | Mar.   | April   | May     | June    | July       | Aug. | Sept.            |
|--------|-------------|--------------|--------|--------|-------|--------|---------|---------|---------|------------|------|------------------|
| 1      | a .1        | a .5         | a 1 0  | b 2.0  | b 24  | 65     | * 665   | 8 5     | 10      | * 7.7      | .4   | .3               |
| 2      | * 2         | a .8         | a 1 3  | b 2.0  | b 24  | 62     | 542     | 82      | 8       | 7.7        | .4   | .3               |
| 3      | .3          | a 1.5        | a 1 8  | b 2.0  | b 26  | 65     | 415     | 75      | 7.4     | 7.4        | .4-  | .3               |
| 4      | a .3        | a .9         | *23    | b 2.5  | b 30  | 62     | 390     | 70      | 6.5     | 6.8        | .4   | .3               |
|        | <u>a .3</u> | a .7         | 24     | b 3.0  | - 35  | 6.8    | 440     | 61      | 5.9     | 6.8        | .4   | 3                |
| 6      | a .4        | a .7         | 24     | b 4.0  | 30    | 18     | 446     | 54      | 5.9     | 6.8        | ••   | .3               |
| 7      | a .4        | a ./         | 23     | D 7.0  | . 40  | 7 1    | 395     | 49      | 21.9    | 5.6        | .4   | .3               |
| 8      | a .4        | *1.1         | 29     | D 9.1  | 42    | 7 0    | 350     | 44      | + 27    | 5.5        | .4   | .3               |
| 9      | a .2        | a 5.0        | 71     | b 30   | 4.5   | 65     | 175     | 34      | 127     | 5.0        | .4   |                  |
| - 10   | <u>a .2</u> | <u>a</u> 4.) | 1 4 5  | b 60   | 111   | 7.0    | 320     | 31      | 121     | 4.4        |      |                  |
| 11     | a .0        | 2 50         | 85     | 105    | 442   | 6.6    | 296     | 28      | a 20    | 30         |      |                  |
| 12     | a 2.0       | a 4.5        | 62     | 130    | 282   | 71     | 268     | 26      | a 17    | 3.6        |      |                  |
| 14     | a 1.0       | a 4.0        | 52     | 171    | 204   | 80     | 228     | 25      | a 14    | 3.6        |      |                  |
| 15     | a 9         | a 3.5        | 4 5    | 119    | 165   | 8 9    | 199     | 28      | a 12    | 3.3        | .3   |                  |
| 16     | a 9         | a 4.5        | 4 5    | 107    | 148   | 130    | 172     | 26      | a 10    | 2.8        | .3 ' | 4                |
| 17     | a .9        | a 5.6        | 38     | 99     | 140   | 218    | 163     | 22      | a 9.0   | * 2.5      | 3    | .4               |
| 18     | a .9        | a 8.0        | 34     | 76     | 128   | 436    | 232     | 20      | a 9.0   | 2.2        | * .3 | 3.0              |
| 19     | a .9        | a12          | 29     | 80     | 115   | 274    | 181     | * 27    | a 8.0   | 2.0        | .3   | 2.0              |
| 20     | a .9        | a10          | 26     | 7 1    | 101   | 242    | 155     | 33      | * 6.8   | 1.7        | .3   | 1.7              |
| 21     | a .9        | a 9.0        | 12     | * 65   | 93    | 282    | * 1 4 0 | 30      | 6.2     | 1.5        | .3   | 1.3              |
| 22     | a .8        | a 7.0        | b15    | 36     | 78    | 358    | 135     | 25      | 6.2     | 1.5        | .3   | * 1.1            |
| 23     | · a .8      | a 5.0        | b 2 0  | b 32   | 78    | 481    | 132     | 19      | 7.7     | 1.3        | .3   | 1.1              |
| 24     | a .7        | a 5.0        | b 2 5  | b 30   | 60    | 406    | 148     | 16      | 10      | 1.3        | .3   | .9               |
| 25     | a .7        | a 4.0        | b30    | b 28   | 6 ?   | *376   | 148     | 14      | 12      | 1.1        | .3   | .9               |
| 26     | a .5        | a 3.0        | b15    | b 26   | 60    | 495    | 118     | 15      | 9.2     | .9         | .3   | .9               |
| 27     | a .4        | a 3.0        | b 8.0  | b 25   | 53    | 632    | 100     | 18      | 8.6     | .9         | .3   | .9               |
| 28     | a .4        | a 3.0        | b 7.0  | b 24   | * 65  | 221    | 92      | 19      | 8.0     | .8         | .3   | .9               |
| 29     | a .4        | a 4.0        | b 5.0  | b 24   |       | 696    | 125     | 16      | 8.0     | .8         | .)   | .9               |
| 30     | a .4        | a 7.0        | b 4.0  | D 24   |       | 136    | 100     | 14      | 8.6     | .6         | .3   | .9               |
| 31     | a .4        |              | 1.9    | b 24   |       | 194    |         | 12      |         | .4         | .3   |                  |
| Total  | 100         | 1289         | 9849   | 1.4375 | 2731  | 8.172  | 7.8 5 5 | 1.0 5 7 | 4 4 5.9 | 1044       | 102  | 21.8             |
| Mann   | 0.64        | 4.30         | 31.8   | 46.4   | 97.5  | 264    | 262     | 34.1    | 14.9    | 3.37       | 0.33 | 0.73             |
| Max    | 2.0         | 12           | 145    | 171    | 442   | 794    | 665     | 85      | 127     | 7.7        | 0.4  | 3.0              |
| tin    | 0.1         | 0.5          | 1.9    | 2.0    | 24    | 62     | 92      | 12      | 5.9     | 0.4        | 0.3  | 0.3              |
| Ac-ft  | 39          | 256          | 1,950  | 2,850  | 5,420 | 16,210 | 15,580  | 2,100   | 884     | 207        | 20   | 43               |
| Cal yr | 1968 :      | Mean 10      | .2 Max | x 280  | ) Mi  | in C   | Ac-     | rt 7,38 | 0       | an an an a |      | 1 4 - 1 81 - 1 4 |

\* Discharge measurement made on this day.

a No gage height record.b Stage-discharge relation affected by ice.

# STATE OF OREGON

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION.--Lat 45°20'15", long 120°03'40", in NW1SW1 sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

PERIOD OF RECORD. -- April 12, 1965, to current year.

GAGE.--Water-stage recorder.

· ..

EXTREMES.--Current year: Maximum discharge, 2,420 cfs Jan. 23 (gage height, 4.73 ft); minimum, 0.1 cfs Aug. 25, 26

(gage height, 0.73 ft).

Period of record: Maximum recorded discharge, 2,420 cfs Jan. 23, 1970 (gage height, 4.73 ft); no flow at times. REMARKS.--Records good.

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| Day   | Oct.  | Nov.  | Dec. | Jan.    | Feb.    | Mar.    | April   | May     | June  | July  | Aug. | Sent. |
|-------|-------|-------|------|---------|---------|---------|---------|---------|-------|-------|------|-------|
| 1     | 0.9   | 3.3   | 4.4  | 8.6     | 157     | 67      | 93      | 4 3     | 7.5   | 26    | 0.5  | 0.0   |
| 2     | .9    | 3.3   | 4.2  | 8.0     | 138     | 74      | 87      | 39      | 6.8   | 2.0   | 0.5. | 0.2   |
| 3     | 1.1   | 3.3   | 3.9  | 6.2     | 128     | 72      | 79      | 35      | 5.8   | 2.4   |      |       |
| 4     | 1.1   | 3.6   | 4.2  | 6.8     | 107     | 70      | 74      | 33      | 4.8   | 29    | .0   |       |
| 5     | 1.1   | 4.4   | 4.4  | 4.4     | 101     | 72      | 72      | 32      | 4.1   | 2.2   |      |       |
| 6     | 1.1   | 4.7   | 4.4  | 7.1     | 112     | 97      | 74      | 29      | 4.1   | 1.8   | 4    |       |
| 7     | 1.1   | 4.7   | 4.7  | 7.1     | 203     | 355     | 76      | 29      | 4.8   | 1.6   |      | 1.0   |
| 8     | 1.1   | 4.7   | 4.4  | 8.0     | 192     | 350     | 72      | 27      | 6.5   | 1.6   | 4    | 1.0   |
| 9     | 1.1   | 4.7   | 4.4  | 22      | 172     | 234     | 67      | 35      | 7.5   | 1.6   | 4    | 1.0   |
| 10    | 1.1   | 4.4   | 4.4  | 78      | 154     | 186     | 72      | 39      | -8-0  | 1.4   | 4    | 12    |
| 11    | 1.1   | 4.4   | 5.0  | 52      | 148     | 160     | 76      | 35      | 8.4   | 1.2   | 3    | 12    |
| 12    | 1.1   | 4.4   | 5.6  | 121     | 145     | 157     | 67      | 33      | 8.4   | 1.2   | 3    | 12    |
| 13    | .9    | 4.4   | 5.9  | 53      | 365     | 157     | 60      | 36      | 10    | . 1.4 |      | 12    |
| 14    | .9    | 4.4   | 6.2  | 58      | 3 0 5   | 217     | 56      | 31      | 11    | 1.2   | 2    | 14    |
| 15    | .9    | 4.4   | 6.5  | 55      | 242     | 281     | 52      | 26      | 12    | 1.0   | 2    | 1.4   |
| 16    | 1.5   | 4.4   | 7.1  | 60      | * 217   | * 234   | 47      | 23      | *     | 1.0   | 2    | 1.4   |
| 17    | 1.5   | 4.4   | 6.8  | 60      | 317     | 224     | 47      | 20      | . 9.2 | .8    | * 2  | 1 4   |
| 18    | 1.5   | * 4.4 | 7.7  | 157     | 228     | 189     | 4 3     | 19      | 7.5   | .6    | 2    | 1.4   |
| 19    | 1.3   | 4.4   | 8.0  | 232     | 178     | 160     | 46      | 18      | 6.1   | .6    | 2    | 1.4   |
| 20    |       | 4.4   | 10   | * 3 3 2 | 160     | 145     | 48      | 16      | 5.5   | * .6  | .1   | 1.4   |
| 21    | 1.3   | 4.2   | 21   | 242     | 145     | 135     | # 46    | 14      | 4.4   | .5    | .1   | 1.6   |
| 22    | 1.3   | 4.2   | 34   | 1000    | 1 3 0   | 120     | 43      | *13     | * 3.5 | .5    | i    | 1.4   |
| 23    | . 1.3 | 4.2   | * 28 | 1.090   | 114     | 112     | 41      | 12      | 3.2   | .6    | .1   | * 16  |
| 24    | 1.5   | 4.2   | 21   | 640     | 105     | 105     | 39      | 1       | 32    | .6    | .1   | 1.6   |
| 25    | 1.2   | 4.4   |      | 040     | 91      | 99      | 40      | (9.8)   | 2.9   | .8    | .1   | 1.6   |
| 26    | 1.1   | 4.4   | 13   | 680     | 91      | 91      | 42      | er      | 2.6   | .8    | .1   | 1.6   |
| 27    | * 2.0 | 4.4   | 13   | +165    | 87      | 93      | 4 7     | 8.0     | 2.9   | 1.0   | .1   | 1.6   |
| 28    | 2.2   | 4.4   | 14   | 325     | 0 ?     | 91      | 4 5     | 1.5     | 2.0   | .8    | .1   | 1.6   |
| 29    | 2.2   | 4.4   | 10   | 245     |         | 89      | 4 2     | 8.C     | 2.0   | .8    | .1   | 1.4   |
| 30    | 2.0   | 4.4   | 10   | 200     |         | 93      | 4 2     | 8.4     | 2.9   | .8    | .2   | 1.4   |
| 31    | 3.0   |       | 9.2  | 200     |         | 107     |         | 8.4     |       | .6    | .2   |       |
|       | 127   | 1293  | 3014 | 01000   | 4622    | 4622    | 1720    | 7000    |       |       |      |       |
|       | - 3.1 | 1 20  | 0.72 | 0.102.2 | 4.0 2 3 | 4.0 3 3 | 1.1.3.9 | 1 0 6.5 | 179.9 | 3 8.1 | 8.0  | 3 6.2 |
| can   | 1.41  | 4.20  | 9.12 | 264     | 165     | 149     | 58.0    | 22.8    | 6.00  | 1.23  | 0.26 | 1.21  |
|       | 3.0 1 | 4.1   | 34   | 1,660   | 365     | 355     | 93      | 43      | 12    | 2.9   | 0.6  | 1.6   |
|       | 0.9   | 3.3   | 3.9  | 4.4     | 85      | 67      | 39      | 7.5     | 2.6   | 0.5   | 0.1  | 0.2   |
| and 1 | . 8/  | · 254 | DA8  | 16,230  | 9,170   | 9,190   | 3,450   | 1,400   | 357   | 76    | 16   | 72    |

\* Discharge measurement made on this day.

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### STATE OF OREGON

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

JOHN DAY RIVER BASIN

#### 14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION.--Lat 45°20'15", long 120°03'40", in NWESWE sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

DRAINAGE AREA. -- 350 sq mi.

PERIOD OF RECORD. -- April 12, 1965 to current year.

GAGE .-- Water-stage recorder.

AVERAGE DISCHARGE .-- 6 years (1965-71), 37.7 cfs (27,310 acre-ft per year).

EXTREMES.--Current year: Maximum discharge, 774 cfs Jan. 20 (gage height, 3.52 ft); no flow Aug. 6-27.

Period of record: Maximum recorded discharge, 2,420 cfs Jan. 23, 1970 (gage height, 4.73 ft); no flow at times. REMARKS .-- Records good.

| Discharge, in cubic feet | per second for | the year ending | September 30, | 1971 |
|--------------------------|----------------|-----------------|---------------|------|
|--------------------------|----------------|-----------------|---------------|------|

| Day   | Oct.     | Nov.    | Dec.   | Jan.      | Feb.    | Mar.  | April   | May   | June  | July  | Aug. | Sept. |
|-------|----------|---------|--------|-----------|---------|-------|---------|-------|-------|-------|------|-------|
| 1     | 1.4      | 2.4     | 11     | 12        | 117     | 30    | 142     | 58    | 20    | 2.6   | 0.1  | 0.2   |
| 2     | 1.4      | 2.4     | 13     | 6.8       | 101     | 25    | 133     | 54    | 22    | 2.3   | .1   | .3    |
| 3     | 1.4      | 2.6     | 13     | b 6.0     | 77      | 33    | 126     | 50    | 18    | 1.8   | .1   | • .3  |
| 4     | 1.2      | 2.6     | 11     | b 5.4     | 74      | 30    | 122     | 44    | 18    | 1.5   | .1   | .4    |
| 5     | 1.2      | 2.9     | 11     | b 5.0     | 59      | 25    | 145     | 40    | 16    | 1.3   | .1   |       |
| 6     | 1.2      | 3.2     | 11     | b 5.8     | 44      | 25    | 126     | 38    | 14    | 1.3   | 0    | .4    |
| 7     | 1.4      | 3.8     | 19     | ь 7.0     | , 43    | 28    | 124     | 34    | 12    | 1.0   | 0    | .5    |
| 8     | 1.0      | 4.1     | 48     | 510       | 43      | 24    | 103     | 30    | 11    | .9    | 0    | 5     |
| 9     | 1.0      | 4.1     | 39     | 13        | 4 3     | 26    | 99      | 27    | 10    | 1.0   | 0    | .5    |
| 10    | 1.0      | 4.1     | 29     | 24        | 4.8     | 25    | 97      | 25    | 10    | 2.0   | 0    |       |
| 11    | 1.4      | 5.8     | 24     | 33        | 67      | 2 A   | 90      | 22    | 10    | 2.0   | 0    |       |
| 12    | 1.4      | 5.8     | 20     | 29        | 6.2     | 44    | 84      | 20    | 10    | 1.5   | 0 .  | .5    |
| 13    | 1.4      | 6.5     | 15     | 22        | 60      | 50    | 76      | 55    | 9.6   | 1.0   | 0    | .4    |
| 14    | 1.4      | 6.5     | 18     | 28        | 59      | 43    | 69      | 23    | 8.3   | .8    | 0    |       |
| 15    | 1.4      | 6.5     | 18     | 32        | 67      | .4 3  | 65      | 21    | 7.4   | • .8  | 0    | .4    |
| 16    | 1.4      | * 5.8   | 18     | 89        | 64      | 31    | 60      | 22    | 6.7   | ./    | 0    | .4    |
| 17    | 1.4      | 5.8     | 16     | 480       | 24      | 34    | 65      | 20    | 5.0   | .7    | 0    | .4    |
| 18    | 1.7      | 6.5     | 11     | 610       | 50      | * 32  | 70      | 18    | 6.7   | 7     | 0    | .4    |
| 19    | 1.4      | 6.2     | 12     | 214       | 40      | 32    | 65      | 11    |       | .6    | 0    | .4    |
| 20    | 1.0      | 6.1     | 14     | 218       | 43      | 33    | * 28    | 10    | 1.4   | 0. *  | 0    |       |
| 21    | 1.0      | 0.0     | * 13   | 232       | 10      | 31    | 69      | 10    | 5.0   | -2    | 0    |       |
| 22    | 1.6      | 2.2     | 13     | 1 28      | * 40    | 4 8   | 93      | 12    | 20    | .4    | 0    | * -   |
| 23    | 1.6      | 0.1     | 1.2    | 1 3 1     | 4.3     | 140   | 101     | 1 9   | 0.5   | .4    | 0    |       |
| 24    | 1.0      |         | 12     | 113       | 4 4     | 330   | 101     | 1 2   | 2.6   | .4    | 0    | -     |
| 25    | 1.0      | 10      | 12     | 99        | 4 3     | 210   | 92      | * 1 2 | * 3.0 |       | 0    |       |
| 26    | 2.0      | 10      | 1 2    | * 7 .     | 25      | "5 00 | 93      | 27    | 2.2   |       | 0    | .0    |
| 27    | 2.0      | 11      | 12     | 95        | 10      | 310   | 83      | 27    | 2.2   |       | 0    |       |
| 28    | * 2.0    |         | 12     | 70        | 50      | 216   | 14      | 20    | 3.3   | 2     |      |       |
| 29    | 2.0      |         | 11     | 8.2       |         | 219   | 0 9     | 12    | 3.0   | .2    |      | -     |
| 30    | 22       | 1.1     | 12     | 111       |         | 216   | 0 2     | 1.4   | 3.3   | -<    |      |       |
| 31    | 6.4      |         | 12     |           |         | 177   | -       | 1 4   |       | .1    | .1   |       |
| otal  | 4 8.4    | 201.4   | 501.8  | 3.7 8 4.0 | 1.5 2 4 | 3,116 | 2.7 5 8 | 784   | 272.6 | 2 8.4 | 0.9  | 1 4.1 |
| fean  | 1.56     | 6.71    | 16.2   | 122       | 54.4    | 101   | 91.9    | 25.3  | 9,10  | 0.92  | 0.01 | 0.43  |
| fax   | 2.2      | 16      | 48     | 610       | 117     | 500   | 145     | 58    | 22    | 2.6   | 0.1  | 0.1   |
| tin   | 1.2      | 2.4     | 9.8    | 5.0       | 30      | 24    | 58      | 12    | 3.3   | 0.1   | 0    | 0.1   |
| c-ft  | 96       | 399     | 995    | 7,510     | 3,020   | 6,180 | 5.470   | 1,560 | 541   | 56    | 1.8  | 21    |
|       |          |         |        |           | -10-00  |       | -1.00   | .,    |       | 201   | 1.0  |       |
| al yr | 1970 : 7 | Mean 57 | .3 Mas | × 1.66    | 0 MI    |       | Ac-ft   | 41.4  | 50    |       |      |       |
| tr vr | 1071 : 2 | Mean 3  | 7 May  |           | 0 11    |       | 40.0    | 25.0  | 150   |       |      |       |

Discharge measurement made on this day.
 b Stage-discharge relation affected by ice.

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION.--Lat 45°20'15", long 120°03'40", in NW±SW± sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

DRAINAGE AREA. -- 350 sq mi.

PERIOD OF RECORD. -- April 12, 1965 to current year.

GAGE.--Water-stage recorder.

AVERACE DISCHARGE. -- 7 years (1965-72), 41.6 cfs (30,140 acre-ft per year).

EXTREMES .-- Current year: Maximum discharge, 12,500 cfs June 8 (gage height, 8.57 ft); no flow at times.

Period of record: Maximum recorded discharge, 12,500 cfs June 8, 1972 (gage height, 8.87 ft); no flow at times. REMARKS. -- Records good.

| Day    | Oct.     | Nov.    | Dec.   | Jan.    | Feb.  | Mar.    | April | May     | June      | July   | Aug. | Sept. |
|--------|----------|---------|--------|---------|-------|---------|-------|---------|-----------|--------|------|-------|
| 1      | 8.0      | 2.0     | 43     | ь 18    | b 4 4 | 278     | 80    | 40      | 6.8       | a 0.5  | 0    | О     |
| 2      | .7       | 2.0     | 34     | b 1 7   | 4 5   | 218     | 78    | 3 9     | 6.1       | a .5   | 0    | 0     |
| 3      | .7       | 2.0     | 32     | 16      | 4 5   | 395     | 74    | 3:      | 6.1       | a .5   | 2    | 0     |
| 4      | .7       | 2.3     | 28     | 15      | 60    | 294     | 72    | 30      | 6.1       | a .5   | 0    | 0     |
| 5      | .7       | 2.3     | 28     | b 1 6   | 80    | 290     | 78    | 28      | 6.1       | a .5   | 0    | 2     |
| 6      | .7       | 2.3     | 147    | 618     | 88    | * 3 1 4 | 80    | 25      | 20        | a .6   | 0    | 0     |
| 7      | .6       | 2.6     | 101    | P 55    | 86    | 266     | 32    | 23      | 1. 2. 0.4 | a .7   | 0    | 0     |
| 8      | .6       | 2.6     | 69     | . 21    | * 90  | 222     | 74    | 30      | 1.200     | a 1.0  | 0    | 0     |
| 9      | .6       | 2.6     | 500    | 0 20    | 80    | 218     | 00    | 4.7     | 3.640     | a .8   | 0    | 0     |
| 10     | 0.       | 7.0     | 650    | + 27    | 0 /   | 298     | 57    | 26      | a 30      | a ./   | 0    | 0     |
| 11     | .0       | 10      | 645    | 1 27    | 55    | 330     | 50    | 20      | a 20      | a .0   | 0    | 0     |
| 12     | .7       | 4.3     | 542    | b 27    | . 72  | 550     | 6 4   | 25      | 3 80      | a # .0 | 0    | 0     |
| 1.5    | .1       | 43      | 630    | b 28    | 92    | 136     | 72    | 22      | 2 60      | a .0   | 0    | 0     |
| 15     |          | 4.6     | b 3 8  | b 28    | 84    | 310     | 8.6   | 19      | a + 5.0   | - 5    | 0    | 0     |
| 16     | .0       | 5.0     | # 3.8  | b 29    | 145   | 278     | 92    | 18      | 3.8       | a .5   | 0    | 0     |
| 17     | .9       | 5.3     | 35     | 31      | 270   | 266     | 98    | 16      | 3.2       | a .4   | ő    | 0     |
| 18     | .9       | * 5.C   | 37     | 34      | 278   | 2 5 0   | 90    | 17      | 2.2       | a .4   | 0    | õ     |
| 19     | 1.0      | 5.0     | 38     | 74      | 258   | 212     | 84    | 18      | 1.5       | .4     | 0.6  | õ     |
| 20     | * 1.C    | 5.0     | 38     | 148     | 335   | 185     | 78    | 16      | 1.0       | 5      |      | õ     |
| 21     | 1.0      | 5.0     | 37     | 687     | 250   | 167     | 74    | 10      | 1.3       | .6     | 1.1  | 0     |
| 22     | 1.3      | 5.0     | 35     | 425     | 212   | 158     | 7 ?   | 33      | .8        | .5     | .7   | 0     |
| 23     | 1.5      | 5.3     | 46     | 270     | 185   | 161     | 66    | 32      | .7        | .5     | .6   | 0.3   |
| 24     | 1.5      | 5.6     | 50     | 179     | 155   | 142     | 6 ?   | * 25    | .8        | .5     | * 5  | .5    |
| 25     | 1.5      | 6.3     | 50     | 142     | 1 3 5 | 128     | 59    | 23      | .8        | .5     | .1   | .6    |
| 26     | 1.3      | 7.9     | 50     | 96      | 126   | 116     | 55    | 19      | .6        | .4     | 0    | *.6   |
| 27     | 1.3      | 20      | 38     | 43      | 128   | 108     | 51    | 16      | .6        | .4     | 0    | .6    |
| 28     | 1.5      | 28      | 27     | 6 4 2   | 350   | 105     | 47    | 13      | .6        | .4     | 0    | .6    |
| 29     | 1.3      | 24      | b 2 3  | D 41    | 4 2 5 | * 94    | 45    | 11      | .5        |        | 0    | .6    |
| 30     | 1.5      | 43      | 621    | 0 4 1   |       | 8 8     | 44    | 9.5     | a .5      | .1     | 0    | .6    |
| 31     | 2.0      |         | 620    | 044     |       | 84      |       | 1.1     |           | 0      | 0    |       |
| Total  | 30.5     | 219.1   | 1.379  | 2.6 6 2 | 4.290 | 7.3 4 8 | 2.099 | 7 5 8.2 | 5.001.1   | 1 5.5  | 43   | 4.4   |
| Mean   | 0.98     | 7.30    | 44.5   | 85.9    | 148   | 237     | 70.0  | 24.5    | 167       | 0.50   | 0.14 | 0.15  |
| Max    | 2.0      | 43      | 147    | 687     | 425   | 550     | 98    | 45      | 3,640     | 1.0    | 1 1  | 0.15  |
| Min    | 0.6      | 2.0     | 20     | 15      | 44    | 84      | 44    | 7.7     | .5        | 0      |      | .0    |
| Ac-ft  | 60       | 435     | 2,740  | 5,280   | 8,510 | 14,570  | 4,160 | 1,500   | 9,920     | 31     | 8.5  | 8.7   |
|        |          |         |        |         |       |         |       |         |           |        |      |       |
| Cal yr | 1971 : 1 | Mean 38 | .1 Max | 6       | 10 MI | n 0     | Ac-f  | 27,     | 590       |        |      |       |
| Wtr yr | 1972 : 1 | Mean 65 | .1 Max | 3,64    | 40 MI | n 0     | Ac-f  | 47,     | 230       |        |      |       |

Discharge, in cubic feet per second for the year ending September 30, 1972

\* Discharge measurement made on this day. a No gage height record. b Stage-discharge relation affected by ice.

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#### STATE OF OREGON

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

JOHN DAY RIVER BASIN

#### 14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION.--Lat 45°20'15", long 120°03'40", in NWESWE sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

(60 m) downstream from county bridge, and 15 mi (24 km) northeast of Condon. DRAINAGE AREA.--350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD. -- April 12, 1965 to current year.

GAGE.--Water-stage recorder.

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AVERAGE DISCHARGE.--8 years (1965-73), 37.2 ft<sup>3</sup>/s (1.05 m<sup>3</sup>/s), 26,950 acre-ft/yr (33.2 hm<sup>3</sup>/yr).

EXTREMES.--Current year: Maximum discharge undetermined; no flow June 30 to Sept. 23.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft

(2.704 m); no flow at times.

REMARKS. -- Records good.

REVISIONS (WATER YEARS).--1972. Revised figures of discharge, in cubic feet per second, for the water year 1972, superceding those published in 1972, are given herewith:

| Date         | Discharge  | Month                   | ft <sup>3</sup> /s-days | Maximum | Mean    | Acre-ft |
|--------------|------------|-------------------------|-------------------------|---------|---------|---------|
| June 9, 1972 | 300 ·      | June 1972               | 1,661.1                 | 1,200   | 55.4    | 3,290   |
|              | Water year | ft <sup>3</sup> /s-days | Maximum                 | Mean    | Acre-ft |         |
|              | 1972       | 20,471.1                | 1,200                   | 55.9    | 40,600  |         |

Discharge, in cubic feet per second for the year ending September 30, 1973

| and an other states of the |                  | 11011             | Dec.               | Jan.      | Feb.             | Mar.       | April  | May     | June         | July  | Aug.      | Sept. |
|----------------------------|------------------|-------------------|--------------------|-----------|------------------|------------|--------|---------|--------------|---|-----------|-------|
| 1                          | 16               | 1.1               | 5.1                | 21        | 1.6              | 124        | 4.4    | 9,0     | 1.2          |   |           |       |
| 2                          | .6               | 1.2               | 5.1                | 17        | 17               | 120        | 42     | 9,9     | 1.2          |   |           |       |
| 3                          | .6               | 16                | 5.0                | 15        | 17               | 121        | 35     | 7.9     | 1.2          |   |           | 0     |
| 4                          | .6               | 2.4               | 4.5                | 1 1       | 16               | 87         | 33     | P.4     | 1.1          |   |           | i     |
| 5                          | .6               | 2.6               | 4.0                | 1?        | 1 =              | 74         | 35     | 07      | 1.0          |   |           | 2     |
| 6                          | .6               | 2.6               | 3.0                | 11.       | 2.0              | 6 8        | 37     | P.A     | 1.2          | 1000  |           |       |
| 7                          | .6               | 3.0               | 2.0                | 10        | 17               | 64         | 34     | 7.3     | 1.0          | 1. 1. 1. 1.   |           | 3     |
| 8                          | .6               | 3.0               | 5.8                | 1)        | 15               | 57         | 31     | 6.7     | 1.0          |   |           |       |
| 9                          | .6               | 3.2               | 2.P                | 1 )       | 10               | 57         | 30     | -       | .9           |   |           | O     |
| 10                         | .7               | 3.2               | 2.8                | 13        | 1 8              | 61         | 50     | 5.9     | .8           | 1   |           | 2     |
| 11                         | 1.0              | 3.4               | ?.E                | 20        | 1 .              | 76         | 50     |         | .8           |   |           | 3     |
| 12                         | 1.0              | 3.4               | 3.5                | 35        | 1 0              | 53         | 5 0    | 4.1     | 1.2          |   |           | )     |
| 13                         | 1.5              | 3.4               | 2.8                | 66        | 1 4              | 54         | 31     | 4.1     |              |   |           |       |
| 14                         | 1.2              | 3.4               | 2.0                | 113       | 1                | 40         | 32     | 25      | -1           |   |           | C     |
| 15                         | 1.0              | 3.0               | 1.8                |           | 2.0              | 4.6        | 24     | 2.2     | .0           | Report of the second |           | 1     |
| 16                         |                  | 4.1               | 1.2                | 2.12      | 24               | 4 3        | 24     | 21      | 0.           |   |           |       |
| 17                         |                  | 4.1               | 26                 | 132       | 25               | 47         | 26     | 2.0     |              |   |           |       |
| 18                         | .7               | 4.1               | 24                 | 82        | 25               | 4 1        | 20     | 1.8     | .0           |   |           |       |
| 19                         |                  | 4.1               | 24                 | 55        | 251              | 4 1        | 20     | 1.6     | .0           |   |           |       |
| 20                         | <br>G            | 4.1               | 12                 | 4 0       | 24               | 41         | 20     | 1.4     | .5           |   |           |       |
|                            | .8               | 3.5               | 84                 | 35        | 21               | 42         | 25     | 1.2     | .5           |   | 1000      |       |
|                            | .8               | 3.8               | 7 2                | 30        | 24               | 40         | 23     | 12      | .5           |   |           |       |
| 24                         | c                | 3.P               | 74                 | 34        | 24               | 37         | 21     | 1.7     | .4           |   |           | 1     |
| 25                         | 0                | 3.F               | 64                 | 32        | 2 11             | 42         | 1.9    | 2.0     | .7           |   | 1         | 1     |
| 26                         | .9               | 3.8               | 47                 | 14        | 40               | 4 2        | 14     | 2.0     | .5           |   |           | .1    |
| 27                         | 1.0              | 4.3               | 4 ?                | 16        | 57               | 4 0        | 12     | 1.8     | .4           |   |           | .1    |
| 28                         | 1.1              | 5.1               | 40                 | 22        | 64               | 35         | 11     | 1.8     | .2           |   | 10-0-10 3 | .1    |
| 2.9                        | 1.1              | 5.1               | 32                 | 26        |                  | 34         | 10     | 1.7     | .1           |   |           | .1    |
| 30                         | 1.1              | 5.1               | 2 R                | 26        |                  | 34         | 0.6    | 1.3     | 0.0          |   | 1.1       | .1    |
| 31                         | 1.1              |                   | 25                 | 21        |                  | 40         |        | 1.2     |              |   |           |       |
|                            | 240              | 1040              | 6 8 2 0            | 1 4 3 3 1 | 676              | 1 7 7 0    | 0.18.6 | 1244    | 215          |   |           |       |
| Total                      | 2 6.5            | 1044              | 0.030              | 1.4 3 3   | 010              | 1.774      | 9.75.6 | 1 2 4.4 | 21.5         |   |           | 1.7   |
| Mean                       | 0.87             | 3.47              | 21.9               | 45.3      | 24.1             | 57.4       | 26.9   | 4.01    | 0.72         | 2   |           | 0.02  |
| Max                        | 1.5              | 5.1               | 84                 | 200       | 64               | 129        | 44     | 9.2     | 1.2          | ;   |           | 0.1   |
| Min                        | 0.6              | 1.1               | 2.8                | 10        | 15               | 34         | 9.6    | 1.2     | 0            |   |           | 0     |
| Ac-ft                      | 53               | 206               | 1,350              | 2,780     | 1,340            | 3,530      | 1,600  | 247     | 43           | 4   |           | 1.4   |
| Cal yr<br>Wir yr           | 1972 :<br>1973 : | Mean 5:<br>Mean 1 | 3.7 Max<br>5.4 Max | 1,.       | 200 Mi<br>200 Mi | n 0<br>n 0 | Ac-f   | 38      | 980<br>1,150 |   |           |       |

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# STATE OF OREGON

#### OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

JOHN DAY RIVER BASIN

#### 14-0474. ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION .-- 45°20'15", long 120°03'40", in NWtSWt sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

(60 m), downstream from county bridge, and 15 mi (24 km) northeast of Condon.

DRAINAGE AREA.--350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD .-- April 12, 1965 to current year.

GAGE.--Water-stage recorder.

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AVERAGE DISCHARGE.--9 years (1965-74), 45.7 ft<sup>3</sup>/s (1.29 m<sup>3</sup>/s), 33,150 acre-ft/yr (40.9 hm<sup>3</sup>/yr).

EXTREMES.--Current year: Maximum discharge, 6,050 ft<sup>3</sup>/s (171 m<sup>3</sup>/s), Jan. 18, gage height, 6.87 ft (2.094 m); no flow Oct. 9.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s), June 8, 1972, gage height, 8.87 ft

(2.704 m); no flow at times.

REMARKS .-- Records good.

REVISIONS (WATER YEARS) .-- 1972. See 1973 publication.

| -      | -                                       | -         | -      |        |        |        |         |        | and the second se |       |      |       |
|--------|---|-----------|--------|--------|--------|--------|---------|--------|---|-------|------|-------|
| Day    | Oct.                                    | · Nov.    | Dec.   | Jan.   | Feb.   | Mar.   | April   | May    | June  | July  | Aug. | Sept. |
| 1      | 0.1                                     | 0.9       | 854    | 75     | 145    | 108    | 365     | 116    | 12  | 0.7   | 0.4  | 0.1   |
| 2      | .1                                      | .9        | 380    | 70     | 118    | 112    | 3 3 2 2 | 110    | 11  | .7    | .4   | .1    |
| 3      | .1                                      | .8        | 179    | 7 0    | 104    | 92     | 246     | 96     | 10  | .7    | .4   | .1    |
| 4      | .1                                      | .9        | 113    | 7 0    | 102    | 94     | 222     | 86     | 11  | .7    | .3   | .1    |
| 5      | .1                                      | 1.1       | 76     | 70     | 98     | 90     | 229     | 78     | 11  | .7    | .3   | .1    |
| G      | .1                                      | 1.2       | 49     | 70     | 80     | 102    | 254     | 70     | 14  | .8    | .3   | .1    |
| 7      | .1                                      | 1.7       | 626    | 70     | 96     | 56     | 218     | 62     | 13  | .'    |      | .1    |
| 8      | .1                                      | 2.6       | 250    | 70     | 98     | 70     | 191     | 59     | 0,9   | 0.    |      | -1    |
| 9      | 0                                       | 1 1 4 0   | 170    | 70     | 94     | 70     | 170     | 50     | 77  | .9    | 2    | .1    |
| 10     |   | 155       | 149    | 70     | 75     | 70     | 161     | 4 8    | 71  | .0    |      | 2     |
| 11     |   | 312       | 1 32   | 70     | 8.8    | 92     | 152     | 41     | 64  | 1.1   | 2    | 2     |
| 1.     |   | 208       | 108    | 80     | 82     | 102    | 135     | 3.8    | 59  | 1.3   | 2    | 2     |
| 14     |   | 118       | 90     | 200    | 82     | 120    | 130     | 37     | 5.9   | 1.2   | 2    | 2     |
| 15     | .1                                      | 96        | 88     | 1.000  | 90     | 120    | 126     | 38     | 4.8   | 1.2   | .2   | 2     |
| 16     | .1                                      | 155       | 143    | 2120   | 161    | 286    | 124     | 36     | 4.6   | • 1.1 | .2   | 2     |
| 17     | .1                                      | 155       | 266    | 2.050  | 182    | 430    | 116     | 36     | 4.1   | 1.2   | .2   | 2     |
| 18     | .1                                      | 113       | 330    | 2.620  | 152    | 345    | 114     | 37     | 3.8   | 1.4   | .2   | 2     |
| 19     | .1                                      | 86        | 197    | 2.590  | 222    | 286    | 118     | 37     | 3.6   | 1.4   | .2   | 2     |
| 20     | .1                                      | 78        | 155    | 806    | 194    | 212    | 106     | 37     | . 3.4   | 1.3   | .2   | 2     |
| 21     | .2                                      | 68        | 936    | 442    | 167    | 191    | 96      | 34     | 3.2   | 1.2   | 2    | .2    |
| 22     | .2                                      | 63        | 562    | 322    | 135    | 191    | 90      | 30     | 3.0   | 1.1   | -1   | 2     |
| 23     | -2                                      | 57        | 342    | 254    | 124    | 182    | 122     | 27     | 2.8   | .9    | -1   | 2     |
| 24     | -2                                      | 24        | 224    | 220    | 120    | 170    | 204     | 26     | 2.6   | .8    | .1   | 2     |
| 25     | .2                                      | 25        | 101    | 209    | 114    | 1/3    | 230     | 24     | 2.4   | .7    |      | .2    |
| 26     | 2                                       | 4 9       | BA     | 101    | 100    | 20.9   | 176     | 22     | 1.8   | .6    |      | 2     |
| 27     | 2                                       | 70        | 124    | 1 2 0  | 100    | 274    | 176     | 21     | 1.2   | .6    |      | 2     |
| 28     | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 400       | 121    | 128    | 2.0    | 246    | 148     | 16     | 1.1   | .0    |      | 2     |
| 25     |   | 782       | 96     | 118    |        | 518    | 124     | 15     |   |       |      | 4 2   |
| 30     | .5                                      | 102       | 82     | 118    |        | 460    |         | 13     | .7  |       | .i-  |       |
|        | .0                                      |           |        |        |        |        |         |        |   |       |      |       |
| Total  | 4.7                                     | 3.322.1   | 7.671  | 14.581 | 3.34 A | 5.774  | 5.289   | 1.402  | 1787  | 27.4  | 6.3  | 5.1   |
| Mean   | 0.15                                    | 111       | 247    | 470    | 120    | 186    | 176     | 45.2   | 5.96  | 0.88  | 0.20 | 0.17  |
| Max    | 0.6                                     | 782       | 854    | 2,620  | 222    | 538    | 365     | 116    | 14  | 1.4   | 0.4  | 0.2   |
| Min    | 0                                       | 0.8       | 82     | 70     | 82     | 70     | 90      | 13     | 0.9   | 0.4   | 0.1  | 0.1   |
| Ac-ft  | 9.3                                     | 6,590     | 15,220 | 28,920 | 6,640  | 11,450 | 10,490  | 2,780  | 354   | 54    | 12   | 10    |
| Cal yr | 1973 :                                  | Mean 43.3 | Max    | 200    | MI     | n 0    | Ac-f    | 31,350 | -   |       |      |       |
| Wtr Jr | 1974 :                                  | Mean 114  | Max    | 2,620  | MI     | n 0    | Ac-f    | 82,530 | -   |       |      |       |

Discharge, in cubic feet per second for the year ending September 30, 1974

#### STATE OF OREGON

#### WATER RESOURCES DEPARTMENT

### JOHN DAY RIVER BASIN

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION.--Lat 45°20'15", long 120°03'40", in NWsSWs sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft (60 m) downstream from county bridge, and 15 mi (24 km) northeast of Condon.

DRAINAGE AREA.--350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD .-- April 1965 to current year.

GAGE.--Water-stage recorder.

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AVERAGE DISCHARGE.--10 years (1965-75), 45.8 ft<sup>3</sup>/s (1.30 m<sup>3</sup>/s), 33,180 acre-ft/yr (40.9 hm<sup>3</sup>/yr).

EXTREMES.--Current year: Maximum discharge, 496 ft<sup>3</sup>/s (14.0 m<sup>3</sup>/s) Mar. 2, gage height, 3.20 ft (0.975 m); no flow at times.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft (2.704 m); no flow at times.

REMARKS. -- Records good.

REVISIONS (WATER YEARS).--1972. See 1973 publication.

| Day    | Oct.     | Nov.      | Dec.        | Jan.  | Feb.    | Mar.    | April  | May    | June  | July  | Aug. | Sept. |
|--------|----------|-----------|-------------|-------|---------|---------|--------|--------|-------|-------|------|-------|
| 1      | 2        | 1.4       | 3.8         | 59    | 4.0     | 175     | 254    | 164    | 21    | 2.4   | 0.1  | 0.2   |
| 2      | 2        | 1.4       | 3.8         | 5.4   | 38      | 395     | 218    | 152    | 22    | 2.2   | .1   | 2     |
| 3      | .3       | 1.4       | 4.1         | 5.6   | 20      | 278     | 236    | 152    | 22    | 1.8   |      | .2    |
| 4      | .3       | 1.4       | 4.1         | 6.1   | 2 5     | 206     | 218    | 148    | 21    | 1.6   | .11  | 2     |
| 5      | .3       | 1.4       | 4.1         | 6.1   | 23      | 167     | 179    | 130    | 15    | 1.5   | .1   | .2    |
| 6      | .3       | 1.5       | 4.1         | 6.1   | 21      | 132     | 176    | 114    | 13    | 1.2   | .1   | .1    |
| 7      | .4       | 1.8       | 4.1         | 6.4   | 21      | 114     | 176    | 108    | 10    | 1.2   | .1   | .1    |
| 8      | .4       | 2.0       | 4.3         | 7.3   | 2.2     | 104     | 173    | 104    | 8.0   | 1.3   | .1   | .1    |
| 9      | .4       | 1.8       | 4.3         | 6.4   | 18      | 132     | 164    | 98     | 7.0   | 4.9   | .1   | .1    |
| 10     | .4       | 1.8       | 4.3         | 6.4   | 26      | 124     | 173    | 100    | 6.0   | 15    | .1   | .1    |
| 11     | .5       | 2.0       | 4.6         | 6.1   | 2.8     | 104     | 179    | 100    | 5.0   | 40    | .1   | .1    |
| 12     | .5       | 2.0       | 4.6         | 5.9   | 4 3     | 86      | 250    | 92     | 4.0   | . 2.4 | .1   | .1    |
| 13     | .5       | 1.8       | 4.6         | 7.7   | 212     | 78      | 365    | 8 2    | 3.4   | 1.3   | .1   | .1    |
| 14     | .5       | 1.8       | 4.6         | 8.6   | 179     | 66      | 350    | 72     | 3.0   | .7    | 0    | .1    |
| 15     | .6       | 1.8       | 4.8         | 9.9   | 110     | 64      | 274    | 62     | 2.5   | .6    | .)   | .1    |
| 16     | .6       | 1.8       | 4.8         | 15    | 102     | 64      | 246    | 51     | 2.1   | .5    | 0    | .1    |
| 17     | .6       | 2.0       | 4.8         | 18    | 72      | 65      | 212    | 4 5    | 2.0   | .5    | 2    | .1    |
| 18     | .7       | 2.6       | 4.8         | 43    | 6 2     | 62      | 197    | 41     | 2.0   | .5    | 0    | .1    |
| 19     | .7       | 2.6       | 4.8         | 50    | 53      | 130     | 212    | 37     | 2.4   | .4    | .1   | .1    |
| 20     | .7       | 2.6       | 4.8         | 41    | 92      | 126     | 218    | 37     | 2.8   | .4    | .2   | .1    |
| 21     | ./       | 2.6       | 5.6         | 34    | 591     | 108     | 215    | 36     | 3.4   | .4    | .2   | -1    |
| 22     | .8       | 2.8       | 6.1         | 25    | 64      | 88      | 222    | 32     | 3.6   |       | .2   | -1    |
| 23     | 0.       | 3.0       | 2.9         | 23    | 60      | 90      | 218    | 28     | 3.2   |       | -2   | -1    |
| 24     | .0       | 3.4       | 2.0         | 23    | 23      | 94      | 226    | 26     | 2.8   | 4     | .2   | -1    |
| 25     | 0.       | 3.4       | 3.9         | 108   | - 22    | 1 2 8   | 393    | 2.4    | 2.6   | -4    | .2   |       |
| 26     | 1.0      | 3.4       | 0.1         | 213   | 5 7     | 148     | 200    | 22     | 2.6   | 2     | 2    | -1    |
| 27     | 1.2      | 3.4       | 0.1         | 100   | 1 2 4   | 1 2 6   | 240    | 21     | 2.4   | 47    | 4    |       |
| 28     | 1 4      | 3.4       | 5.4         | 04    | 134     | 1 2 0   | 200    | 19     | 2.4   |       | 4    |       |
| 20 1   | 1 4      | 3.41      |             |       |         | 266     | 170    | 20     | 2.2   |       | 2    |       |
| 30     | 1 31     | 101       | 5.4         | 261   |         | 200     | 112    | 20     | 2.4   |       |      | ·     |
| - 11   | 1.2      |           | 7.4         | 20    |         | 340     |        | 20     |       |       |      |       |
| Tatal  | 232      | 603       | 1528        | 9750  | 1.1.6.1 | 4577    | 6801   | 2156   | 2018  | 827   | 2.0  | 15    |
| Mann   | 0.65     | 2 21      | 1 02        | 21 5  | 62.0    | 140     | 227    | 60 5   | 201.0 | 2 67  | 0.10 | 0.10  |
| Mean   | 0.05     | 2.31      | 4.33<br>6 A | 215   | 212     | 205     | 205    | 164    | 0.73  | 2.07  | 0.12 | 0.12  |
| Max    | 0.2      | 1.0       | 2.9         | 5 4   | 10      | 595     | 164    | 104    | 2 2   | 40    | 0.2  | 0.2   |
| Acatt  | 0.2      | 127       | 3.0         | 1 040 | 2 400   | 9 670   | 13 400 | 1 290  | 2.2   | 1.64  | 7 6  | 0.1   |
| Acon ] | 40]      | 13/ 1     | 303 ]       | 1,940 | 3,490   | 0,0/0 ] | 15,490 | 4,200  | 400   | 104   | 1.5  | 0.9   |
| Cal yr | 1974 : : | Mean 84.5 | Max         | 2,620 | Mi      | 0.1     | Ac-f   | 61,200 |       |       |      |       |
| Wir Jr | 1975 : 1 | Mean 46.0 | Max         | 395   | Mit     | • 0     | Ac-f   | 33,320 |       |       |      |       |
|        |          |           |             |       |         |         |        |        |       |       |      |       |

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#### STATE OF OREGON

#### WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION.--Lat 45°20'11", long 120°03'40", in NWsSWs Sec.3, T.3 S., R.22 E., Gilliam County, on left bank 200 ft (60 m) downstream from county bridge, and 9 mi (14 km) northeast of condon.

DRAINAGE AREA.--350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD. -- April 1965 to current year.

GAGE.--Water-stage recorder.

AVERAGE DISCHARGE.--11 years (1965-76), 44.2 ft<sup>3</sup>/s (1.252 m<sup>3</sup>/s), 32,020 acre-ft/yr (39.5 hm<sup>3</sup>/yr). EXTREMES.--Current year: Maximum discharge, 302 ft<sup>3</sup>/s (8.55 m<sup>3</sup>/s) Apr. 9, gage height, 2.83 ft (0.863 m); no flow at times.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft

(2.704 m); no flow at times. REMARKS .-- Records good.

REVISIONS (WATER YEARS) .-- 1972. See 1973 publication.

| Day    | Oct.   | Nov.                   | Dec.       | Jan.       | Feb.  | Mar.  | April          | May     | June    | July | Aug.  | Sept. |
|--------|--------|------------------------|------------|------------|-------|-------|----------------|---------|---------|------|-------|-------|
| 1      | 0.1    | 2.2                    | 5.9        | 23         | 37    | 36    | 96             | 51      | 9.5     | 0.8  | 0     | 4.1   |
| 2 !    | .1     | 2.2                    | 6.1        | - 1 8      | 35    | 37    | 90             | 47      | 9.9     | .7   | 0     | 3.5   |
| 21     | .:     | 2.4                    | 7.7        | 33         | 34    | 34    | 104            | 44      | 9.5     | .7   | .1    | 3.6   |
| 4      | .1     | 2.4                    | 9.0        | 34         | 17    | 16;   | 114            | 41      | 8.6     | .6   | .1    | 3.4   |
| 5      | 2      | 2.6                    | 9.5        | 37:        | 14    | 27    | 145            | 37      | 8.2     | .5   | .1    | 3.0   |
| 6      | 2      | 3.0                    | 9.0        | 35.        | 17    | 30;   | 209            | 32      | 7.3     | .5   | 2     | 2.8   |
| 7      | .3     | 3.4                    | 9.5        | 33         | 20    | 32    | 185            | 29      | 6.8     | .5   | 10    | 2.6   |
| 8      | .3     | 3.4                    | 9.9        | 106        | 25    | 28    | 176            | 25      | 5.9     | .4   | 14 !  | 2.6   |
| 9      | .3     | 3.4                    | 11         | 116        | 25    | 28    | 266            | 23      | 5.9     | .4   | 6.8   | 22    |
| 10     | .3     | 4.1                    | 10         | 82         | 22    | 34    | 203            | 20      | 5.9     | .4   | 5.6   | 12    |
| 11     | .4     | 4.1                    | 9.5        | 66         | 20    | 38    | 179            | 18      | 5.6     | .)   | 4.6   | .6    |
| 12     | .4     | 4.1                    | 9.0        | 57         | 21    | 34    | 173            | 18      | 5.4     | .3   | 4.1   | .4    |
| 13     | .4     | 4.1                    | 9.0        | 4 4        | 23    | 37    | 176            | 14      | 4.6     | 3    | 3.8   | 3     |
| 14     | .4     | 4.1                    | 7.7        | 4 5        | 26    | 41    | 152            | 11      | 4.3     | 2    | 4.3   | 1.0   |
| 15     | .5     | 4.1                    | 7.7        | 74         | 301   | 41    | 138            | 10      | 4.1     | 21   | 5.9   | 2.8   |
| 16     | .5     | 4.3                    | 8.6        | 167        | 29    | 47    | 130            | 9.5     | 3.8     | -2   | 7.3   | 3.6   |
| 17     | .5     | 4.3                    | 8.6        | 179        | 45!   | 94    | 116            | 9.0     | 3.4     | 2    | 12    | 3.4   |
| 18     | .5     | 4.3                    | 8.2        | 152        | 501   | 173   | 114            | 8.6     | 3.2     | 2    | 11    | 3.2   |
| 19     | .5     | 4.3                    | 8.2        | 112        | 50    | 202   | 102            | 8.6     | 3.0     | .1   | 9.5   | 3.0   |
| 20     | .5     | 4.3                    | 7.7        | 8.6        | 40    | 126   | 108            | 9.0     | 2.4     | .1   | 8.6   | 2.8   |
| 21     | .6     | 4.3                    | 7.3        | 68         | 33    | 110   | 110            | 9.5     | 2.2     | .1   | 7.7   | 2.8   |
| 22     | .7     | 4.3                    | 7.3        | 59         | 32    | 110   | 94             | 8.6     | 2.0     | .1 ( | 6.8   | 3.2   |
| 23     | .8     | 4.6                    | 7.7        | 59         | 29.   | 108   | 98             | 8.2     | 1.7     | .1   | 6.4   | 3.2   |
| 24     | .8     | 4.6                    | 9.9        | 51         | 2 5   | 114   | 70             | 7.3     | 1.7     | -1   | 8.1   | 3.4   |
| 25     | 1.0    | 4.6                    | 11         | 4 3        | 32    | 150   | 84             | 7.3     | 1.5     | 0    | 8.2   | 3.4   |
| 26     | 1.6    | 5.1                    | 13         | 37         | 41    | 114   | 76             | 6.8     | 1.5     | 0    | 7.7   | 3.2   |
| 27     | 2.4    | 6.4                    | 45         | 37         | 55    | 102   | 70             | 6.4     | 1.2     | 0    | 6.8   | 3.2   |
| 28     | 2.6    | 6.4                    | 45         | 36         | 66    | 98    | 66             | 6.4     | 1.0     | 0    | 6.1   | 3.2   |
| 29     | 2.4    | 6.1                    | 40         | 4 4        | 55    | 84    | 64             | 6.4     | .8      | 0    | 5.6   | 3.0   |
| 20     | 2.2    | 5.9                    | 59         | 45         |       | 541   | 39             | 6.8     | .9      | 0    | 5.1   | 2.8   |
| 31     | 2.0    | 1                      |            | 40         |       | 100   |                | 7.7     |         | c    | 4.6   |       |
| Total  | 2 3.7  | 123.4                  | 4 6 7.0    | 2.018      | 951   | 2329  | 3.767          | 5 4 6.1 | 1 3 1.8 | 8.0  | 181.1 | 81.8  |
| Mean   | 0.76   | 4.11                   | 15.1       | 65.1       | 32.8  | 75.1  | 126            | 17.6    | 4.39    | 0.26 | 5.84  | 2.73  |
| Max    | 2.6    | 6.4                    | 59         | 179        | 66    | 202   | 266            | 51      | 9.9     | 0.8  | 14    | 4.1   |
| Min    | 0.1    | 2.2                    | 5.9        | 18         | 14:   | 27    | 59             | 6.4     | 0.8     | 0    | 0     | 0.3   |
| Ac-ft  | 47     | 245                    | 926        | 4,000      | 1,890 | 4,620 | 7,470          | 1,080   | 261     | 16   | 359   | 162   |
| Cal yr | 1975 : | Mean 47.0<br>Mean 29.0 | Max<br>Max | 395<br>266 | Min   | 0     | Ac-ft<br>Ac-ft | 34,060  |         |      |       |       |

Discharge, in cubic feet per second for the year ending September 30, 1976

5-11

#### WATER RESOURCES DEPARTMENT

5-12

#### JOHN DAY RIVER BASIN

# 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION.--Lat 45°20'11", long 120°03'40", in NW½SW½ sec.3, T.3 S., R.22 E., Gilliam County, on left bank

200 ft (60 m) downstream from county bridge and 9 mi (14 km) northeast of Condon.

DRAINAGE AREA. -- 350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD.--April 1965 to current year.

GAGE.--Water-stage recorder.

AVERAGE DISCHARGE.--12 years (1965-77), 41.1 ft<sup>3</sup>/s (1.164 m<sup>3</sup>/s), 29,780 acre-ft/yr (36.7 hm<sup>3</sup>/yr).

EXTREMES.--Current year: Maximum discharge, 112 ft<sup>3</sup>/s (3.17 m<sup>3</sup>/s) April 6, gage height, 2.25 ft (0.686 m); no flow July 16 to Sept. 30.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft

(2.704 m); no flow at times.

REMARKS. -- Records good.

REVISIONS.-- 1972, see 1973 publication.

| Day     | Oct.     | Nov.    | Dec.       | Jan.    | Feb.  | Mar.  | April | May    | June  | July  | Aug. | Sept. |
|---------|----------|---------|------------|---------|-------|-------|-------|--------|-------|-------|------|-------|
| 1       | 2.8      | 2.0     | 3.6        | 4.6     | 5.4   | 8.2   | 1.8   | 4.6    | 6.1   | .2    |      |       |
| 2       | 2.8      | 3.0     | 4.1        | 4.5     | 5.1   | 8.6   | 20    | 4.8    | 6.1   | .2    | 1    |       |
| 3       | 2.6      | 3.0     | 4.3        | 4.8     | 5.1   | 9.5   | 20    | 5.4    | 5.6   | .2    | 1    |       |
| 4       | 2.6      | 3.0     | 4.6        | 4.3     | 5.1   | 9.9   | 37    | 5.4    | 5.6   | .2    |      |       |
| 5       | 2.6      | 3.0     | 4.6        | 3.0     | 5.0   | 9.0   | 64    | 5.6    | 5.1   | .2    |      |       |
| 6       | 2.6      | 3.0     | 4.6        | 2.8     | 4.9   | 8.6   | 88    | 5.9    | 4.6   | .2    |      |       |
| 7       | 2.6      | 3.0     | 4.6        | 2.7     | 4.8   | 9.5   | 78    | 7.3    | 3.8   | 2     |      |       |
| 8       | 2.6      | 3.2     | 4.6        | 2.6     | 4.8   | 11    | 64    | 7.7    | 3.4   | .2    |      |       |
| 3 !     | 2.6      | 3.0     | 4.6        | 2.6     | 4.8   | 16    | 44    | 7.7    | 3.0   | .2    |      |       |
| 10 1    | 2.6      | 3       | 4.6        | 2.8     | 4.9   | 18    | 35    | 9.9    | 2.8   | .2    |      |       |
| 11      | 2.6      | 3.6     | 4.8        | 3.0     | 5.1   | 17    | 28    | 35     | 2.4   | .1    |      |       |
| 12      | 2.4      | 3.6     | 4.8        | 3.3     | , 5.4 | 16    | 24    | 35     | 2.4   | .1    |      |       |
| 13      | 2.2      | 3.6     | 4.8        | 3.7     | 5.9   | 16    | 21    | 34     | 2.2   | .1    |      |       |
| 14      | 2.2      | 3.6     | 4.6        | 4.0 !   | 6.4   | 13    | 20    | 26     | 2.2   | .1    |      |       |
| 15      | 2.2      | 3.6     | 4.8        | 4.5     | 6.8   | 13    | 17    | 27.    | 1.7   | .1    |      | -     |
| 16      | 2.2      | 4.3     | 4.8        | 5.2     | 6.4   | 12    | 16    | 21     | 1.5   | 0     |      |       |
| 17      | 2.2      | 4.3     | 4.8        | 5.9     | 6.1   | 12    | 14    | 19     | 1.3   | 0     |      |       |
| 18      | 2.4      | 4.3     | 4.8        | 5.9     | 6.1   | 12    | 13    | 18     | 1.3   | )     |      |       |
| 19      | 2.6      | 4.6     | 4.8        | 5.9     | 6.1   | 12    | 12    | 16     | .8    | 0.    |      |       |
| 20      | 2.6      | 4.6     | 3.8        | 5.6     | 6.1   | 12    | 11    | 15     | .8    | 0     |      | _     |
| 21      | 2.6      | 4.8     | 4.8        | 5.4     | 6.4   | 12    | 9.9   | 13     | .8    | 0     |      |       |
| 22      | 2.4      | 4.8     | 4.6        | 5.4     | 6.4   | 11    | 9.5   | 11     | .7    | 0     |      |       |
| 23      | 2.4      | 4.8     | 5.1        | 5.4     | 6.8   | 12    | 8.2   | 10     | .6    | 0     |      |       |
| 24      | 2.4      | 4.6     | 4.6        | 5.4     | 6.4   | 14    | 6.8   | 11     | .5    | 0     |      |       |
| 25      | 2.6      | 4.7     | 5.1        | 5.4     | 6.4   | 16    | 6.1   | 11     | .4    | C     |      |       |
| 26      | 2.6      | 4.8     | 4.8        | 4.6     | 6.4   | 16    | 5.9   | 11     | .3    | 3     |      |       |
| 27      | 2.6      | 4.1     | 4.8        | 4.8     | 6.4   | 17    | 5.6   | 9.5    | .3    | 0     |      |       |
| 2.8     | 2.6      | 4.6     | 4.6        | 5.1     | 7.3   | 18    | 5.1   | 9.5    | .3    | 0     |      |       |
| 29      | 2.8      | 3.6     | 4.8        | 4.8     |       | 18    | 4.8   | 9.0    | .2    | 0     |      |       |
| 30      | 2.8      | 3.6     | 4.8        | 4.6     |       | 18    | 4.6   | 8.2    | .2    | 0     |      |       |
| 31      | 2.8      |         | 4.8        | 4.8     |       | 17    |       | 7.3    |       | 0     |      |       |
| ul      | 7 8.6    | 11 6.3  | 1 4 4.0    | 1 3 7.5 | 162.8 | 412.3 | 710.5 | 4 20.8 | 6 7.0 | 2.5   | 0    |       |
| AD      | 2.54     | 3.88    | 4.65       | 4.44    | 5.81  | 13.3  | 23.7  | 13.6   | 2.23  | 0.08  | 0    | 1     |
| x       | 28       | 4.8     | 5.1        | 5.91    | 7 3   | 18    | 88    | 35     | 61    | 0.2   | 0    |       |
| n       | 2.2      | 3.0     | 3.6        | 2.6     | 4.8   | 8.2   | 4.5   | 4.6    | 0.2   | 0.0   | 0    |       |
| -ti     | 156      | 231     | 286        | 273     | 323   | 818   | 1.410 | 835    | 133   | 5.0 1 | õ    |       |
| - malan |          | 00.0    | and a star |         |       |       | -1    |        |       |       |      |       |
| n 19    | 976 : Me | an 28.3 | Max        | 266     | Min   | 0     | Ac-ft | 20,530 |       |       |      |       |

bischarge, in cubic feet per second for the year ending September 30, 1977

5-13 LAST POGE

#### JOHN DAY RIVER BASIS

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONCON, SPES.

LOCATION.--Lat 45/20111", long 120°03'40", in NMISWE sec.3, T.3 S., R.22 E., Gilliam Iburty, on left bank

200 ft (60 - downstream from county bridge and 9 mi (14 km) nontheast of Condon.

DRAINAGE AREA. -- 350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD.--Abril 1965 to current year.

GAGE.--Water-stage recorder.

AVERAGE DISCHARGE.--13 years (1965-78), 41.2 ft<sup>3</sup>/s (1.167 m<sup>3</sup>/s), 29,850 acre-ft pr (36.3 m<sup>3</sup>/yr).

EVIREMES.--Current year: Maximum discharge,478 ft<sup>3</sup>/s (13.5 m<sup>3</sup>/s) Feb. 7, gane height, 2-18 ft (0.969 m); no flow

Oct. 1-19.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft (2.704 m); no flow at times.

REMARKS .-- Records good except for August which are fair.

REVISIONS. -- 1972, see 1973 publication.

| Day | Oct. | Nov.  | Dec.  | Jan.    | Feb.  | Mar.  | April | May   | June  | July  | Aug.  | Sep   |
|-----|------|-------|-------|---------|-------|-------|-------|-------|-------|-------|-------|-------|
| 1   | 0    | 0.3   | 28    | 8.4     | 64    | 145   | 74    | 66    | 15    | 4.3   | 0.2   | 1.    |
| 2 1 | 0    | .3    | 23    | 9.9     | 66    | 124   | 96    | 55    | 1.1   | 4.6   | 2     | 1     |
| 3   | C    | 3     | 29    | 13      | 64    | 108   | 76    | 48    |       | 7 3   | 2     | 1     |
| 4   | 0    | 3     | 28    | 1 26    | 72    | 106   | 58    | 0.0   |       | 10    | 1 .2  | 1 1   |
| 5   | C    | .4    | 23    | 82      | 80    | 104   | 64    | 44    | 1.1   | 9.9   | 2     | 1     |
| 6   | 0    |       | 19    | 90      | 135   | 112   | 62    | 40    |       | 77    | 2     | 1     |
| -   | 0    | 1 4   | 17    | 62      | 218   | 118   | 70    | 36    | 5 1   | 6.1   | 2     | 1 . 1 |
| .   | 0    | 5     | 16    | 50      | 365   | 152   | 65    | 20    | 1 0   | 8.0   | 2     | 1     |
|     | 0    |       | 10    | 114     | 240   | 200   | 57    | 27    | 4.0   | 12    | .2    | 1 1   |
|     | 0    |       | 12    | 170     | 104   | 210   | 33    | 20    | 7.5   | 15    |       | 1     |
| 10  | 0    |       | 13    | 1/0     | 194   | 240   | 40    | 27    |       | 9.5   | 1 2   | 1 1   |
|     | 0    | .0    | 13    | 142     | 150   | 203   | 40    | 21    | 4.2   | 1.3   |       | 1     |
| 12  | 0    | .0    | 15    | 135     | 118   | 185   | 31    | 25    | 4.3   | 0.4   |       | 1. 1. |
| 13  | 0    |       | 18    | 1 142   | 120   | 164   | 30    | 25    | 4.5   | 5.4   | .2    | 1 1.  |
| 14  | 0    | ./    | 130   | 188     | 106   | 142   | 35    | 24    | 5     | 4.6   | -2    | 1.    |
| 15  | 0    | .5    | 185   | 310     | 104   | 125   | 33    | 33    | 5.6   | 3.8   | .2    | 1.    |
| 16  | 0    | .8    | 118   | 335     | 84    | 116   | 35    | 40    | 5.1   | 3.6   | .2    | 1.    |
| 17  | 0    | .9    | 80    | 282     | 80    | 110   | 37    | 30    | 4.8   | 3.6   | .2    | 1 1.  |
| 18  | 0    | 1.2   | 55    | 197     | 84    | 110   | 36    | 26    | 4.3   | 3.4   | .2    | 2.    |
| 19  | 0 .  | 1.4   | 37    | 182     | 102   | 102   | 32    | 23    | 3.8   | 3.0   | .2    | 2.    |
| 20  | .1   | 1.1   | 28    | 158     | 135   | 96    | 29    | 19    | 3.2   | 2.5   | .2    | 2.    |
| 21  | .1   | 1.4   | 25    | 132     | 140   | 90    | 28    | 17    | 1.5   | 2.2   | 1.0   | 2.    |
| 22  | .1   | 1.5   | 24    | 124     | 135   | 86    | 27    | 16    | 1.0   | 1.8   | 4.0   | 2.    |
| 3 1 | .1   | 1.6   | 23    | 102     | 138   | 84    | 28    | 18    | 1.8   | 1.6   | 3.0   | 2     |
| 24  | 1    | 2.8   | 23    | 82      | 140   | 106   | 28    | 17    | 3.0   | 1.4   | 2.0   | 2     |
|     | 1    | 9.8   | 24    | 76      | 164   | 90    | 26    | 17    | 3.5   | 1 2   | 1 1 4 | 2     |
| 16  | 1    | 56    | 26    | 62      | 170   | 76    | 71    | 17    | 3.6   | 1.0   | 1.4   | 2     |
| -   | 2    | 44    | 24    | 68      | 194   | 66    | 170   | 16    | 3.0   | 1.0   | 1.0   | 2     |
| . 1 |      | 25    | 22    | 66      | 161   | 50    | 122   | 16    | 2.0   |       | -/    | 2.    |
|     |      | 20    | 22    | 64      | 101   | 53    | 94    | 15    | 1 12  |       |       | 2.    |
| .9  | . 4  | 22    | 21    | 70      |       | 50    | 76    | 13    | 13    |       |       | 2.    |
| 10  | . 4  | 32    | - 10  | 60      |       | 50    | 10    | 13    | 1.6   |       | .0    | C.    |
| 1   | .3   |       | 19    | 08      |       | 50    |       | 16    |       | .6    | 1.5   |       |
| tal | 1.8  | 225.9 | 1,140 | 3,619.3 | 3,823 | 3,677 | 1,694 | 862   | 151.3 | 135.3 | 20.4  | 52.6  |
| an  | 0.06 | 7.53  | 36.8  | 117     | 137   | 199   | 56.5  | 27.8  | 5.05  | 4.37  | 0.66  | 1.7   |
| *   | 0.3  | 56    | 185   | 335     | 365   | 298   | 170   | 66    | 1 13  | 13    | 4.0   | 2.1   |
|     | 0    | 0.3   | 13    | 8.4     | 64    | 50    | 26    | 12    | 1 1.0 | 0.2   | 0.2   | 1 1   |
|     | 3.6  | 448   | 2,260 | 7,180   | 7.580 | 7.290 | 3.360 | 1.710 | 300   | 268   | 40.5  | 104   |
| -11 | 5.0  | 110   | -1200 | 1,100   | 1,000 | 1,200 | 5,500 | 1,710 | 500   | 200   | 40.5  | 104   |



# CAMAS PRAIRIE

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1월 MILES ABOVE OLEX AXEL OLSEN PLACE 9-19-85

1호 MILES BELOW FRENCH CHARLIE

12-25-75







8-10-75



WOLF HOLLOW BRIDGE 8-10-75



LOWER ROCK CREEK 1½ MILES BELOW FRENCH CHARLIE

8-10-75



. : 3.

DEBRIS 1974

4



1/19/24





BETTENCOURT SPRING

4

8

JANUARY 13, 1979

5

OLEX JANUARY 13,1979

2 . .

MARVEL BRIDGE 3/4 MILE ABOVE FRENCH CHARLIE

JANUARY 13, 1979



MOUTH OF ROCK CREEK JANUARY 1979

# SPRING NEAR MOUTH OF ROCK CREEK

6

AUGUST 30, 1989



RECEIVED

NOV 1 6 1994



DEPARTMENT OF

OCT 4 1996

RECEIVED

NATER RESOURCES DEPT. SALEM, OREGON

WATER RESOURCES DEPT. SALEM, OREGON



FISH AND

WILDLIFE

HABITAT CONSERVATION DIVISION

November 15, 1994

Mike Mattick Water Resources Department 158 12th Street, NE Salem, OR 97310

RE: Instream Water Right 70251; supporting information

Dear Mike:

Attached is the subject material you requested. Hopefully it will serve to support our application for sufficient water to operate the fishway at Harper Dam on Rock Creek (John Day River).

Sincerely,

5 addunt.

Albert H. Mirati, Jr. Fish Passage Coordinator

Burchfield c:



EXHIBIT \_\_\_\_\_ PAGE \_\_\_\_ OF \_\_\_\_

2501 SW First Avenue PO Box 59 Portland, OR 97207 (503) 229-6967



Koor VL, pur ony

UNITED STATES DEPARTMENT OF COMMERCE National Oceanic and Atmospheric Administration RECEIVED NATIONAL MARINE FISHERIES SERVICE ENVIRONMENTAL & TECHNICAL SERVICES DIVISION 1002 NE HOLLADAY STREET - ROOM 620 PORTLAND. OREGON 97232 503/230-5400

IWR 20251

January 24, 1990

NATER RESOURCES DEPT F/NWRALEM. OREGON

NOV 1 6 1994

Sharon Conyers Oregon Department of Fish and Wildlife 506 S.W. Mill Street P.O. Box 59 Portland Or. 97207

Dear Ms. Convers,

Attached is the functional design for the Harper Dam Fishway on Rock: (Enclosed). This is the second fishway of a series of upwards of 6 that is needed to insure safe and efficient adult anadromous fish passage into the upper basin of Rock Creek in the John Day River Basin. It is our understanding that the Oregon Department of Fish and Wildlife (ODFW) plans to construct the Harper Fishway during the summer of 1990 with funds carried over from FY89.

As you recall the National Marine Fisheries Service (NMFS) volunteered to help design the first couple of fishways to expedited the project. The first fishway at Ramsey Dam was designed by NMFS last September and ODFW personnel constructed it in October.

Please have your engineering staff review the enclosed functional design for the Harper Fishway. Detailed structural design is required before construction can begin on this fishway. The NMFS is not prepared to do the structural design for the Harper Dam site so the ODFW will need to either do the structural design or contract it out to a private engineering firm. As nearly \$18,000 in engineering related funding was provided to ODFW by NMFS for this project, the design costs should be covered.

Technical comments or questions on the design should be directed to Mr. Randy Lee at 230-5411. Any other comments or questions can be directed to Mr. Mike Delarm of my staff at 230-5412. We look forward to moving ahead with this project.

Sincerely

Robert Z./Smith Director, Columbia River Fisheries Development Program

EXHIBIT / PAGE 2 OF 10



# RECEIVED

Harper Dam Fishway Rock Creek John Day River Basin NOV 1 6 1994 NATER RESOURCES DEPT. SALEM, OREGON

# Background

Rock Creek enters the John Day River at river mile 21.6. The Oregon Department of Fish and Wildlife (ODFW) personnel indicated that 75 miles of habitat would be opened by correcting passage problems on Rock Creek. According to ODFW, steelhead is the only' species of anadromous fish which utilize the Rock Creek drainage. Steelhead currently utilize the lower 25 miles of the creek:

There are six irrigation dams within a 20 mile creek reach. The dams are located at creek miles 7 (Ramsey Dam), 19.75 (#2), 23.5 (Irby Dam), 25.5 (Harper Dam), 27 (McCoin Dam), and 28 (#6). Steelhead passage is entirely blocked at the Harper damsite, but all the other dams probably delay or blocks passage during low to moderate flows (possibly during higher flows).

In October of 1989, ODFW constructed a fishway designed by the National Marine Fisheries Service (NMFS) at the Ramsey damsite. In general, the fishway consists of two pools with a vertical slot insert placed between the pools.

The following presents a functional design for providing safe and efficient passage of adult steelhead at Harper Dam.

EXHIBIT / PAGE <u>3</u> OF 10

Harper Dam Fishway Rock Creek John Day River Basin

Summary

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13+1+

- Location: Approximate creek mile 25.5 T2S, R22E, Sec. 5 Gilliam County, Oregon
- Fishway type: Vertical Slot Floor slope 1 vertical to 8 horizontal 7 vertical slots with one 15-inch entrance Pool dimensions 6 foot wide by 8 foot long Vertical slot either can be formed concrete or inserts.

Design Flows: 57 cfs maximum 47 cfs normal 34 cfs minimum

EXHIBIT / PAGE 4 OF 10

# RECEIVED

NOV 1 6 1994

NATER RESOURCES DEPT. SALEM, OREGON

# Hydraulic Design

The proposed fishway at the Harper Dam is a vertical slot type with each slot having a width of one foot. Field surveys by ODFW taken May 4, 1988 indicated a head of approximately 8 feet will need to be managed by the fishway. This results in a fishway with 7 vertical slots and one 15-inch wide entrance to satisfactorily manage the 8 foot drop. Due to cost and space limitations, the fishway proposed is to have a slope of 1 vertical to 8 horizontal and have pool dimensions of 6 foot wide by 8 foot long. This is considered to be minimum dimensions for this type of fishway. Vertical slots can be either formed concrete or fabricated metal inserts which may be constructed offsite and installed in the flume when completed.

It is expected that adult steelhead will be present during the months of February through May, therefore, the fishway is designed to accomodate passage during this period. Design flows for the fishway are as follows: 57 cubic feet per second (cfs) maximum, 47 cfs normal and 34 cfs minimum. From high water marks, there appears to be 4 feet of head over the dam crest. Using the standard weir formula, this converts to a streamflow of approximately 1259 cfs. At this streamflow the effectiveness of the fishway entrance flow to attract fish is negligible without auxiliary water, however, at this high streamflow it appears fish may choose to pass over the dam or wait and use the fishway when streamflows subside.

Stoplogs at the entrance are utilized to control the discharge from the fishway. To increase operational flexibility and ease of adjustments, a gate may be considered. Adjustments to the logs or gate will be necessary to insure a hydraulic drop of 1.25 feet across the entrance. This will result in and entrance jet velocity of approximately 9 feet per second. A short flow deflecting wall is constructed between the entrance pool and the first slot upstream from the fishway entrance. The purpose of this wall is to dissipate the energy from the oncoming jet. Additionally, for dewatering purposes, stoplog slots are located at the exit. A coarse trashrack is also located at the exit. To allow passage of fish past the trashrack, the spacing between vertical rack bars are 9 inches and the spacing between horizontal members are 2 feet. To facilitate cleaning of debris from the rack, the rack face is set at a slope or 4 vertical to 1 horizontal. To insure safety, it is recommended the fishway be covered by the use of metal walkway grating.


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|-----------|---|
|           | EXHIBIT<br>PAGE 6_0   |
| SHEET NO. | TITLE   |
| 1         | INDEX TO DRAWINGS   |
| 2         | PLAN  |
| 3         | SECTION   |
| . 4       | HYDRAULIC PROFILE   |
| 5         | DETAILS   |
|           | PRELIMINARY<br>FOR REVIEW<br>NATIONAL MARINE FISHERIES SERVICE<br>1002 NE HOLLADAY STREET - RM 520<br>PORTLAND. OREGON 97232<br>HARPER DAM FISHWAY<br>INDEX TO DRAWINGS |









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EXHIBIT \_2 PAGE \_1\_ OF \_1\_

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

14-Oh74." Rock Creek above Cayuse Canyon, near Condon, Oreg.

Location .-- Lat 45\*20'15", long 120\*03'40", in MM4SW4 sec.3, T.3 S., R.22 E., on left bank about 200 ft below

county road bridge, 15 miles northeast of Condon, Gilliam County.

Records available .- April 12, 1965, to Sept. 30, 1966.

Gage .--- Water-stage recorder.

Extremes. -- Maximum discharge, 36h cfs Mar. 1h (gage height, 2.48 ft); no flow at times.

1965, 1966: Maximum discharge, that of Mar. 14, 1966; no flow at times.

Remarks .-- Records good except for period of no gage-height record, which are poor.

CAYUSE 66 - 78



| Day          | Oct.    | Nov.          | Dec.       | Jan.    | Feb.  | Mar.    | April   | May      | June    | July   | Aug. | Sept. |
|--------------|---------|---------------|------------|---------|-------|---------|---------|----------|---------|--------|------|-------|
| 1            | 2.9     | 3.9           | 8.3        | 6.1     | 12    | 19      | 174     | 9.7      | 3.3     | 1.9    | 5.0  | 0     |
| 2            | 2.9     | 4.1           | 8.0        | 9.7     | 11    | 17      | 158     | 9.3      | 3.8     | 4.1    | :1   | 0     |
| 3            | 2.9     | 4.3           | 0.9        | 12      | 12    | 14      | 121     |          | 3.8     | 3.8    | 0    | 0     |
|              | 2.9     | 5.1           | 8.0        | 12      | 11    | 14      | 96      | 1 (8.2   | 5.2     | 2.8    | 0    | 0     |
| 5            | 3.2     | 5.1           | <u>P.0</u> | 16      | 11    | 14      | 83      |          | 3.8     | 2.1    | 0    | 0     |
| 6            | 2.8     | 5.1           | P.3        | 20      | 11    | 16      | 1 14    | 7.1      | 3.8     | 1.6    | 0    | 0     |
| 1            | 5.1     | 5.1           | 8.5        | 22      | 12    | * 16    | 60      | 67       | 4.1     | 1.9    | 0    | 0     |
| 0            | 3.1     | 5.5           | 5.1        | 30      | 11    | a 21    | 52      | 64       | 4.1     | 1.0    | 0    | 0     |
| 10           | 3.1     | * 55          | a 3.5      | 23      | 11    | #2 64   | - 51    | . 55     | 3.0     | 1.4    | 0    | 0     |
| 11           | 31      | 5.5           | 4 5.5      | 21      | 10    | 114     | 50      | 55       | 3.0     | 1.5    | 0    |       |
| 12           | * 3.2   | 5.8           | a 5.5      | 10      | 10    | 1 0 9   | * * 45  | 5.2      | 3.6     | 1.1    | ő    | 0     |
| 13           | 3.4     | 6.9           | 0 55       | 19      | 10    | 217     | - 41    | 5.0      | 36      | 1.3    | 1    | ő     |
| 14           | 3.4     | 8.6           | a 5.5      | 17      | 10    | 266     | . 28    | 5.0      | 3.3     | 11     | .1   | ő     |
| 15           | 3.5     | 8.3           | a 5.5      | 17      | 10    | # 234   | . 20    | 5.0      | 2.8     | 6.7    | .1   | .4    |
| 16           | 3.5     | 8.6           | a 5.5      | 17      | 9.7   | 165     | · 29    | 5.0      | 2.4     | a 4    | * .1 | .6    |
| 17           | 3.5     | 8.3           | a 5.5      | 15      | # 10  | 104     | . 27    | 5.0      | 1.9     | a 3    | .1   | .6    |
| 18           | 3.7     | 8.3           | a 6        | 14      | 10    | 94      | - 26    | 4.4      | 1.9     | a 2    | 0    | .6    |
| 19           | 3.9     | 7.6           | •a 6       | 14      | 10    | 89      | · 23    | * 4.1    | 1.9     | a 1    | C    | .6    |
| 20           | 3.9     | 1.2           | a 6.5      | * 13    | 11    | 81      | · # 22  | 3.8      | 1.6     | a 1    | 0    | • .6  |
| 21           | 3.9     | 7.0           | * 6.7      | 13      | 11    | 69      | . 21    | 5.6      | 1.6     | a .5   | 0    | .4    |
| 22           | 5.9     | 76            | 5.5        | 14      | 12    | 58      | - 21    | 5.5      | 1.6     | a .5   | 0    | .4    |
| 23           | 3.9     | 9.6           | 4.1        | 13      | 14    | 58      | - 20    | 2.2      | 1.6     | a .5   | 0    | 5.    |
| 24           | 3.9     | 10            | 6.6        | 13      | 10    | 59      | . 16    | 31       | 1.9     | a .4   | 0    | 2     |
| 20 .         | 3.9     | 10            | 67         | 13      | 21    | 1 1 4 4 | • 14    | 2.6      | 1.4     | a .4   | 0    | .4    |
| 27           | 3.9     | 9.6           | 7.1        | 13      | 20    | 190     | - 13    | 2.6      | # 14    | a 2    | 1    | 2     |
| 28           | 3.9     | 8.6           | 7.4        | 13      | 20    | 230     | . 12    | 2.6      | 1.3     | + .1   | .1   | 2     |
| 20           | 3.0     | 0.9           | 7.4        | 13      |       | 2 34    | . 11    | 2.6      | 1.1     | .2     | .1   | .2    |
| 20           | 3.9     | 0.3           | 1.4        | 13      |       | 230     | - 10    | 2.8      | 1.1     | .6     | * 3  | = 2   |
| 31           | 3.0     | Martin Contra | 7.8        | 13      |       | 195     |         | * 3.3    |         | .5     | .1   |       |
|              | 1 CP.0  | Second Second | 2 C 4.9    |         | 346.7 |         | 1.4 C 1 | a second | 80.5    |        | 1.3  |       |
|              |         | 5 C B 9       |            | 5 C 5.P |       | 3.4 32  |         | 1 5 7.4  |         | 59.0   |      | 5.8   |
| Mean         | 3.48    | 6.96          | 6.61       | 16.3    | 12.4  | 111     | 46.7    | 5.08     | 2.68    | 1.90   | 0.04 | 0.19  |
| Acre         | 21h     | կուն          | 406        | 1,000   | 688   | 6,810   | 2,780   | 312      | 160     | 117    | 2.6  | 12    |
| Calend.      | ar year | 1965          | Max        | -       | Min   | -       | Mean    | -        | Acre-ft | -      |      |       |
| Period Water | rat     | 1965-66       | Hax        | 266     | Min   | 0       | Noan    | 17.8     | Acre-ft | 12,910 |      |       |

Discharge in cubic feet per second for the year ending Sentember 30, 19, 66

. Discharge measurement made on this day, a No gage-height record.

Water year

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

11-Oh7h. Pock Creek above Cayuse Canyon, near Condon, Creg.

Location .-- Lat 45\*20'15", long 120\*03'40", in NW15W1 sec.3, T.3 S., R.22 E., on left bank about 200 ft downstream

from county bridge, 15 miles northeast of Condon, Gilliam County.

Records available .-- April 12, 1962, to Sept. 30, 1967.

Gage .-- Water-stage recorder.

1,3

Extremes. -- Maximum discharge during year, 832 cfs Jan. 28 (gage height, 3.27 ft); no flow at times.

1965-67: Maximum discharge, that of Jan. 28, 1967; no flow at times.

Remarks .-- Records good except for period of no gage-height record, which are poor.

| Day    | Oct.  | Nov.    | Dec.  | Jan.    | Feb.   | Mar.  | April | May    | June    | July  | Aug.  | Sept. |
|--------|-------|---------|-------|---------|--------|-------|-------|--------|---------|-------|-------|-------|
| 1      | 0.4   | 1.4     | 25    | 32      | * 2 36 | 4 8   | 83    | .5 4 C | 21      | 2.0   | 0.2   | 0     |
| 2      | .4    | 1.4     | 56    | 32      | 1 9 5  | 51    | 6.9   | 240    | 19      | 1.4   | 99 .Z | C     |
| 3      | .4    | 1.4     | 51    | * 50    | 169    | 30    | 1 6 4 | 201    | 16      | 1.0   | .4    | 0     |
| 2      | .4    | 1.0     | 50    | 35      | 156    | 30    | 111   | 1 53   | 15      | 1.2   |       | C C   |
| 6      | .4    | 24      | # 52  | 36      | 1 1 0  | 41    | 1 25  | 1 30   | 10      | # 1.0 |       | C     |
| 7      |       | 2.4     | 50    | 35      | 1 10   | 40    | 130   | 125    | RE      | 1.1   | .1    | č     |
| 8      | 4     | 2.4     | 46    | 33      | 1 00   | 39    | 121   | 114    | F.0     | 1.1   | .1    | õ     |
| 9      | 2     | 2.4     | 40    | 31      | 93     | 39    | 110   | 1 ( 4  | 7.2     | 1.1   | .1    | 0     |
| 10     | .4    | 2.6     | 41    | 30      | F 3    | 42    | 110   | 112    | 6.9     | 1.1   | .1    | C     |
| 11     | .4    | 3.3     | 62    | 31      | 76     | 42    | 1 4 0 | 112    | 45      | .º    | .1    | 0     |
| 12 .   | .4    | a 5     | 70    | 36      | ,71    | 38    | 125   | 96     | (é.1)   | P. (  | .1    | С     |
| 13     | .5    | a 7     | 2.56  | 39      | 70     | 42    | 110   | 94     | 5.1     | .5    | .1    | 0     |
| 14     | .6    | alC     | 5 5 0 | F1      | 66     | 38    | 104   | 60     | 5.7     | .5    | .1    | .1    |
| 15     | ٩,    | a15     | 142   | 142     | 59     | 34    | 100   | 70     | 5.0     | .5    | .1    | .1    |
| 10     | .9    | aze     | 100   | 1 1 1 1 | 54     | 01    | 99    | 02     | 4.7     | .4    | .1    | -1    |
| 18     | .0    | 815     | 67    | 123     | 54     | 1 00  | 51    | 54     | 9.1     | .4    | 0     | -1    |
| 19     | 1.0   | 240     | 61    | 76      | 50     | 87    | 80    | 45     | 3.1     | 4     | ŏ     |       |
| 20     | .4    | 11 50   | 57    | 89      | 46     | 80    | 78    | 40     | 25      | .4    | č     | .1    |
| 21     | 1.3   | a 70    | 57    | 1 6     | 51     | 93    | 71    | 33     | 3.4     | .4    | 0     | .1    |
| 22     | 1.6   | a 5 0   | 46    | 79      | 48     | 94    | 73    | * 30   | 6.5     | .4    | c     | .1.   |
| 23     | 1.6   | a 4 0   | 39    | 64      | * 51   | 110   | 68    | 27     | 10      | .4    | 0     | .1    |
| 24     | 1.6   | a 3C    | 31    | 65      | 51     | 1 C 4 | 75    | 25     | 7.6     | .3    | C     | .1    |
| 25     | 1.6   | a 25    | 37    | 65      | 51     | 87    | 145   | 23     | 5.7     | 3     | C     | .1    |
| 26     | * 1.6 | a 20    | 21    | 62      | 4 8    | 16    | #153  | 21     | 4.7     | 2     | C     | .1    |
| 27     | 1.4   | R 16    | 26    | 70      | 43     | 1 1   | 166   | 18     | 4.1     | 2     | 0     | .1    |
| 28     | 1.4   | a 15    | 25    | 36H     | 45     | 25    | 1 / 5 | 16     | 3.8     | 2.    | C     | .1    |
| 29     | 1.4   | * 19    | 35    | 1 21    |        | 70    | 144   | 21     | 3.1     | 2     | 0     | .1    |
| 30     | 1.4   | £."     | 32    | 3 0 5   |        | *76   | 1-5   | 21     | 2.5     | 2     |       | .6    |
| Total  | 274   |         | 2033  | 200     | 2411   | 1     | 3356  | ~ 1 ]  | 2199    |       | 20    |       |
|        |       | 6 C E.2 |       | 3.6 1 0 |        | 1.943 |       | 2.576  | E 1 2.0 | 21.6  |       | 1.8   |
| Mean   | 0.88  | 20.2    | 65.6  | 116     | 86.1   | 62.7  | 112   | 83.1   | 7.33    | 0.70  | 0.06  | 0.06  |
| Max    | 1.6   | 150     | 290   | 731     | 236    | 110   | 175   | 240    | 21      | 2.0   | 12    | 0.2   |
| Min    | 0.2   | 1.4     | 25    | 29      | 43     | 34    | 68    | 16     | 2,5     | 0.2   | 0     | 0     |
| Ac-ft  | 54    | 1,200   | 4,030 | 7,160   | 4,780  | 3,850 | 6,660 | 5,110  | 436     | 43    | 4.0   | 3.6   |
| Cal yr | 1966  | Mean    | 23.7  | Max     | 290    | Hin   | 0     | Ac-ft  | 17,170  |       |       |       |
| htr vr | 1967  | Hean    | 46.0  | Max     | 290    | Min   | 0     | Ac-ft  | 33, 340 |       |       |       |

Discharge, in cubic feet per second for the year ending September, 30, 1967 ...

Discharge measurement made on this day. \*\* Field estimated made on this day. \*



EXHIBIT \_\_\_\_\_ PAGE \_\_\_\_ OF \_\_\_\_

OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

Location .-- Lat 45°20'15", long 120°03'40", in NW45W4 sec.3, T.3 S., R.22 E., on left bank about 200 ft downstream from

county bridge, 15 miles northeast of Condon, Gilliam County.

Records available .-- April 12, 1965, to Sept. 30, 1968.

Gage .-- Water-stage recorder.

99

.

Extremes .-- Maximum discharge during year not determined; no flow at times.

1965-68: Maximum recorded discharge, 832 cfs Jan. 28, 1967; no flow at times.

Remarks .- Records good except for periods of ice effect or no gage-height record, which are poor.

Revisions .-- The maximum daily discharge for water year 1967 is corrected to 731 cfs.

| Day   | Oct.   | Nov.   | Dec.   | Jan.  | Feb.   | Mar.   | April   | May   | June  | July  | Aug.                                    | Sept.            |
|---|--|--|--|---|--|--|---|---|---|---|---|------------------|
| Day<br>1<br>2<br>3<br>4<br>5<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17 | 0ct.<br>0.2 2<br>* a 2 2<br>a 2 2 | Nov.<br>a 0.9<br>a .9<br>a .9<br>a .9<br>a .9<br>a .9<br>a .9<br>a .9<br>a .9<br>a .9<br>a .10<br>a 1.1<br>a 1.1<br>a 1.2<br>a 1.2<br>a 1.2<br>a 1.3 | Dec.<br>a 1.4<br>a 1.6<br>a 2.0<br>a 2.3<br>* 2.8<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.2<br>a 2.0<br>a 1.5<br>a 1.4<br>a 1.6<br>a 2.0<br>a 2.3<br>* 2.8<br>a 2.0<br>a 2.3<br>* 2.8<br>a 2.0<br>a 2.5<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 1.5<br>a 1.6<br>a 1.6<br>a 2.0<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 2.5<br>a 1.5<br>a 1.5<br>a 1.6<br>a 1.6<br>a 1.6<br>a 1.8<br>a 1 | Jan.<br>a 7<br>a 6<br>*b 5<br>a 4<br>*b 2.5<br>b 3.0<br>b 3.5<br>b 4.0<br>c 5<br>c 5<br>c 6<br>c 7<br>c 7<br>c 7<br>c 7<br>c 7<br>c 7<br>c 7<br>c 7 | Feb.<br>16<br>15<br>15<br>17<br>24<br>29<br>28<br>a 25<br>a 21<br>a 19<br>a 16<br>29<br>28<br>a 25<br>a 21<br>a 19<br>a 14<br>a 12<br>a 11<br>a 11<br>a 12 | Mar.<br>37<br>34<br>29<br>* 27<br>25<br>24<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21<br>21 | April<br>1 C<br>9.6<br>9.6<br>9.6<br>9.6<br>9.2<br>8.0<br>7.1<br>6.3<br>6.3<br>5.9<br>5.9<br>5.9<br>5.9 | May<br>4.2<br>3.8<br>3.4<br>3.4<br>3.4<br>3.4<br>3.4<br>3.4<br>3.4<br>3.4<br>2.4<br>2.4<br>2.4<br>2.4<br>2.4<br>2.4<br>2.4<br>2.4<br>2.4<br>2 | June<br>3.1<br>3.1<br>3.1<br>3.2<br>2.8<br>2.4<br>2.2<br>2.4<br>2.0<br>2.0<br>1.7<br>1.9<br>1.7<br>1.5<br>1.5 | July<br>* 0.6<br>a .5<br>a .4<br>a .3<br>a .2<br>a .2<br>a .2<br>a .2<br>a .1<br>a .1<br>a .1<br>a 0<br>a 0 / | Aug.                                    | Sept.            |
| 18<br>19  | a 2<br>a 2   | a 1.3<br>a 1.3   | a .9   | 22  | a 14<br>a 17   | b 13<br>b 13   | 5.6<br>5.2  | 1.9   | 1.3<br>1.3  | 00  |   |                  |
| 20<br>21<br>22<br>23<br>24<br>25<br>26<br>27<br>28<br>29<br>30<br>31                        | a .2<br>a .3<br>a .4<br>a .5<br>a .5<br>a .6<br>a .6<br>a .6<br>a .6<br>a .1.5<br>a 1.4<br>a 1.1   | a 1.3<br>a 1.3                                    | a 1.0<br>a 1.3<br>a 1.6<br>a 2.2<br>a 2.6<br>a 4.0<br>a 8.0<br>a 17<br>a 25<br>a 15<br>a 10<br>a 8.0<br>a 8.0  | 16<br>25<br>70<br>46<br>36<br>30<br>b12<br>b 8<br>b 9<br>b10<br>b12<br>b14  | a 25<br>a 120<br>a 280<br>a 90<br>a 70<br>a 55<br>a 50<br>a 45<br>a 40   | 15<br>14<br>14<br>13<br>12<br>12<br>14<br>16<br>14<br>13<br>11<br>10                                   | 5.2<br>5.6<br>5.6<br>5.9<br>5.6<br>5.6<br>5.6<br>5.6<br>5.6<br>4.8<br>4.5                               | 5.2<br>4.2<br>4.5<br>3.8<br>4.2<br>4.8<br>4.8<br>4.8<br>4.8<br>4.8<br>4.5<br>4.2<br>3.8<br>3.4  | 1.3<br>1.1<br>1.0<br>1.1<br>1.1<br>1.1<br>5.5<br>.5<br>.5<br>.6<br>.6<br>.6                                   |   |   |                  |
| Total<br>Mean<br>Max<br>Min<br>As-fi  | 1 2.2<br>0.39<br>1.5<br>0.2<br>24  | 34.8<br>1.16<br>1.3<br>0.9<br>69   | 1 2 6.0<br>4.06<br>25<br>0.8<br>250  | 4 9 1.8<br>15.9<br>70<br>2.5<br>975   | 1 1 6 2<br>10.1<br>280<br>11<br>2,300  | 568<br>18.3<br>37<br>10<br>1,130   | 2 0 5.9<br>6.86<br>10<br>4.5<br>108   | 1 0 5.6<br>3.ltl<br>5.2<br>1.9<br>209   | 4 8.6<br>1.62<br>3.1<br>0.5<br>96   | 3.0<br>0.10<br>0.6<br>0<br>6.0  | 000000000000000000000000000000000000000 | 0<br>0<br>0<br>0 |
| Wir yr  | 1968 :   | Mean 7.5   | i Max  | 280   | M  |  | Ac-   | n 5,  | 470   |   |   |                  |

EXHIBIT \_3 PAGE \_3\_OF\_13

Discharge, in cubic feet per second for the year ending September 30, 1968.

\* Discharge measurement made on this day.

a No gage-height record.

JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION.--Lat 45°20'15", long 120°03'40", in NWYSWY sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

PERIOD OF RECORD .-- April 12, 1965, to current year.

GAGE.--Water-stage recorder.

EXTREMES.--Current year: Maximum discharge, 1,010 cfs June 10 (gage height, 3.69 ft); minimum observed, 0.1 cfs Oct. 2

(gage height, 0.67 ft); and may have been no flow sometime Oct. 1.

Period of record: Maximum recorded discharge, 1,010 cfs June 10, 1969 (gage height, 3.69 ft); no flow at times. REMARKS .-- Records good except for periods of no gage height record, which are poor.

| Discharge, | in cubic | feet p | er second | for | the year | ending | September | 30, | 1969 |  |
|------------|----------|--------|-----------|-----|----------|--------|-----------|-----|------|--|
|------------|----------|--------|-----------|-----|----------|--------|-----------|-----|------|--|

| Day         Oct.         Nev.         Dec.         Jan.         Feb.         Mar.         April         May         June         July         Aug.         Sep           1         a         1.1         a         5         a         1.0         b         2.0         b         2.4         65         * 6.65         8.5         1.0         * 7.7         .4           3         a         1.3         a         1.8         b         2.0         b         2.6         653         4.15         7.5         7.4         7.4         .4           4         a         .7         2.4         b         2.7         1.3         6.6         5.4         5.9         6.8         .4           4         a         .7         2.4         b         7.0         1.3         6.5         1.4         .3         6.8         2.1         3.5         4.4         .7         .4         .3         .4         .4         .7         .4         .3         .4         .4         .7         .4         .3         .3         .3         .3         .3         .3         .3         .3         .3         .3         .3         .3         .3   |        |             |            |             |            | The second part      |                               | 1       | I selected        |         |       |                 |                      |
|--|--------|-------------|------------|-------------|------------|----------------------|-------------------------------|---------|-------------------|---------|-------|-----------------|----------------------|
| 1       a       1       a       5       a 10       b       2.0       b       2.4       6.5       *       6.6       5       10       *       7.7       .4         3       a       1.5       a 1.8       b       2.0       b       2.6       6.5       4.15       7.5       7.4       7.4       7.4       7.4         4       a       3       a       7       2.4       b       3.0       1.5       6.8       4.4       7.5       7.4       7.4       7.4       7.4         5       a       .4       a       .7       2.4       b       3.0       1.5       6.8       4.4       1.5       6.8       4.4       1.5       6.8       4.4       2.1       5.3       5.6       4.4       7.7       4.4       4.5       5.9       5.6       4.4       2.1       5.3       5.0       4.6       b       2.0       4.5       7.0       4.6       5.9       6.8       1.2       7.3       3.4       2.1       2.3       5.0       4.4       2.6       2.7       7.3       3.4       2.2       3.5       4.2       3.3       3.5       4.2       3.3       3.5  | Day    | Uct.        | Nov.       | Dec.        | Jan.       | Feb.                 | Mar.                          | April   | May               | June    | July  | Aug.            | Sept.                |
| $\begin{array}{c} \mathbf{s} & \mathbf{t} & $ | 1      | a .1        | a .5       | a 1 0       | b 2.0      | b 24                 | 65                            | * 665   | 85                | 10      | * 7.7 | .4              | .3                   |
| *  | 2      | * 2         | a .8       | a 1 3       | b 2.0      | b 24                 | 62                            | 542     | 82                | 8       | 7.7   | .4              | .3                   |
| 3       a       3       a       3       7       2       4       b       2.0       b       3.0       6       6       2       3.90       7.0       6.5       6.8       .4         4       a       .7       2       4       b       4.0       1       3.9       7       6       4       4.0       5.9       6.8       .4         7       a       .4       a       .7       2.3       b       7.0       .4       0       8       3       9.5       4       4       5.9       6.8       .4         1       a       .5       a       5.0       .4       2       71       3       8       5       4       2.0       7.1       3.85       5       4       4       2.1       5.3       .4       4       3.9       4       2.3       5.0       .4       .4       .3       .4       .3       .4       .2       .3       .3       .4       .3       .4       .2       .3       .3       .3       .4       .3       .3       .3       .3       .3       .3       .3       .3       .3       .3       .3       .3       .3   | 3      | .3          | a 1.5      | a 1 8       | b 2.0      | b 26                 | 65                            | 415     | 75                | 7.4     | 7.4   | .4.             | .3                   |
| *       •       2       4       b       3.7       2.4       b       3.7       1.       3.5       6.8       4.4       6       1       5.9       6.8       .4         7       a       .4       a       .7       2.3       b       7.0       .4       0       8.3       3.9       5       4.9       5.9       5.6       .4         1       a       .4       a       .7       2.3       b       7.0       .4       0       8.3       3.9       5       4.9       5.9       5.6       .4         a       .5       a       .5       .4       .7       1       3.0       4.1       6.5       3.7       5       3.4       4.2       7.1       3.6       4.4       2.7       4.4       .3       5       4.2       7.1       3.6       3.7       1.1       3.5       4.2       7.1       3.6       3.9       3.1       1.1       3.5       4.2       7.3       3.6       3.3       3.9       3.3       3.9       3.3       3.9       3.3       3.9       3.3       3.9       3.3       3.9       3.3       3.9       3.3       3.9       3.3       3.9   |        | a .3        | a .9       | *23         | b 2.5      | E 30                 | 62                            | 390     | 70                | 6.5     | 6.8   | .4              | .3                   |
| a       a       a       a       a       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       b       a       c       b       a       c  |        | <u>a .3</u> | a .7       | 24          | b 3.0      | 1. 35                | 68                            | 440     | 61                | 5.9     | 6.8   | .4              |                      |
| a       A       *       1.1       2.3       b       2.0       4.0       0       0.3       3.3       3.5       4.4       4.4       2.1       5.3       4.4         s       a       5.0       4.46       b       2.0       4.5       7.0       3.8 0.5       3.4       4.2       7.1       3.4       1.27       4.4       3.1         11       a       .6       a       3.5       1.4.5       6.0       1.11       7.0       3.20       3.1       a       3.5       4.2       .3         11       a       .6       a       4.5       6.2       1.30       2.8 2       7.1       2.6.8       2.0       3.9       .3 <td>6</td> <td>a .4</td> <td>a .7</td> <td>24</td> <td>b 4.0</td> <td>10</td> <td>18</td> <td>446</td> <td>24</td> <td>5.9</td> <td>6.8</td> <td>••</td> <td></td>  | 6      | a .4        | a .7       | 24          | b 4.0      | 10                   | 18                            | 446     | 24                | 5.9     | 6.8   | ••              |                      |
| a       a       b       20       45       70       350       36       42       50       44         a       a       a       42       71       b       30       44       65       375       34       127       44       34         11       a       a       a       43       b       60       111       70       320       31       a       35       42       33         12       a       10       a       45       62       130       282       71       266       28       a       20       39       3       33       44       35       442       33       34       17       3.6       33       36       42       33       34       17       3.6       33       36       42       33       34       17       16       36       22       20       80       22       20       80       22       43       34       17       16       36       22       20       80       22       43       35       41       36       33       4       12       14       130       17       22       20       20       20       20       2  |        | 8.4         | a ./       | 20          | b 90       | . 40                 | 71                            | 385     | 49                | 21      | 5.0   | .4              |                      |
| in       a  <  |        | a .4        | - 50       | 46          | b 20       | 45                   | 70                            | 350     | 30                | + 27    | 5.0   | .4              |                      |
| 11       a       b       a       5.6       0       1       1       70       520       51       a       5.5       42       33         11       a       1.0       a       4.5       6.2       1.30       2.96       2.8       a       2.0       3.9       .3         13       a       1.0       a       4.5       6.2       1.30       2.82       7.1       2.6.8       2.5       a       1.4       .3.6       .3         14       a       .9       a       4.5       4.5       1.0       7.6       1.2.8       8.0       2.2.8       2.5       a       1.4       .3.6       .3         16       a       .9       a       4.5       1.0       7.6       1.2.8       1.6.2       2.6       a       1.0       2.2       2.0       a       9.0       2.2       .3       .3         18       a       .9       a       1.0       2.6       7.1       1.0.1       2.4.2       1.55       .3       a       6.2       1.5       .3       .4         19       a       .9       a.1.0       .2.6       7.1       1.0.1       2.4.2       1.55 </td <td>10</td> <td>a .5</td> <td>a 4.5</td> <td>71</td> <td>b 30</td> <td>41</td> <td>65</td> <td>375</td> <td>34</td> <td>127</td> <td>4.4</td> <td></td> <td></td>   | 10     | a .5        | a 4.5      | 71          | b 30       | 41                   | 65                            | 375     | 34                | 127     | 4.4   |                 |                      |
| it       a 2.0       a 5.0       8 5       1 0 5       4 4 2       6 6       2 9 6       2 8       a 2 0       3.9       3.3         it       a .9       a 4.0       5 2       1 7 1       2 0 4       8 0       2 2 8       2 5       a 1 4       3.6       3         is       a .9       a 4.5       4 5       1 0 7       1 4 8       1 3 0       1 7 7       2 66       a 1 2       3.3       3         is       a .9       a 4.5       4 5       1 0 7       1 4 8       1 3 0       1 7 7       2 66       a 1 2       3.3       3         is       a .9       a .43       4 5       1 0 7       1 4 8       1 3 0       1 7 7       2 66       a 1 2       3.3       3         is       a .9       a .10       2 6       7 1       1 0 1       2 4 2       1 8 1       6 3       2 2 2       4 3.0       3         is       a .9       a .0       b 2 0       b 3 2       7 8       3 5 8       1 3 5       2 5       6 2 1.5       3 3       *         is       a .9       a .0       b 2 0       b 3 2       7 8       4 8 1       1 3 2       1 6       1 0       1 3 3  | 11     | a .8        | a 5.4      | 145         | b 60       | 111                  | 70                            | 320     | 21                | a 35    | 4.2   | .3              |                      |
| iii       a 1.0       a 4.5       6.2       1.30       2.82       7.1       2.68       2.6       a 1.7       3.6       3         iis       a .9       a 3.5       4.5       1.19       1.65       8.9       1.9       2.8       a 1.2       3.3       3         iis       a .9       a 4.5       4.5       1.07       1.48       1.00       1.72       2.6       a 1.0       2.33       3         iis       a .9       a 4.5       4.5       1.07       1.48       1.00       1.72       2.6       a 1.0       2.25       .3         iis       a .9       a 1.2       2.9       8.0       1.5       2.7       4       1.81       4.2       2.0       2.2       4.3       2.2       4.3         iii       a .9       a 1.2       2.9       8.0       1.5       2.7       4       1.81       ± 2.5       3.3       4       6.8       1.7       3.3         iii       a .9       a 1.0       2.6       7.1       1.01       2.4.2       ± 1.55       3.3       4       6.8       1.7       3.3       5         iii       a .70       b 1.5       3.6       7.6       <  | 12     | a 2.0       | a 5.0      | 85          | 105        | 442                  | 66                            | 296     | 28                | a 20    | 3.9   | .3              | .3                   |
| 14       a. 9       a. 4.0       5.2       1.7 1       2.0.4       8.0       2.2 8       a. 1.4       .3.6       .3         15       a. 9       a. 4.5       4.5       1.0.7       1.4.8       1.30       1.7.2       2.6       a. 1.4       .3.6       .3         17       a. 9       a. 4.5       4.5       1.0.7       1.4.8       1.30       1.7.2       2.6       a. 1.0       2.6       .3         18       a. 9       a. 8.0       3.4       7.6       1.2.8       4.3.6       2.2.2       2.0       a. 9.0       2.2.2       *.3         19       a. 9       a.10       .2.6       7.1       1.0.1       2.4.2       1.5.5       3.3       *.6.6       1.7       .3         11       a. 9       a. 9       a.10       .2.6       7.1       1.0.1       2.4.2       1.5.5       3.3       *.6.6       1.7       .3       .3       *.7         12       a. 8       a.7.0       b.15       3.6       7.8       3.5.8       1.3.5       2.5       6.2       1.3       .3       *.7         13       a.7       a.4.0       b.3.0       b.2.8       6.2       4.9.1       1.2  | 13     | a 1.0       | a 4.5      | 62          | 130        | 282                  | 71                            | 268     | 26                | a 17    | 3.6   | .3              | .3                   |
| is       a. g       a. 3.5       4.5       1 1 9       1 6.5       8.9       1 9 9       2.8       a. 12       3.3       .3         is       a. 9       a. 5.6       3.8       9.9       1 4.0       2.18       1 6.3       2.2       a. 9.0       * 2.5       .3         is       a. 9       a. 12       2.9       8.0       3.4       7.6       1 2.8       2.7       4.18       1.63       2.2       a. 9.0       * 2.5       .3         is       a. 9       a. 12       2.9       8.0       3.4       7.6       1.2.8       2.7       4.18       1.81       * 2.7       a.80       2.0       .3       .3         is       a. 9       a. 9.0       1.2       * 6.5       0.1       2.8.2       * 1.40       3.0       6.2       1.5       .3         it       a. 8       a.7.0       b.15       3.6       7.8       3.58       1.35       2.5       6.2       1.5       .3       .4         it       a. 8       a.7.0       b.2.0       b.2.4       6.5       5.1       3.2       6.2       1.8       1.5       9.2       9.3       3.3         it       a. 4       a   | 14     | a .9        | a 4.0      | 52          | 171        | 204                  | 80                            | 228     | 25                | a 14    | . 3.6 | .3              | 3                    |
| is       a. 9       a. 4.3       4.5       1.6       7       1.4       1.7       2.1       8       1.6       3       2.2       3.3       3.3         is       a. 9       a. 0.0       3.4       7.6       1.2.8       4.3.6       2.3.2       2.0       a. 9.0       2.2.2       +.3.3         is       a. 9       a.10       .2.6       7.1       1.0.1       2.42       1.5       3.3       * 6.8       1.7       .3         is       a. 9       a.9.0       1.2       * 6.5       9.1       2.4.2       1.5       3.3       * 6.8       1.7       .3         it       a. 8       a.7.0       1.2       * 6.5       9.1       2.8.2       * 1.40       3.0       6.2       1.5       .3         it       a. 8       a.7.0       b.2.5       b.3.0       6.0       4.8.1       1.3.5       2.5       6.2       1.5       .3       *         it       a.7       a.4.0       b.2.0       b.2.8       6.2       * 3.7.6       1.4.8       1.4.6       1.0       1.3       .3         it       a.7       a.4.0       b.2.6       5.3       0.6.0       4.9.5       1.8 <t< td=""><td>15</td><td>a .9</td><td>a 3.5</td><td>45</td><td>119</td><td>165</td><td>89</td><td>199</td><td>2.8</td><td>a 12</td><td>3.3</td><td>.3</td><td>.3</td></t<>   | 15     | a .9        | a 3.5      | 45          | 119        | 165                  | 89                            | 199     | 2.8               | a 12    | 3.3   | .3              | .3                   |
| 17       a. 9       a. 7.0       3.4       7.6       1.2.6       4.3.6       2.3.2       2.2.2       a. 9.0       * 2.2.3       .3.3         18       a. 9       a. 1.2       2.9       8.0       1.1.5       2.7.4       1.8.1       * 2.7       a. 8.0       2.0       .3.3         19       a. 9       a. 1.0       .2.6       7.1       1.0.1       2.4.2       1.5.5       3.3       * 6.8       1.7.7       .3.3         11       a. 9       a. 9.0       1.2       * 6.5       9.1       2.8.2       * 1.4.0       3.0       6.2.2       1.5       .3         12       a. 8       a. 7.0       b.1.5       3.6       7.8       3.5.8       1.3.5       2.5       6.2       1.5       .3         13       a. 7       a. 5.0       b.2.0       b.3.2       7.6       4.4.8       1.4       1.2       1.1       .3         14       a. 7       a. 3.0       b.1.5       b.2.6       6.2       * 3.7       6.3       2.2.7       1.3.3       *         15       a. 7.7       a. 3.0       b.2.4       6.2       * 3.7       6.6       1.4.8       1.4.4       1.2       1.1.3       .3  | 16     | a .9        | a 4.5      | 45          | 107        | 14 R                 | 130                           | 172     | 26                | a 10    | 2.8   | .3              | .4                   |
| 18       a9       a. 0.0       2.4       7.6       1.1.5       2.7.4       1.8.1       2.7.6       1.8.1       2.7.6       a. 8.0       2.2.0       3.3         20       a9       a. 10       2.6       7.1       1.0.1       2.4.2       1.5.5       3.3       *       6.8       1.7.7       .3         zt       a9       a. 7.0       b.1.5       3.6       7.8       3.5.8       1.3.5       2.5       6.2       1.5.5       .3       *         zt       a8       a. 5.0       b.2.0       b.3.2       7.8       4.8.1       1.3.2       1.9       7.7       1.3       .3       *         zt       a8       a. 5.0       b.2.5       b.3.0       6.0       4.9.5       1.1.8       1.5       .9.2       .9       .3       *         zt       a7       a. 4.0       b.3.0       b.2.8       6.2       * 3.7.6       1.4.8       1.4       1.2       1.1.1       .3       .3         zts       a7       a. 4.0       b.5.0       b.2.6       6.0       4.9.5       1.0.6       .9       .3         zts       a4       a. 3.0       b.7.0       b.2.4       * 6.5<   | 17     | a .9        | a 2.6      | 30          | 99         | 1 4 0                | 210                           | 2 3 2   | 22                | a 9.0   | * 2.5 | .3              | .4                   |
| iso       a. g       a. 10       2.6       7.1       1.0.7       2.4.2       1.5.7       1.3       1.3         ii       a. g       b. g       c <thc< th="">       c       <thc< th=""> <thc< th=""></thc<></thc<></thc<>  | 18     | a .9        | a 0.0      | 20          | 0          | 115                  | 274                           | 181     | \$ 27             | a 9.0   | 2.2   | * .3            | 3.0                  |
| 10       a       9       a       9       1   | 19     | 4 .9        | a10        | 26          | 71         | 101                  | 242                           | 155     | 33                | * 68    | 1.7   |                 | 2.0                  |
| 11       a       .8       a       7.0       b       1.5       3.6       7.8       3.5.8       1.3.5       2.5       6.2       1.5       .3.       *         12       a       .8       a       5.0       b       2.0       b       3.2       7.8       4.81       1.3.5       2.5       6.2       1.5       .3.       *         13       a       .7       a       4.0       b       3.0       b       2.8       6.2       *       1.6       7.7       1.3.       .3.       .3       *         14       a       .7       a       4.0       b       3.0       b       2.8       6.2       *       3.7.6       1.4.8       1.4       1.2       1.1       .3       .3       *         15       a       .4       a       3.0       b       8.0       b       2.5       5.3       6.3.2       1.00       1.8       1.5       .9       .3   | - 21   | a .7        | a 9.0      | 12          | * 65       | 91                   | 282                           | * 1 4 0 | 30                | 6.2     | 1.5   |                 | 1./                  |
| 13       a       .6       a       5.0       b       20       b       3.2       7.8       4.81       1.92       1.0       7.7       1.3       .3         14       a       .7       a       4.0       b       30       b       2.8       6.2       * 3.7       6       1.48       1.6       1.0       1.3       .3         15       a       .7       a       4.0       b       2.0       1.48       1.6       1.0       1.3       .3         15       a       .7       a       4.0       b       2.0       1.48       1.6       1.0       1.3       .3         17       a       .4       a       3.0       b       8.0       b       2.5       5.3       6.32       10.0       1.8       6.6       .9       .3         18       a       .4       a       3.0       b       7.0       b       2.4       6.5       5.5       1.92       1.9       8.0       .8       .3         19       a       .4       a       7.0       b       2.4       7.3       6       10.0       1.4       8.6       6.6       .3       .3   | 22     | a .8        | a 7.0      | b15         | 3.6        | 78                   | 358                           | 135     | 25                | 6.2     | 1.5   | 3               | * 1 1                |
| 11       a       .7       a       5.0       b       30       60       406       148       16       10       1.3       .3         15       a       .7       a       4.0       b       30       b       28       62       *376       148       14       12       1.1       .3       .3         16       a       .5       a       3.0       b       15       b       26       600       495       118       15       92       .9       .3         17       a       .4       a       3.0       b       7.0       b       24       * 65       551       92       19       8.0       .8       .3         18       a       .4       a       4.0       b       5.0       b       24       * 65       551       92       19       8.0       .8       .3         19       a       .4       a       7.0       b       24       794       12       .4       .3       .3         19.9       12       8.9       9       8.4.9       1.4.3       7.5       2.7.3       1       8.1 72       7.9 55       1.0 5 7       4.4 5.9  | 23     | · a .8      | a 5.0      | 620         | b 32       | 78                   | 481                           | 1 3 2   | 19                | 7.7     | 1.3   |                 | 1.1                  |
| 15       a       .7       a       4.0       b 30       b       28       6 2       * 37 6       1 4 8       1 4       1 2       1.1       .3         16       a       .5       a       3.0       b 15       b       26       60       495       1 1 8       15       92       .9       .3         17       a       .4       a       3.0       b       8.0       b       25       53       63 2       100       18       15       92       .9       .3         18       a       .4       a       3.0       b       8.0       b       25       53       63 2       100       18       16       6.6       .9       .3         29       a       .4       a       4.0       b       2.4       # 65       55 1       92       19       6.0       .8       .3         30       a       .4       a       1.9       b       2.4       7.94       100       14       8.6       6       .3         31       a       .4       a       a       1.7       2.731       8.172       7.855       1.057       4.45.9       10.4.4       10.2<   | 24     | a .7        | a 5.0      | b25         | b 30       | 60                   | 406                           | 148     | 16                | 10      | 1.3   | .3              | 9                    |
| 16       a       .5       a       3.0       b       1.5       b       2.6       6.0       4.9.5       1.1.8       1.5       9.2       .9       .3         17       a       .4       a       3.0       b       8.0       b       2.5       5.5       1.1.8       1.5       9.2       .9       .3         18       a       .4       a       3.0       b       7.0       b       2.4       #       6.5       5.5.1       9.2       1.9       8.0       .8       .3         19       a       .4       a       0.0       b       2.4       #       6.5       6.5       1.25       1.6       8.0       .8       .3         30       a       .4       a       7.0       b       2.4       7.3.6       1.00       1.4       8.6       .6       .3         31       a       .4       0.0       b       2.4       7.3.6       1.00       1.4       8.6       .6       1.3         32       a       .4       a       7.5       2.7.3.1       8.1.7.2       7.8.5.5       1.0.5.7.7       4.4.5.9       1.0.4.4       10.2       2       2 <t< td=""><td>25</td><td>a .7</td><td>a 4.0</td><td>b 3 O</td><td>b 28</td><td>6 ?</td><td>* 376</td><td>148</td><td>14</td><td>12</td><td>1.1</td><td>.3</td><td>.9</td></t<>  | 25     | a .7        | a 4.0      | b 3 O       | b 28       | 6 ?                  | * 376                         | 148     | 14                | 12      | 1.1   | .3              | .9                   |
| 17       a       .4       a       3.0       b       8.0       b       2.5       5.3       6.3.2       10.0       1.8       6.6       .9       .3         18       a       .4       a       3.0       b       7.0       b       2.4       #       6.5       5.51       9.2       1.9       1.9       8.0       .8       .3         29       a       .4       a       4.0       b       5.0       b       2.4       #       6.5       6.6       1.2       1.6       8.0       .8       .3         30       a       .4       a       7.0       b       2.4       7.9.4       1.2       1.6       8.0       .6       .3         31       a       .4       1.9       b       2.4       7.9.4       1.2       .4       .3         Total       1.9.9       1.2 8.9       9.8.4.9       1.4.3       7.5       2.7.3 1       8.1 7.2       7.8.5 5       1.0 5.7       4.4 5.9       1.0 4.4       10.2       2         Mean       0.64       4.30       31.8       46.4       97.5       264       262       34.1       14.9       3.37       0.33       0.3<  | 26     | a .5        | a 3.0      | b15         | b 26       | 60                   | 495                           | 118     | 15                | 92      | .9    | .3              | .9                   |
| 13       a       .4       a       3.0       b       7.0       b       2.4       #       6.5       5.5 1       9.2       1.9       8.0       .8       .3         13       a       .4       a       4.0       b       5.0       b       2.4       7.3       6.96       1.2.5       1.6       8.0       .8       .3         30       a       .4       a       7.0       b       2.4       7.3       6.96       1.2.5       1.6       8.0       .8       .3         30       a       .4       a       7.0       b       2.4       7.3       6.10.0       1.4       8.6       .4       .3         31       a       .4       a       7.5       2.7       3.1       8.1 7.2       7.8 5.5       1.0.5 7       4.4 5.9       1.0.4.4       1.0.2       2         Mean       0.64       4.30       31.8       46.4       97.5       2.64       262       34.1       1.4.9       3.37       0.33       0.3         Mean       0.1       0.5       1.9       2.0       2.4       62       92       12       5.9       0.4       0.3       0.3       0.3   | 27     | a .4        | a 3.0      | b 8.0       | b 25       | 5)                   | 632                           | 100     | 18                | (8.6)   | .9    | .3              | .9                   |
| 13       a       .4       a       4.0       b       2.4       0       9       6       1       2.5       1       6       8.0       .8       .3         30       a       .4       a       7.0       b       4.0       b       2.4       7       7       6       1       0.0       1.4       8.6       .6       .3       .3         31       a       .4       1.9       b       2.4       7       7.9.4       1       2       .4       .3         Total       1.9.9       1.2.8.9       9.8.4.9       1.4.3       7.5       2.7.3.1       8.1 7.2       7.8.5.5       1.0.5.7       4.4.5.9       1.0.4.4       1.0.2       2         Mean       0.64       4.30       31.8       46.4       97.5       2.64       2.62       34.1       1.4.9       3.37       0.33       0.37       0.33       0         Max       2.0       1.2       1.4.2       7.94       665       85       12.7       7.7       0.4       0.3       0         Min       0.1       0.5       1.9       2.0       2.4       62       92       12       5.9       0.4       0.3 <td>2.8</td> <td>a .4</td> <td>a 3.0</td> <td>b 7.0</td> <td>b 24</td> <td>* 65</td> <td>221</td> <td>92</td> <td>19</td> <td>8.0</td> <td>.8</td> <td>.3</td> <td>.9</td>   | 2.8    | a .4        | a 3.0      | b 7.0       | b 24       | * 65                 | 221                           | 92      | 19                | 8.0     | .8    | .3              | .9                   |
| 30       a .4       a .3         Total       1 9.9       1 2 8.9       9 8 4.9       1.4 3 7.5       2.7 3 1       8.1 7 2       7.8 5 5       1.0 5 7       4 4 5.9       1 0 4.4       1 0.2       2       0 .33       0 .33       0 .33       0 .33       0 .33       0 .33       0 .33       0 .4       0 .3       0 .4       0 .3       0 .4       0 .3       0 .4       0 .3       0 .4       0 .3       0 .4       0 .3       0 .4       0 .3       0 .4       0 .3       0  | 29     | a .4        | a 4.0      | b 5.0       | D 24       |                      | 776                           | 120     | 10                | 8.0     | .8    | .3              | .9                   |
| 11       a       .4       1.9       0       2.4       1.9.4       1.2       .4       .3         Total       1.9.9       1.2.8.9       9.8.4.9       1.4.3       7.5       2.7.3       1       8.1.7       7.8.5       1.0.5       7       4.4.5.9       1.0.4.4       1.0.2       2         Mean       0.64       4.30       31.8       46.4       97.5       264       262       34.1       14.9       3.37       0.33       0.3         Max       2.0       12       145       171       442       794       665       85       127       7.7       0.4       0.3       0.3         Min       0.1       0.5       1.9       2.0       24       62       92       12       5.9       0.4       0.3       0.4         Min       0.1       0.5       1.9       2.0       2.4       62       92       12       5.9       0.4       0.3       0.3         Cal yr       1969 :       Mean       10.2       Max       280       Min       0       Ac-ft       7,380         Wir yr       1969 :       Mean       62.9       Max       794       Min       0.1   | 30     | a .4        | a 7.0      | 0 4.0       | b 24       |                      | 794                           | 100     | 1 2               | 0.0     | .0    | .J              | .9                   |
| Total       1 9.9       1 2 8.9       9 8 4.9       1.4 3 7.5       2.7 3 1       8.1 7 2       7.8 5 5       1.0 5 7       4 4 5.9       1 0 4.4       1 0.2       2         Mean       0.64       4.30       31.8       46.4       97.5       264       262       34.1       14.9       3.37       0.33       0.33       0.33       0.44       3.37       0.33       0.44       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       0.4       0.3       20       20       2.850       5.420       16.210       15.580       2.100       884       207       20<  | 11     | a .4        |            | 1.9         | 0 24       |                      | 1 2 4                         |         | 12                |         | .4    |                 |                      |
| Mean         0.64         4.30         31.8         46.4         97.5         264         262         34.1         14.9         3.37         0.33         0.33           Min         0.1         0.5         1.9         2.0         24         62         92         12         5.9         0.4         0.3         0.37         0.4         0.3         0.3         0.4         0.3         0.3         0.4         0.3         0.3         0.4         0.3         0.3         0.4         0  | Total  | 1 9 9       | 128.9      | 984.9       | 1.4 3 7.5  | 2.7 3 1              | 8.172                         | 7.8 5 5 | 1.0 5 7           | 4 4 5.9 | 104.4 | 10.2            | 21.8                 |
| Mix         2.0         12         145         171         442         794         665         85         127         7.7         0.4         0.3           Min         0.1         0.5         1.9         2.0         24         62         92         12         5.9         0.4         0.3         0.3           Ac-ft         39         256         1.950         2.850         5.420         16.210         15.580         2.100         884         207         20 <td< td=""><td>Mean</td><td>0.64</td><td>4.30</td><td>31.8</td><td>46.4</td><td>97.5</td><td>264</td><td>262</td><td>34.1</td><td>14.9</td><td>3.37</td><td>0.33</td><td>0.73</td></td<>  | Mean   | 0.64        | 4.30       | 31.8        | 46.4       | 97.5                 | 264                           | 262     | 34.1              | 14.9    | 3.37  | 0.33            | 0.73                 |
| Min       0.1       0.5       1.9       2.0       24       62       92       12       5.9       0.4       0.3         Ac-ft       39       256       1,950       2,850       5,420       16,210       15,580       2,100       884       207       20         Cal yr       1968 : Mean       10.2       Max       280       Min       0       Ac-ft       7,380         Wir yr       1969 : Mean       62.9       Max       794       Min       0.1       Ac-ft       45,560         *       Discharge measurement made on this day.       a       No gage height record.       EXHIBIT       3         b<       Stage-discharge relation affected by ice.       5       4       0       0       0   | Max    | 2.0         | 12         | 145         | 171        | 442                  | 794                           | 665     | 85                | 127     | 7.7   | -0.4            | 3.0                  |
| Ac-ft       39       256       1,950       2,850       5,420       16,210       15,580       2,100       884       207       20         Cal yr       1968 : Mean       10.2       Max       280       Min       0       Ac-ft       7,380         Wir yr       1969 : Mean       62.9       Max       794       Min       0.1       Ac-ft       45,560         *       Discharge measurement made on this day.       a       No gage height record.       PAGE       40F         b       Stage-discharge relation affected by ice.       5       5       7       0   | Min    | 0.1         | 0.5        | 1.9         | 2.0        | 24                   | 62                            | 92      | 12                | 5.9     | 0.4   | 0.3             | 0.3                  |
| Cal yr 1968 : Mean 10.2 Max 280 Min 0 Ac-ft 7,380<br>Wir yr 1969 : Mean 62.9 Max 794 Min 0.1 Ac-ft 45,560<br>* Discharge measurement made on this day.<br>a No gage height record.<br>b Stage-discharge relation affected by ice.<br>EXHIBIT 3<br>PAGE 4 OF  | Ac-ft  | 39          | 256        | 1,950       | 2,850      | 5,420                | 16,210                        | 15,580  | 2,100             | 884     | 207   | 20              | 43                   |
| Cal yr 1968 : Mean 10.2 Max 280 Min O Ac-ft 7,380<br>Wir yr 1969 : Mean 62.9 Max 794 Min 0.1 Ac-ft 45,560<br>* Discharge measurement made on this day.<br>a No gage height record.<br>b Stage-discharge relation affected by ice.<br>EXHIBIT 3<br>PAGE 4 OF  |        | · · · · · · | and a set  |             | and an and | and a service second | and state of the later of the |         | which the ball at |         |       | Sal and Artista | · · · · · · · ·      |
| Wir yr 1969 : Mean 62.9 Max 794 Min 0.1 Ac-fi 45,560<br>* Discharge measurement made on this day.<br>a No gage height record.<br>b Stage-discharge relation affected by ice.<br>EXHIBIT 3<br>PAGE 4 OF   | Cal yr | 1968 :      | Mean 10    | .2 Ma       | * 280      | ) M                  | In 0                          | Ac-     | n 7,38            | 0       |       |                 |                      |
| * Discharge measurement made on this day.<br>a No gage height record.<br>b Stage-discharge relation affected by ice.<br>EXHIBIT<br>PAGE _4OF.  | Wir gr | 1969 :      | Mean 62    | .9 Ma       | × 794      | MU                   | n 0.                          | 1 Ac-   | 45,56             | 0       | -     |                 | 7                    |
| * Discharge measurement made on this day.<br>a No gage height record.<br>b Stage-discharge relation affected by ice.<br>PAGE <u>4</u> OF.  |        |             |            |             |            |                      |                               |         |                   |         | FXI   | IIRIT           | 2                    |
| a No gage height record.<br>b Stage-discharge relation affected by ice.<br>PAGE <u>4</u> OF.   | * Dis  | charge mea  | surement m | ade on this | s day.     |                      |                               |         |                   |         | LAI   | IIDIT _         | Concentration of the |
| b Stage-discharge relation affected by ice.  | a No   | gage heigh  | it record. |             |            |                      |                               |         |                   |         | PAC   | F 4             | NE 13                |
|  | b S'ta | ge-dischar  | ge relatio | n affected  | by ice.    |                      |                               |         |                   |         | inc   | the main        | 01                   |

b Stage-discharge relation affected by ice.

#### JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION .-- Lat 45°20'15", long 120°03'40", in NW±SW± sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

PERIOD OF RECORD .-- April 12, 1965, to current year.

CAGE.--Water-stage recorder.

EXTREMES.--Current year: Maximum discharge, 2,420 cfs Jan. 23 (gage height, 4.73 ft); minimum, 0.1 cfs Aug. 25, 26

(gage height, 0.73 ft).

Period of record: Maximum recorded discharge, 2,420 cfs Jan. 23, 1970 (gage height, 4.73 ft); no flow at times. REMARKS. -- Records good.

LI p M d

97

|        |           |  | Discha      | ige, in cub    | ic reet per | Second for | the year of  | ending septe | ember 30, 19 | 10        |                     |       |
|--------|-----------|--|-------------|----------------|-------------|------------|--------------|--------------|--------------|-----------|---------------------|-------|
| Day    | Oct.      | Nov.                                   | Dec.        | Jan.           | Feb.        | Mar.       | April        | May          | June         | July      | Aug.                | Sept. |
| 1      | 0.9       | 3.3                                    | 4.4         | B.6            | 157         | 67         | 93           | 4 3          | 7.5          | 2.6       | 0.5.                | 0.2   |
| 2      | .9        | 3.3                                    | 4.2         | 8.0            | 138         | 74         | 87           | 39           | 6.8          | 2.6       | .5                  | .3    |
| 1      | 1.1       | 3.3                                    | 3.9         | 0.2            | 128         | 12         | 79           | 1 35         | 2.8          | 2.4       | .6                  | .3    |
|        |           | 3.0                                    | 4.2         | 4.4            | 101         | 7 2        | 72           | 1 2 2        | 4.0          | 2.9       | .5                  | .F.   |
|        |           | 4.4                                    | 4.4         | 7.1            | 112         | 07         | 74           | 20           | 4.1          | 2.2       | 4                   |       |
| 7      | 1.1       | 4.7                                    | 4.7         | 7.1            | 203         | 355        | 76           | 29           | 4.8          | 1.6       | .4                  | .8    |
| 8      | 1.1       | 4.7                                    | 4.4         | 8.0            | 192         | 350        | 72           | 27           | 6.5          | 1.6       | .9                  | 1.0   |
| 9      | 1.1       | 4.7                                    | 4.4         | 22             | 172         | 234        | 67           | 35           | 7.5          | 1.6       |                     | 1.2   |
| 10     | 1.1       | 4.4                                    | 4.4         | 78             | 154         | 186        | 72           | 39           | -8-0         | 1.4       | .4                  | 12    |
| 11     | 1.1       | 4.4                                    | 5.0         | 52             | 148         | 160        | 76           | 35           | 8.4          | 1.2       | .3                  | 12    |
| 12     | 1.1       | 4.4                                    | 5.6         | 121            | 145         | 157        | 67           | 33           | 8.4          | 1.2       |                     | 12    |
| 13     | .9        | 4.4                                    | 5.9         | 53             | 365         | 157        | 60           | 36           | 10           | · 1.4     | .3                  | 1.2   |
| 14     | .9        | 4.4                                    | 6.2         | 28             | 305         | 217        | 26           | 31           |              | 1.2       | .2                  | 1.4   |
| -15    |           | 4.4                                    | 6.5         | 60             | 242         | 281        | 22           | 26           |              | 1.0       | .2                  | 1.4   |
| 10     | 1.5       | 44                                     | 6.8         | 60             | 317         | 224        | 47           | 20           | 61           | 1.0       | .2                  | 1.4   |
| 18     | 15        | * 4.4                                  | 77          | 157            | 228         | 189        | 4 3          | 19           | 1.5          | .8        | * .2                | 1.4   |
| 19     | 1.3       | 4.4                                    | 8.0         | 232            | 178         | 160        | 46           | 18           | 6.1          | .0        | 2                   | 1.4   |
| 20     | 1.3       | 4.4                                    | 10          | *332           | 160         | 145        | 48           | 16           | 5.5          | * 6       | -2                  | 1.4   |
| 21     | 1.3       | 4.2                                    | 21          | 542            | 145         | 132        | * 46         | 14           | 4.4          | .5        |                     | 1.4   |
| 22     | 1.3       | 4.2                                    | 34          | 630            | 1 3 0       | 120        | 4 3          | *13          | * 3.5        | .5        |                     | 1.0   |
| 23     | . 1.3     | 4.2                                    | * 2 8       | 1.0 9 0        | 114         | 112        | 4 1          | 12           | 3.2          | .6        | .1                  | * 1.6 |
| 24     | 1.5       | 4.2                                    | 21          | 1.660          | 105         | 105        | 39           | 11           | 3.2          | .6        | .1                  | 1.6   |
| 25     | 1.5       | 4.4                                    | 17          | 640            | 97          | 99         | 40           | (9.8)        | 2.9          | .8        | .1                  | 1.6   |
| 26     | 1.7       | 4.4                                    | 11          | 680            | 91          | 91         | 42           |              | 2.0          | .8        | .1                  | 1.6   |
| 27     | * 2.0     | 4.4                                    | 12          | *465           | 85          | 9 1        | 45           | 7.5          | 2.5          | 1.0       | .1                  | 1.6   |
| 28     | 2.4       | 4.4                                    | 11          | 325            | 0 / .       | 8 9        | 45           | 8.0          | 2.6          | .8        | .1                  | 1.6   |
| 10     | 2.0       | 4.4                                    | 10          | 245            |             | 91         | 45           | 8.4          | 2.9          | .8        | .1                  | 1.4   |
| 11     | 1.0       |  | 9.2         | 200            |             | 107        |              | 8.4          |              | .0        | -2                  | 1.4   |
|        | 7.0       |  |             |                |             |            | THE PROPERTY |              |              | 0.        | .2.                 |       |
| Total  | 4 3.7     | 1 2 8.3                                | 301.4       | 8.182.2        | 4.6 2 3     | 4.6 3 3    | 1.7 3 9      | 7 0 6.5      | 179.9        | 3 8.1     | 8.0                 | 3 6.2 |
| Mean   | 1.41      | 4.28                                   | 9.72        | 264            | 165         | 149        | 58.0         | 22.8         | 6.00         | 1.23      | 0.26                | 1.21  |
| Max    | 3.0       | 4.7                                    | 34          | 1,660          | 365         | 355        | 93           | • 43         | 12           | 2.9       | 0.6                 | 1.6   |
| Min    | 0.9       | 3.3                                    | 3.9         | 4.4            | 85          | 67         | 39           | 7.5          | 2.6          | 0.5       | 0.1                 | 0.2   |
| Ac-ft  | .87       | 254                                    | 598         | 16,230         | 9,170       | 9,190      | 3,450        | 1,400        | 357          |           | 16                  | 72    |
| Cal    | 1969 :    | Mean 61.                               | 1 Ma        | 794            |             | 0.1        | Ar           | ft 44 25     | 0            |           |                     |       |
| Wir Tr | 1970 :    | Mean 56.                               | 5 Ma        | 1,660          | Mi          | n 0.1      | Ac           | 11 40.90     | 0            | -         |                     | 3     |
|        |           |  |             | and the second |             |            |              |              |              | FXH       | IBIT                | 2     |
| + D!-  | charge me | asurement m                            | ade on this | day.           |             |            |              |              |              | En contra |                     |       |
| DIS    |           | Cardel Control Control Control Control |             |                |             |            |              |              |              | PAG       | - 5                 | DF/3  |
|        |           |  |             |                |             |            |              |              |              | 110       | And an and a second |       |

JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION .-- Lat 45°20'15", long 120°03'40", in NWESWE sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

DRAINAGE AREA. -- 350 sq mi.

PERIOD OF RECORD. -- April 12, 1965 to current year.

GAGE .-- Water-stage recorder.

AVERAGE DISCHARGE.--6 years (1965-71), 37.7 cfs (27,310 acre-ft per year).

EXTREMES. -- Current year: Maximum discharge, 774 cfs Jan. 20 (gage height, 3.52 ft); no flow Aug. 6-27.

Period of record: Maximum recorded discharge, 2,420 cfs Jan. 23, 1970 (gage height, 4.73 ft); no flow at times. REMARKS. -- Records good.

| Day | Oct.     | Nov.     | Dec.   | Jan.         | Feb.  | Mar.   | April   | May   | June    | July  | Aug. | Sept. |
|-----|----------|----------|--------|--------------|-------|--------|---------|-------|---------|-------|------|-------|
| 1   | 1.4      | 2.4      | 11     | 12           | 117   | 30     | 142     | . 58  | 20      | 2.6   | 0.1  | 0.    |
| 2   | 1.4      | 2.4      | 13     | 6.8          | 101   | 25     | 133     | 54    | 22      | 2.3   | .1   |       |
| 3   | 1.4      | 2.6      | 13     | b 6.0        | 77    | 33     | 126     | 50    | 18      | 1.8   | .1   | • •   |
| 4   | 1.2      | 2.6      | 1 1    | b 5.4        | 74    | 30     | 122     | 44    | 18      | 1.5   | .1   |       |
| 5   | 1.2      | 2.9      | 11     | b 5.0        | 59    | 25     | 145     | 40    | 16      | 1.3   | .1   |       |
| 6   | 1.2      | ).2      | 11     | b 5.8        | 4 4   | 25     | 126     | 38    | 14      | 1.3   | 0    |       |
| 7   | 1.4      | 3.8      | 1 9    | ь 7.0        | . 43  | 28     | 124     | 34    | 12      | 1.0   | 0    |       |
|     | 1.6      | 4.1      | 4 8    | 610          | 4 3   | 24     | 103     | 30    | 11      | .9    | 0    |       |
| 9   | 1.6      | 4.1      | 39     | 1 3          | 43    | 26     | 99      | 27    | 10      | 1.0   | 0    |       |
| 10  | 1.6      | 4.1      | 29     | 24           | 48    | 25     | 97      | 25    | 10      | 2.0   | 0    |       |
| 11  | 1.4      | 5.8      | 24     | 33           | 67    | 2 9    | 90      | 22    | 10      | 2.0   | 0    |       |
| 12  | 1.4      | 5.8      | 20     | 29           | 6 2   | 4 4    | 84      | 20    | 10      | 1.5   | 0 .  |       |
| 13  | 1.4      | 6.5      | 15     | 2 2          | 60    | 50     | 76      | 22    | 9.6     | 1.0   | 0    |       |
| 14  | 1.4      | 6.5      | 18     | 2.8          | 59    | 43     | 69      | 23    | 8.3     | .8    | 0    |       |
| 15  | 1.4      | 6.5      | 18     | 32           | 67    | .4 3   | 65      | . 21  | 7.4     | · .8  | 0    |       |
| 16  | 1.4      | * 5.8    | 18     | 8 9          | 64    | 37     | 60      | 22    | 6.7     | .7    | 0    |       |
| 17  | 1.4      | 5.8      | 16     | 480          | 54    | 34     | 65      | 20    | 5.0     | .7    | 0    |       |
| 18  | 1.4      | 6.5      | 1 1    | 610          | 50    | * 32   | 70      | 18    | 6.7     | .7    | 0    |       |
| 19  | 1.4      | 6.5      | 12     | 574          | 46    | 32     | 65      | 17    | 1.1 8   | .6    | 0    |       |
| 20  | 1.6      | 6.1      | 14     | 518          | . 4 3 | 33.    | * 58    | 16    | 7.4     | * :6  | 0    |       |
| 21  | 1.6      | 6.8      | * 13   | 232          | JB    | 37     | 69      | 16    | 5.6     | .5    | 0    |       |
| 22  | 1.6      | 5.5      | 1 3    | 158          | * 40  | 4 8    | 93      | 15    | 5.0     | .4    | 0    |       |
| 21  | 1.6      | 6.1      | 12     | 1 3 1        | 4 3   | 140    | 103     | 14    | (33)    | .4    | 0    |       |
| 24  | 1.6      | 11       | 12     | 113          | 4 4   | 3 3 0  | 101     | 12    | 2.0     | .4    | 0    |       |
| 25  | 1.8      | 16       | 12     | 99           | 4 3   | 276    | 9 ?     | * 12  | * 3.6   | .3    | 0    |       |
| 26  | 1.8      | 16       | 9.8    | * 92         | 10    | *5 0 0 | 91      | 18    | J.J     | .3    | 0    |       |
| 27  | 2.0      | 13       | 12     | 90           | 35    | 310    | 8 3     | 27    | 3.3     | .3    | 0    |       |
| 28  | * 2.0    | 11       | 12     | 86           | 30    | 216    | 74      | 23    | 3.3     | .2    | .1   |       |
| 29  | 2.0      | 11       | 12     | 79           |       | 219    | 69      | 20    | 3.6     | .2    | .1   |       |
| 30  | 2.0      | 11       | 11     | 83           |       | 216    | 6 ?     | 12    | 3.3     | .2    | .1   |       |
| 11  | 2.2      |          | 12     | 111          |       | 177    |         | 14    |         | .1    | .1 - |       |
|     | 4 8 4    | 2014     | 5018   | 17 0         | 1524  | 22.2.4 | 2758    | 784   | 2726    | 284   |      |       |
| al  |          | 2 0 1 .4 |        | and to water |       | 3.116  | 6,1 7 0 | 104   | 2 . 2.0 | 2 0.4 | 0.9  | 14.   |
| na: | 1.56     | 6.71     | 16.2   | 122          | 54.4  | 101    | 91.9    | 25.3  | 9.10    | 0.92  | 0.03 | 0.4   |
| IX  | 2.2      | 16       | 48     | 610          | 117   | 500    | 145     | 58    | 22      | -2.6  | 0.1  | 0.    |
|     | 1.2      | 2.4      | 9.8    | 5.0          | 30    | 24     | 58      | 12    | 3.3     | 0.1   | 0    | 0.    |
| -ft | 96       | 399      | 995    | 7,510        | 3,020 | 6,180  | 5,470   | 1,560 | 541     | 56    | 1.8  | 2     |
| 77  | 1970 : * | fean 57  | .3 Mas | 1.66         | 0 Mir | 0.1    | Ac-ft   | 41.4  | 50      |       |      |       |
| 1   |          | (ean     | 7 Mar  |              | o Mir |        | Ac.ft   | 75.0  | 150     |       |      |       |

Discharge measurement made on this day.
 b Stage-discharge relation affected by ice.



OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION .-- Lat 45°20'15", long 120°03'40", in NW15W1 sec.3, T.3 5., R.22 E., Gilliam County, on left bank about 200 ft

downstream from county bridge, and 15 miles northeast of Condon.

DRAINAGE AREA. -- 350 sq mi.

PERIOD OF RECORD. -- April 12, 1965 to current year.

GAGE .-- Water-stage recorder.

AVERAGE DISCHARGE.--7 years (1965-72), 41.6 cfs (30,140 acre-ft per year).

EXTREMES .-- Current year: Maximum discharge, 12,500 cfs June 8 (gage height, 8.67 ft); no flow at times.

Period of record: Maximum recorded discharge, 12,500 cfs June 8, 1972 (gage height, 8.87 ft); no flow at times. REMARKS. -- Records good.

| Day | Oct.  | Nov.  | Dec.  | Jan.    | Feb.       | Mar.    | April | May     | June    | July   | Aug. | Sept. |
|-----|-------|-------|-------|---------|------------|---------|-------|---------|---------|--------|------|-------|
| 1   | 8.0   | 2.0   | 4 3   | b 1 8   | 544        | 27A     | 8 3   | 4 0     | 6.8     | a 0.5  | O    | С     |
| 2   | .7    | 2.0   | 34    | b 17    | 4 5        | 218     | 78    | 39      | 6.1     | a .5   | 0    | 0     |
| 3   | .7    | 2.0   | 32    | 16      | 45         | 395     | 74    | ):      | 6.1     | a .5   | 2    | 0     |
| 4   | .7    | 2.3   | 28    | 15      | 60         | 294     | 72    | ))      | 6.1     | a .5   | 0    | 0     |
| 5   | .7    | 2.3   | 28    | 516     | 8 0        | 290     | 78    | 28      | 6.1     | a .5   | 0    | С     |
| 6   | .7    | 2.3   | 147   | b 1 A   | 88         | * 314   | 6 B   | 25      | 2.5     | a .6   | 0    | 0     |
| 7   | .6    | 2.6   | 101   | P 2 5   | 86         | 266     | 8 ?   | 23      | 6.4     | a .7   | 0    | 0     |
|     | .6    | 2.6   | 69    | 27      | * 90       | 222     | 74    | 30      | 1.200   | a 1.0  | 0    | 0     |
| 9   | .6    | 2.6   | 6.0   | b 2 6   | 6 8        | 218     | 66    | 4 5     | 3.640   | a .8   | 0    | 0     |
| 10  | .6    | 2.8   | 650   | 26      | 6 2        | 298     | 60    | 41      | a 50    | a .7   | 0    | 0     |
| 11  | .6    | 3.1   | b 4 5 | * 27    | 55         | 3 3 0   | 57    | )6      | a 20    | a .6   | 0    | 0     |
| 12  | .7    | 3.9   | b 4 2 | b 27    | 55         | 390     | 59    | 29      | a 10    | a * .6 | 0    | 0     |
| 13  | .7    | 4.3   | b40   | b 27    | . 72       | 550     | 64    | 25      | a 8.0   | a .6   | 0    | 0     |
| 14  | .7    | 4.3   | b 3 9 | b 28    | 9 ?        | 4 3 6   | 72    | 22      | a 6.0   | a .5   | 0    | 0     |
| 15  | .8    | 4.6   | b 3 R | b 28    | <b>月</b> 4 | 310     | 86    | 19      | a + 5.0 | a .5   | 0    | 0     |
| 16  | .8    | 5.0   | * 38  | b 29    | 145        | 278     | 9 ?   | 1.8     | 3.8     | a .5   | 0    | 0     |
| 17  | .9    | 5.3   | 35    | 31      | 270        | 266     | 98    | 16      | 3.2     | a .4   | 0    | 0     |
| 8   | .9    | * 5.C | 37    | 34      | 278        | 250     | 90    | 17      | 2.2     | a .4   | 0    | 0     |
| 9   | 1.0   | 5.0   | 38    | 74      | 258        | 212     | 84    | 18      | 1.5     | .4     | 0.6  | 0     |
| 10  | * 1.C | 5.0   | 38    | 148     | 3 3 5      | 185     | 78    | 16      | 1.0     | .5     | .7   | 0     |
| 1   | 1.0   | 5.0   | 37    | 687     | 250        | 167     | 74    | 10      | 1.3     | .6     | 1.1  | 0     |
| 2   | 1.3   | 5.0   | 35    | 4 2 5   | 212        | 158     | 7?    | 33      | .8      | .5     | .7   | 0     |
| 3   | 1.5   | 5.3   | 4 6   | 273     | 185        | 161     | 66    | )2      | .7      | .5     | .6   | 0     |
| 4   | 1.5   | 5.6   | 50    | 179     | 155        | 142     | 6 ?   | * 25    | .8      | .5     | * .5 |       |
| 5   | 1.5   | 6.3   | 50    | 142     | 1 3 5      | 128     | 59    | 23      | .8      | .5     | .1   |       |
| 6   | 1.3   | 7.9   | 50    | 96      | 126        | 116     | 55    | 19      | .6      | .4     | 0    | *     |
| 7   | 1.3   | 20    | 38    | 43      | 128        | 108     | 51    | 16      | .6      | .4     | 0    |       |
|     | 1.5   | 28    | 27    | 6 4 2   | 350        | 103     | 47    | 13      | .6      | .4     | 0    |       |
| 9   | 1.3   | 24    | 623   | 6 4 1   | 4 2 5      | * 94    | 45    | 11      | .5      |        | 0    |       |
| 0   | 1.5   | 43    | b 2 1 | 641     |            | 88      | 4 4   | 9.5     | a .5    | .1     | 0    |       |
| 1   | 2.0   |       | 620   | 642     |            | 84      |       | 7.7     |         | 0      | 0    |       |
|     | 30.5  | 219.1 | 1.379 | 2.6 6 2 | 4.290      | 7.3 4 8 | 2.099 | 7 5 8.2 | 5.001.1 | 15.5   | 4.3  | 4     |
|     | 0.98  | 7.30  | 44.5  | 85.9    | 148        | 237     | 70.0  | 74.5    | (167)   | 0.50   | 0.14 | 0     |
|     | 2.0   | 43    | 147   | 687     | 425        | 550     | 98    | 45      | 3.650   | 1.0    | 1.1  | 0.    |
|     | 0.6   | 2.0   | 20    | 15      | 44         | 84      | 44    | 7.7     | 5,040   | 0      |      |       |
|     | 60    | 435   | 2.740 | 5,280   | 8.510      | 14.570  | 4 160 | 1.500   | 9,920   | 11     | A S  | 8     |
| IN  | 00    | 455   |       | 51100   | 01010      |         | 4,100 | 1,000   | 1,120   | 31     | 0.5  | 0     |

\* Discharge measurement made on this day.

a No gage height record. b Stage-discharge relation affected by ice.



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#### OFFICE OF STATE ENGINEER-WATER RESOURCES DEPARTMENT

JOHN DAY RIVER BASIN

#### 14-0474. Rock Creek above Cayuse Canyon, near Condon, Oreg.

LOCATION.--Lat 45"20'15", long 120"03'40", in NWtSWt sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

(60 m) downstream from county bridge, and 15 mi (24 km) northeast of Condon.

DRAINAGE AREA. -- 350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD .-- April 12, 1965 to current year.

GAGE. -- Water-stage recorder.

AVERACE DISCHARGE. -- 8 years (1965-73), .37.2 ft<sup>3</sup>/s (1.05 m<sup>3</sup>/s), 26,950 acre-ft/yr (33.2 hm<sup>3</sup>/yr).

EXTREMES. -- Current year: Maximum discharge undetermined; no flow June 30 to Sept. 23.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft (2.704 m); no flow at times.

REMARKS .-- Records good.

J

REVISIONS (WATER YEARS) .-- 1972. Revised figures of discharge, in cubic feet per second, for the water year 1972, superceding those published in 1972, are given herewith:

| Date       | Discharge  | Honth                   | ft /s-days | Maximum | Hean    | Acre-ft |
|------------|------------|-------------------------|------------|---------|---------|---------|
| ne 9, 1972 | 300 ·      | June 1972               | 1,661.1    | 1,200   | 55.4    | 3,290   |
|            | Water year | ft <sup>3</sup> /s-days | Maximum    | Hean    | Acre-ft |         |
|            | 1972       | 20,471.1                | 1,200      | 55.9    | 40,600  |         |

| Day      | Oct.     | Nov.    | Dec    | Jan.    | Feb.    | Mar.    | April | May  | June | July | Aug.   | Sept.  |
|----------|----------|---------|--------|---------|---------|---------|-------|------|------|------|--------|--------|
| 1        | 16       | 1.1     | 5.1    | 21      | 1.6     | 124     | 4.4   | 0.0  | 1.2  |      |        | o ep a |
| 2        | .6       | 1.2     | 5.1    | 17      | 17      | 120     | 4.2   | 0,0  | 1.2  |      |        |        |
| 3        | .6       | 16      | 5.0    | 15      | 17      | 121     | 35    | 7.9  | 1.2  |      |        | 5      |
| 4        | .6       | 2.4     | 4.5    | 11      | 1.6     | 8 7     | 33    | 9,4  | 1.1  |      |        | 1      |
| 5        | .6       | ?.6     | 4.0    | 1?      | .l =    | 74      | 35    | 02   | 1.0  |      |        | 2      |
| 6        | .6       | 2.6     | 3.0    | 11.     | 2 0     | 6 4     | 3.5   | 5, a | 1.2  |      |        | •      |
| 7        | .6       | 3.0     | 2.9    | 10      | 17      | 64      | 34    | 7.3  | 1.0  |      |        | 1      |
|          | .6       | 1.0     | 2.8    | 1)      | 15      | 50      | 31    | 6.7  | 1.0  |      |        | •      |
| 9        | .6       | 2.2     | 2.0    | 1 3     | 10      | 57      | 30    |      | .9   |      |        | Э      |
| 10       | .7       | 3.6     | 3.5    | 13      | 1 1     | 61      | 50    |      |      |      |        | 2      |
| 11       | 1.0      | 3.4     | 2.5    | 20      | 1 .     | 16      | 20    | 17   |      |      |        | 2      |
| 11       | 15       | 3.4     | 2.8    | 6.6     | 1.0     | 51      | 21    | 4.1  | 1.2  |      |        | 3      |
| 11       | 12       | 3.4     | 2.8    | 111     | 1.8     | 10      | 12    | 12   | 7    |      |        |        |
| 1.       | 1.0      | 1.6     | 2.8    | 9.2     | 1 0     | 4.6     | 28    | 2.5  |      |      |        | 5      |
| 16       | C        | 1.6     | 4.0    | 161     | 20      | 43      | 24    | 2.2  | .0   |      |        |        |
| 17       | c        | 4.1     | 10     | 200     | 2.4     | 47      | 24    | 2.1  | .6   |      |        |        |
| 18       | .9       | 4.1     | 2.6    | 132     | 25      | 47      | 2.6   | 2.5  | 6    |      |        |        |
| 19       | .0       | 4.1     | 24     | 82      | 25      | 4 4     | 2 "   | 1.8  | .6   |      |        |        |
| 20       | .9       | 4.1     | 24     | 55      | 25      | 4 3     | 2.9   | 1.6  | .5   |      |        | 2      |
| 21       | .9       | 4.1     | 33     | 20      | 24      | 4 3     | Su    | 1.4  | .5   |      |        | ,      |
| 22       | 8.       | 3.5     | 84     | 35      | 21      | 4 ?     | 25    | 1.2  | .5   |      |        | ;      |
| 23       | .8       | 3.6     | 7 ?    | 3 "     | 24      | 40      | 23    | 1.2  | .5   |      | i      | .1     |
| 24       | .c       | 1.5     | 74     | 34      | 24      | 37      | 21    | 1.7  | .4   |      |        | .1     |
| 25       | .º.      | 3.5     | 64     | 3?      | 5       | 4 2     | 10    | 5.0  | .7   |      |        | .1     |
| 26       | .9       | 1.8     | 47     | 1 4     | 4 9 1   | 4 2     | 14    | 5.0  | .5   |      |        | .1     |
| 27       | 1.0      | 4.3     | 42     | 1.6     | 21      | 4 3     | 12    | 1.P  | .4   |      |        | .1     |
| 28       |          | 51      | 12     | 26      | 0.4     | 321     | 10    | 1.7  | -2   |      |        | .1     |
| 29       |          | 5.1     | 28     | 26-     |         | 14      | 0     | 1.4  | 20   |      |        | .1     |
| 30 1     |          | 2.1     | 24     | 21 -    |         | 10      | 0.0   | 1.2  | 1.6  |      | -      |        |
| 31       | 1.1      |         |        |         |         | a.j     |       | 1.4  |      |      |        |        |
|          | 260      | 104.0   | 582.0  | 1.4.2.3 | 576     | 1.7.7.8 | 9156  | 1244 | 215  | ,    |        |        |
| -        | 0.87     | 1.47    | 21.9   | 45.3    | 26 1    | 57 /    | 26.0  | 1.01 | 0.72 | j    |        |        |
| iean .   | 1.5      | 5.1     | 84     | 200     | 64      | 129     | 20.9  |      | 0.72 | 1    |        | 0.02   |
|          | 0.6      | 1.1     | 2.8    | 10      | 15      | 36      | 0.6   | 1.2  | 1.2  | 2    |        | 0.1    |
| e.ft     | 53       | 206     | 1.350  | 2.780   | 1.340   | 3, 530  | 1,600 | 267  | 43   | 3    | :      |        |
| te-in    |          |         | 11330  |         | 1,540   | 5,550   | 1,000 |      | 43   |      |        | 1.4    |
| al yr    | 1972 : 1 | Mean 53 | .7 Max | 1,2     | 00 Mile | 0       | Ac-II | 38,  | 980  |      |        |        |
| u sr     | 19/3 : 1 | 15      |        | 2       | 00 344  | 0       | Ac-11 | 11,  | 150  | -    |        | 2      |
|          |          |         |        |         |         |         |       |      |      | -X   | HIRIT  |        |
| 0.00-114 |          |         |        |         |         |         |       |      |      | LA   | IIDII  |        |
|          |          |         |        |         |         |         |       |      |      | DA   | CE 8   | OF     |
|          |          |         |        |         |         |         |       |      |      | E A  | 175 () |        |

SP+43700-119

### JOHN DAY RIVER BASIN

14-0474. ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION .-- 45°20'15", long 120°03'40", in NW15W1 sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft

(60 m), downstream from county bridge, and 15 mi (24 km) northeast of Condon.

DRAINAGE AREA. -- 350 m1<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD .-- April 12, 1965 to current year.

CACE .-- Water-stage recorder.

AVERAGE DISCHARGE.--9 years (1965-74), 45.7 ft<sup>3</sup>/s (1.29 m<sup>3</sup>/s), 33,150 acre-ft/yr (40.9 hm<sup>3</sup>/yr).

EXTREMES.--Current year: Maximum discharge, 6,050 ft<sup>3</sup>/s (171 m<sup>3</sup>/s), Jan. 18, gage height, 6.87 ft (2.094 m); no flow Oct. 9.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s), June 8, 1972, gage height, 8.87 ft

(2.704 m); no flow at times.

REMARKS .-- Records good.

REVISIONS (WATER YEARS).--1972. See 1973 publication.

| Day    | Oct.   | · Nov.    | Dec.   | Jan.    | Feb.  | Mar.   | April   | May      | June  | July  | Aug. | Sept.                                   |
|--------|--------|-----------|--------|---------|-------|--------|---------|----------|-------|-------|------|---|
| 1      | 0.1    | 0.9       | 854    | 75      | 145   | 1 D R  | 365     | 116      | 12    | 0.7   | 0.4  | 0.1                                     |
| 2      | .1     | .9        | 380    | 70      | 118   | 112    | 3 3 2 2 | 110      | 11    | .7    | .4   | .1                                      |
| 3      | .1     | .8        | 179    | 7 0     | 104   | 92     | 246     | 96       | 10    | .7    | .4   | .1                                      |
| 4      | .1     | .9        | 113    | 7 0     | 102   | 94     | 222     | 86       | 11    | .7    |      | .1                                      |
| 5      | .1     | 1.1       | 16     | 7 3     | 9 R   | 90     | 229     | 78       | 11    | .7    |      |   |
| 6      | .1     | 1.2       | 49     | 70      | 80    | 102    | 254     | 70       | 14    | .8    |      | .!                                      |
| 7      | -1     | 1.7       | 6 2 6  | 10      | 96    | 50     | 218     | 62       | 1 3   | -1    |      | -1                                      |
|        | .1     | 2.6       | 258    | 70      | 90    | 70     | 1 8 5   | 59       | 8.6   | 0.    |      | -                                       |
| 9      | 0.     | 140       | 170    | 70      | 90    | 70     | 170     | 50       | 7.7   | .5    | 2    |   |
| 10     |        | 155       | 140    | 70      | 8.8   | 70     | 161     | 4 0      | 71    | .0    |      | ~ ~                                     |
|        |        | 312       | 1 1 2  | 7 2     | 8.8   | 92     | 152     | 41       | 6.4   | 1.1   | 2    | 42                                      |
| 11     |        | 208       | 108    | 8.0     | 82    | 102    | 135     | 3.8      | 5.9   | 1.3   | 2    | 2                                       |
| 14     |        | 118       | 90     | 20.0    | 82    | 120    | 130     | 17       | 5.9   | 12    | 2    | 2                                       |
| 15     |        | 96        | 88     | 1.0 0 0 | 90    | 120    | 126     | 38       | 4.8   | 1.2   | .2   | 2                                       |
| 16     | .1     | 155       | 143    | 2.120   | 161   | 286    | 124     | 16       | 4.6   | · 1.1 | 2    | 2                                       |
| 17     | .1     | 155       | 266    | 2.050   | 182   | 430    | 116     | 36       | 4.1   | 12    | 2    | 2                                       |
| 18     | .1     | 113       | 330    | 2.620   | 152   | 345    | 114     | 37       | 3.6   | 1.4   | .2   | 2                                       |
| 19     | .1     | 86        | 197    | 2.590   | 222   | 286    | 118     | 37       | 3.6   | 1.4   | 2    | 2                                       |
| 2.0    | .1     | 78        | 155    | 906     | 194   | 212    | 106     | 37       | . 3.4 | 1.3   | .2   | 2                                       |
| 21     | 2      | 68        | 956    | 442     | 167   | 191    | 96      | 34       | 3.2   | 1.2   | 2    | 2                                       |
| 22     | .2     | 63        | 295    | 322     | 135   | 191    | 90      | 30       | 3.0   | 1.1   | -1   | 2                                       |
| 23     | -2     | 57        | 347    | 254     | 124   | 182    | 122     | 27       | 2.8   | .9    |      | 2                                       |
| 24     | -2     | 24        | 224    | 220     | 120   | 170    | 224     | 26       | 2.6   | .0    |      | -2                                      |
| 2.5    | .2     | 25        | 107    | 209     | 114   |        | 230     | 24       | 2.4   | .7    |      | 2                                       |
| 26     | -2     | 49        | 8.6    | 101     | 100   | 200    | 176     | 22       | 1.8   | .6    |      | 2                                       |
| 27     | 2      | 70        | 124    | 1 4 2   | 0.0   | 274    | 176     | 21       | 1.5   | .6    |      | 2                                       |
| 2.8    | 2      | 400       | 121    | 128     | 3.0   | 246    | 148     | 16       | 1.4   | .0    |      | ~                                       |
| 29     |        | 782       | 96     | 118     |       | 538    | 124     | 15       | 1.1   | .2    |      | 40                                      |
| 30     | 5      | 102       | 82     | 118     |       | 460    |         | 11       | .7    |       |      | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ |
| - 11   | 0.     |           |        |         |       |        |         |          |       |       |      |   |
|        | 47     | 3.1221    | 7671   | 14.581  | 3.348 | 5774   | 5.289   | 1.4 3 2  | 1787  | 274   | 6.3  | 51                                      |
| LOCAL  | 0.15   | 111       | 247    | 470     | 120   | 186    | 176     | 45.2     | 5.96  | 0.86  | 0.20 | 0 17                                    |
| Man    | 0.6    | 782       | 854    | 7.620   | 222   | 538    | 365     | 116      | -14   | 1.4   | -0.4 | 0.2                                     |
| Min    | 0      | 0.8       | 82     | 70      | 82    | 70     | 90      | 13       | 0.9   | 0.4   | 0.1  | 0.1                                     |
| Acatt  | 9.3    | 6,590     | 15,220 | 28,920  | 6,640 | 11,450 | 10,490  | 2,780    | 354   | 54    | 12   | 10                                      |
|        |        |           |        |         |       |        |         |          |       |       |      |   |
| Cal ar | 1973 . | Mean 43.3 | Max    | 200     | MI    | a 0    | Ac-I    | 1 31,350 | -     |       |      |   |
| Wir Tr | 1974 1 | Mean 114  | Max    | 2,620   | ML    | . 0    | Ac-f    | 82,530   | -     |       |      |   |

Discharge, in cubic feet per second for the year ending September 30, 1974

#### WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION .-- Lat 45°20'15", long 120°03'40", in NWsSWs sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft (60 m) downstream from county bridge, and 15 mi (24 km) northeast of Condon.

DRAINAGE AREA .-- 350 m12 (906 km2).

PERIOD OF RECORD .-- April 1965 to current year.

GAGE.--Water-stage recorder.

AVERAGE DISCHARGE.--10 years (1965-75), 45.8 ft<sup>3</sup>/s (1.30 m<sup>3</sup>/s), 33,180 acre-ft/yr (40.9 hm<sup>3</sup>/yr). EXTREMES.--Current year: Maximum discharge, 496 ft<sup>3</sup>/s (14.0 m<sup>3</sup>/s) Mar. 2, gage height, 3.20 ft (0.975 m); no flow at times.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft (2.704 m); no flow at times.

REMARKS .-- Records good.

REVISIONS (WATER YEARS), -- 1972. See 1973 publication.

| Day  | Oct.       | Nov. | Dec. | Jan.  | Feb.  | Mar.  | April  | May    | June  | July  | Aug.   | Sept. |   |
|------|------------|------|------|-------|-------|-------|--------|--------|-------|-------|--------|-------|---|
| 1    | .2         | 1.4  | 3.8  | 5.9   | 4 0   | 375   | 254    | 164    | 21    | 2.4   | 0.1    | 0.2   |   |
| 2    | .2         | 1.4  | 3.8  | 5.4   | 38    | 395   | 218    | 152    | 22    | 2.2   | .1     | 2     |   |
| 3    | .3         | 1.4  | 4.1  | 5.6   | 30    | 278   | 236    | 152    | 22    | 1.8   | .1     | .2    |   |
| 4    | .3         | 1.4  | 4.1  | 6.1   | 28    | 206   | 218    | 148    | 21    | 1.6   | .1:    | .2    |   |
| 5    | .3         | 1.4  | 4.1  | 6.1   | 23    | 167   | 179    | 1.3.0  | 15    | 1.5   | .1     | .2    |   |
| 6    | .3         | 1.5  | 4.1  | 6.1   | 21    | 1 3 2 | 176    | 114    | 13    | 1.2   | .1     | .1    |   |
| 7    | .4         | 1.8  | 4.1  | 6.4   | 21    | 114   | 176    | 108    | 10    | 1.2   | .1     | .1    |   |
|      | .4         | 2.0  | 4.3  | 7.J   | 2 2   | 104   | 173    | 104    | 8.0   | 1.3   | .1     | .1    |   |
| 9    | .4         | 1.8  | 4.3  | 6.4   | 1 8   | 132   | 164    | 98     | 7.0   | 4.9   | .1     | .1    |   |
| 10   | 4          | 1.8  | 4.3  | 6.4   | 26    | 124   | 173    | 120    | 6.0   | 15    | .1     | .1    |   |
| 11   | .5         | 2.0  | 4.6  | 6.1   | 28    | 104   | 179    | 100    | 5.0   | 40    | .1     | .1    |   |
| 12   | .5         | 2.0  | 4.6  | 5.9   | 4 3   | 86    | 250    | 92     | 4.0   | . 2.4 | .1     | .1    |   |
| 13   | .5         | 1.8  | 4.6  | 7.7   | 212   | 78    | 165    | 8 2    | 3.4   | 1.3   | .1     | .1    |   |
| 14   | .5         | 1.8  | 4.6  | 8.6   | 179   | 66    | 350    | 72     | 3.0   | .7    | 0      | .1    |   |
| 15   | .6         | 1.8  | 4.8  | 9.9   | 110   | 6.4   | 274    | 6.2    | 2.5   | .6    | .)     | .1    |   |
| 14   | .0         | 1.8  | 4.8  | 12    | 102   | 64    | 246    | 51     | 2.1   | .5    | 0      | .1    |   |
| 17   | .0         | 2.0  | 4.0  | 18    | 12    | 6 2   | 212    | 45     | 2.0   | .5    | 2      | .1    |   |
| 18   | .1         | 2.0  | 4.0  | 4 3   | 02    | 62    | 197    | 4 1    | 2.0   | .5    | 0      | .1    |   |
| 19   |            | 2.0  | 4.0  | 20    | 231   | 130   | 212    | 37     | 2.4   | .4    | .1     | .1    |   |
| 20   | .1         | 2.01 | 4.C  |       | 9 2 : | 126   | 218    | 37     | 2.8   | .4    | .2     | .1    |   |
|      | .'         | 2.0  | 1.0  | 26    | 39    | 108   | 215    | 36     | 3.4   | .4    | .2     | .1    |   |
| "    | .0         | 2.0  | 5.01 | 2 2   | 0 4   | 5 8   | 222    | 35     | 3.6   |       | .2     | .1    |   |
|      | .0         | 3.0  | 5.4  | 23    | 0 3   | 90    | 218    | 28     | 3.2   |       | .2     | .1    |   |
|      | .0         | 2.4  | 5.0  | 100   | 5 6   | 94    | 220    | 26     | 2.8   | .2    | .2     | .1    |   |
|      | 0          | 1.4  | 61   | 215   | 5.0   | 1 2 8 | 395    | 24     | 2.6   | .2    | .2     | .1    |   |
|      | 1.0        | 14   | 61   | 136   | 57    | 1 4 0 | 200    | 22     | 2.6   | .2    | .2     | .1    |   |
|      | 1.2        | 14   | 6.4  | 6.4   | 111   | 1 2 8 | 240    | 21     | 2.4   | 2     | .2     | .1    |   |
|      | 1.4        | 3.4  | 8.2  | 5 3   | 1.7.4 | 1 5 0 | 200    | 19     | 2.4   | -2    | -2     | .1    |   |
| 10 1 | 14         | 16   |      |       |       | 2 4 4 | 170    | 19     | 2.2   |       | .2     | .1    |   |
|      | 1 3        | 10   | 5.4  | i.t   |       | 200   |        | 201    | 2.4   |       | .2     |       |   |
|      |            |      |      | 20    |       | 140   |        | 20     |       |       | .2     |       |   |
| 1.1  | 23.2       | 601  | 1528 | 9750  | 1161  | 4573  | 6001   | 2154   |       | 8.2.7 |        |       |   |
|      | 0.55       | 2 21 | 1 02 | 21 5  |       |       | 0.501  | 2156   | 201.8 | 0 2.1 | 3.8    | 3.5   |   |
|      | 0.05       | 2.51 | 4.93 | 31.5  | 02.9  | 148   | 22/    | 69.5   | 6.73  | 2.67  | 0.12   | 0.12  |   |
|      | 0.2        | 3.0  | 2.4  | 215   | 212   | 395   | 395    | 164    | 22    | 40    | 0.2    | 0.2   |   |
|      | 0.2        | 127  | 3.8  | 3.4   | 18    | 50    | 104    | 19     | 2.2   | 0.1   | 0      | 0.1   |   |
| m    | 40         | 13/  | 303  | 1,940 | 3,490 | 8,670 | 13,490 | 4,280  | 400   | 164   | 7.5    | 6.9   |   |
|      | 1074       | 84 5 | Max  | 2 620 |       | 0.1   |        | 61 200 |       |       |        |       |   |
| 1 77 | 1075       | 46.0 | Mar  | 305   | Alle  | 0.1   | Acti   | 32,220 |       |       |        |       | - |
| . 11 | 13/3 : 140 | 40.0 |      | 333   | 200   | 0     | Ac-fi  | 33,320 |       |       | EVILLE | TIC   | 2 |
|      |            |      |      |       |       |       |        |        |       |       | EAHIE  | 511   | 0 |
|      |            |      |      |       |       |       |        |        |       |       | DAOF   | 100   | F |
|      |            |      |      |       |       |       |        |        |       |       | DALL   | 10 0  |   |

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#### WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION.--Lat 45°20'15". long 120°03'40", in NW4SW4 sec.3, T.3 S., R.22 E., Gilliam County, on left bank about 200 ft (60 m) downstream from county bridge, and 15 mi (24 km) northeast of Condon.

DRAINAGE AREA.--350 m1<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD .-- April 1965 to current year.

GAGE.--Water-stage recorder.

AVERAGE DISCHARGE.--10 years (1965-75), 45.8 ft<sup>3</sup>/s (1.30 m<sup>3</sup>/s), 33,180 acre-ft/yr (40.9 hm<sup>3</sup>/yr). EXTREMES.--Current year: Maximum discharge, 496 ft<sup>3</sup>/s (14.0 m<sup>3</sup>/s) Mar. 2, gage height, 3.20 ft (0.975 m); no flow at times.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft (2.704 m); no flow at times.

REMARKS .-- Records good.

REVISIONS (WATER YEARS).--1972. See 1973 publication.

| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$  |        |          | -         |       | Discharge, in | cubic feet pe         | er second for | the year end         | ing Septembe | er 30, 1975 |       |       |       |
|---|--------|----------|-----------|-------|---------------|-----------------------|---------------|----------------------|--------------|-------------|-------|-------|-------|
| 1       2       1.4       3.6       5.5       4       0       3.7       5       2.5       4       1.6.4       2.1       2.4       0.1       0.2         3       3.1       1.4       4.1       5.6       3.0       2.7.6       2.1.6       1.5       2.2       2.2       1.1       2.3         4       3.1       1.4       4.1       6.1       2.3       2.7.6       1.4       4.6       1.2       1.7.9       1.1.0       1.5       1.1.3       1.4       4.1       6.1       2.3       1.6       1.1       1.1       1.1       2.1       1.4       1.2       1.1       1.1       2.1       1.4       1.1       2.1       1.4       1.3       2.2       1.4       1.3       2.2       1.4       1.3       1.2       1.1   | Day    | Oct.     | Nov.      | Dec.  | Jan,          | Feb.                  | Mar.          | April                | May          | June        | July  | Aug.  | Sept. |
| a       2       1.4       3.8       5.4       3.8       1.9       5       2.1       6       1.5       2.2       2.2       2.1       3.2         a       3.3       1.4       4.1       6.1       2.8       2.0       6       2.1       6       1.5       2.2       1.6       1.3       1.4       4.1       6.1       2.3       6       1.5       2.2       1.6       1.3       1.4       4.1       6.1       2.2         a       1.3       1.4       4.1       6.1       2.1       1.1       1.4       1.1       1.2       1.1       2.1       1.1       2.1       1.1       2.1       1.1       1.2       1.1       1.2       1.1       1.1       1.2       1.1 <th< td=""><td>1</td><td>.2</td><td>1.4</td><td>3.8</td><td>5.9</td><td>40</td><td>375</td><td>254</td><td>164</td><td>21</td><td>2.4</td><td>0.1</td><td>0.2</td></th<>  | 1      | .2       | 1.4       | 3.8   | 5.9           | 40                    | 375           | 254                  | 164          | 21          | 2.4   | 0.1   | 0.2   |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 2      | .2       | 1.4       | 3.8   | 5.4           | 38                    | 395           | 218                  | 152          | 22          | 2.2   |       | 2     |
| 4   | 3      | .3       | 1.4       | 4.1   | 5.6           | 30                    | 278           | 236                  | 152          | 22          | 1.8   |       | 2     |
| 3   | •      | .3       | 1.4       | 4.1   | 6.1           | 28                    | 206           | 218                  | 148          | 21          | 1.6   | .11   | 2     |
| 4       .3       1.5       4.1       6.1       21       1 J 2       1 7 6       1 1 4       1 3       1.2       1       1         1       4       1.8       4.1       6.4       21       1 1 4       1 7 6       1 1 4       1 3       1.2       1       1         1       4       1.8       4.3       6.4       2 6       1 2.4       1 7 3       1 0.4       9.0       1.3       1       1         1       4       1.8       4.3       6.4       2 6       1 2.4       1 7 3       1 0.0       6.0       1.5       1       1       1         1       4       1.8       4.3       6.4       2 6       1 2.4       1 7 3       1 0.0       6.0       1.5       1  | 5      | .3       | 1.4       | 4.1   | 6.1.          | 23                    | 167           | 179                  | 130          | 15          | 1.5   | .1    | .2    |
| 7       .4       1.8       4.1       6.4       21       1 1 4       1 7 6       1 0 8       1 0       1.2       1       1         9       .4       1.8       4.3       6.4       1 9       1 3 2       1 6 4       9 8       7.0       4.9       1       1       1         10       .4       1.8       4.3       6.4       2 6       1.24       1 7 3       1 0 0       6.0       1.5       1       1       1         11       .5       2.0       4.6       6.1       2 8       1 0 4       1 7 9       1 0 0       5.0       4 0       .1       .1       .1         11       .5       2.0       4.6       5.9       4       8 6       2 5 0       9 2       4.0       .2.4       .1       .1       .1         11       .5       1.8       4.6       5.0       1 7 9       6 6       3 5 0       7 2       .0       .7       0       .1       .1       .1       .1       .1       .1       .5       0       .1       .1       .1       .1       .1       .1       .1       .1       .1       .1       .1       .1       .1       .1   | 6      | .3       | 1.5       | 4,1   | 6.1           | 21                    | 1 3 2         | 176                  | 114          | 13          | 1.2   | .1    | .1    |
| i       .4       2.0       4.3       7.3       2.2       1 0.4       1 7.3       1 0.4       8.0       1.3       .1       .1         i       .4       1.8       4.3       6.6       2.6       1.6       4       9.8       7.0       4.9       3.1       .1       .1         ii       .5       2.0       4.6       6.1       2.8       1 0.4       1.7.9       1 0.0       5.0       4.0       .1       .1         iii       .5       2.0       4.6       6.1       2.8       1 0.4       1.7.9       1 0.0       5.0       4.0       .2.4       .1       .1         iii       .5       2.0       4.6       6.1       7.7       2.1.2       7.8       3.6.5       7.7       2.30       .7       0       .1 <t< td=""><td>7</td><td>.4</td><td>1.8</td><td>4.1</td><td>6.4</td><td>21</td><td>114</td><td>176</td><td>108</td><td>10</td><td>1.2</td><td>.1</td><td>.1</td></t<>  | 7      | .4       | 1.8       | 4.1   | 6.4           | 21                    | 114           | 176                  | 108          | 10          | 1.2   | .1    | .1    |
| *       .4       1.8       4.1       6.4       2.6       1.24       1.7.3       1.0.0       6.0       1.5       .1       .1         11       .5       2.0       4.6       6.1       2.8       1.0.4       1.7.9       1.0.0       6.0       1.5       .1       .1         11       .5       2.0       4.6       6.1       2.8       1.0.4       1.7.9       1.0.0       5.0       4.0       .1       .1         13       .5       1.8       4.6       7.7       2.1.2       7.8       3.6.5       8.2       3.4       1.3       .1       .1         14       .6       1.8       4.6       8.6       1.7.9       6.6       3.5.0       7.2       3.0       .7       0       .1       .1         15       .6       1.8       4.8       9.0       1.1.0       6.4       2.4.6       5.1       2.1       .5       0       .1 <td></td> <td>.4</td> <td>2.0</td> <td>4.3</td> <td>7.3</td> <td>22</td> <td>104</td> <td>173</td> <td>104</td> <td>8.0</td> <td>1.3</td> <td>.1</td> <td>.1</td>  |        | .4       | 2.0       | 4.3   | 7.3           | 22                    | 104           | 173                  | 104          | 8.0         | 1.3   | .1    | .1    |
| 10       1       1.5       2.0       4.6       6.1       2.8       1.0.4       1.7.3       1.0.0       6.0       1.5       .1       .   | 9      | .4       | 1.8       | 4.3   | 6.4           | 1 8                   | 132           | 164                  | 98           | 7.0         | 4.9   | .1    | .1    |
| 11       .5       2.0       4.6       6.1       2.8       1.0       4       1.7       9       0.0       5.0       4.0       .1  | 10     | .4       | 1.8       | 4.3   | 6.4           | 26                    | 124           | 173                  | 100          | 6.0         | 15    | .1    | .1    |
| 11       1.5       2.0       4.6       5.9       2.1       7.8       3.6       5.5       7.2       3.4       1.1       1.1         14       .5       1.8       4.6       8.6       1.7.9       6.6       3.50       7.2       3.4       1.3       1.1       1.1         14       .5       1.8       4.6       8.6       1.7.9       6.6       3.50       7.2       3.0       7.7       0       1.1         14       .5       1.8       4.6       8.6       1.7.9       6.6       3.50       7.2       3.6       .7       0       .1         14       .6       1.8       4.8       1.8       7.2       6.2       2.1       2.5       0       .1         17       2.6       4.8       1.8       7.2       6.2       2.1       2.0       .5       0       .1         18       .7       2.6       4.8       5.0       5.3       1.1.0       2.0       .5       0       .1         18       .7       2.6       4.8       5.0       5.3       1.3.0       2.1.2       3.7       2.8       .4       .1.2       .1       .1       .1  | 11     | .5       | 2.0       | 4.6   | 6.1           | 28                    | 104           | 179                  | 100          | 5.0         | 40    | .1    | .1    |
| 11  | 12     | .5       | 2.0       | 4.6   | 5.9           | 4 3                   | 86            | 250                  | 92           | 4.0         | . 2.4 | .1    | .1    |
| 11         3.6       1 7 9       6       3 50       7 2       3.0        7       0          13         1.8       4.8       9.9       1 10       6       4       2 7 4       6 2       2.5        0          14          1.0       2       6.4       2 7 4       6 2       2.5        0          14           1.0       2       6.4       2 4.6       4.1       2.0          1.1         15           0       2.1       2.1       2.1        0        1.1         16         0       5.5       1.1       0.2       1.2       2.1       2.1       2.1       2.1       1.1         18           1.0       8       2.1       3.1       2.0        3.1       1.1       2.1       1.1         14 </td <td>13</td> <td>.2</td> <td>1.8</td> <td>4.6</td> <td>7.7</td> <td>212</td> <td>78</td> <td>365</td> <td>8 2</td> <td>3.4</td> <td>1.3</td> <td>.1</td> <td>.1</td>   | 13     | .2       | 1.8       | 4.6   | 7.7           | 212                   | 78            | 365                  | 8 2          | 3.4         | 1.3   | .1    | .1    |
| 18  .   | 14     |          | 1.8       | 4.0   | 5.6           | 1/9                   | 66            | 350                  | 7 2          | 3.0         | .7    | 0     | .1    |
| 17       .6       2.6       4.8       1 9       7 2       6 2       6 2       2 1 2       3 1       2.1       .3       0       .1         18       .7       2.6       4.8       4 3       6 2       6 2       1 9 7       4 1       2.0       .5       0       .1         19       .7       2.6       4.8       5 0       5 3       1 10       2 1 2       3 7       2.4       .4       .1       .1         19       .7       2.6       4.8       5 0       5 3       1 10       2 1 2       3 7       2.4       .4       .1       .1         11       .7       2.6       4.8       5 0       5 3       1 0 8       2 1 2       3 7       2.4       .4       .1       .1         11       .7       2.6       .6.1       2.5       .6.4       8 8       2 2 2       3 6       3.4       .2       .1       .1       .1       .1         12       .8       3.4       5.6       2.3       5.5       1 5 8       3 9.5       2.4       2.6       2.2       .1         13       .9       3.4       6.1       2.6       5.7       1 3.2  | -15    | .0       | 1.0       | 4.0   | 9.9           | 1 2 2                 | 64            | 274                  | 62           | 2.5         | .6    | .)    | .1    |
| 11       .7       2.6       4.8       4.3       6.2       6.2       1.9       7       4.4       3       1.1         13       .7       2.6       4.8       5.0       5.3       1.30       2.12       3.7       2.4       4.4       1.1       1.1         14       .7       2.6       4.8       5.0       5.3       1.30       2.12       3.7       2.4       4.4       1.1       1.1         14       .7       2.6       4.8       5.0       5.3       1.30       2.12       3.7       2.4       4.4       1.1       1.1         14       .7       2.6       5.6       4.4       5.9       1.2.6       2.1.8       3.7       2.4       4.4       .2       1.1         14       .7       2.6       5.6       1.4       5.9       1.2.6       2.1.5       3.6       3.4       .2.2       1.1         13       .8       2.8       6.1       2.5       6.4       8.8       2.2.2       3.2       3.2       1.1         14       .8       2.6       6.2       2.6       2.2       2.4       2.6       2.2       2.1       1.1         15 </td <td>17</td> <td>.0</td> <td>20</td> <td>4.0</td> <td>1 2</td> <td>7 2</td> <td>6 4</td> <td>240</td> <td>21</td> <td>2.1</td> <td>.2</td> <td>0</td> <td>-!</td>  | 17     | .0       | 20        | 4.0   | 1 2           | 7 2                   | 6 4           | 240                  | 21           | 2.1         | .2    | 0     | -!    |
| 19       .7       2.6       4.8       5.0       5.1       1.30       2.1 2       3.7       2.4       4.4       1.1       1.1         10       .7       2.6       4.8       4.1       92       1.2.6       2.1.8       3.7       2.8       .4       2.1       1.1         11       .7       2.6       4.8       4.1       92       1.2.6       2.1.8       3.7       2.8       .4       2.1       1.1         11       .7       2.6       4.8       4.1       92       1.2.6       2.1.8       3.7       2.8       .4       2.1       1.1         121       .7       2.6       4.8       5.9       2.1       5.8       2.2       3.6       3.4       4.4       2.2       1.1         121       .8       3.0       5.9       2.1       6.0       9.0       2.1.8       2.8       3.2       .3       2.2       .1         123       .8       3.4       5.6       2.3       5.5       1.5.8       3.9       2.4       2.6       2.2       2.1       1.1         124       .8       2.1       1.4       8       2.6       2.2       2.4       2.6<   | 18     | .7       | 26        | 4.8   | 4 1           | 62                    | 67            | 107                  | 4 2          | 2.0         | .2    | 5     |       |
| 10       17       2.6       4.2       4.1       9.2       1.2.6       2.1.8       3.7       2.8       .4       2.1       1         11       .7       2.6       5.6       3.4       5.9       1.0.8       2.1.5       3.6       3.4       .4       .2       .1         12       .8       3.0       5.9       2.3       6.0       9.0       2.1.8       2.2.3       2.3.6       .3.3       .2       .1         13       .8       3.4       5.9       2.3       6.0       9.0       2.1.8       2.8       3.2       .3.3       .2       .1         14       .8       3.4       5.9       2.3       6.0       9.0       2.1.8       2.8       3.2       .3       .2       .1         15       .8       3.4       5.9       1.0.8       5.5       1.5.8       3.9.5       2.4       2.6       2.2       2.1         16       .9       3.4       .6.1       1.0.6       5.7       1.3.2       2.4 0       2.1       2.6       2.2       .1         18       1.2       3.4       6.4       6.4       1.3.4       1.2.8       2.0.0       1.9       2.4   | 19     | .7       | 26        | 4.8   | 50            | 5 1                   | 110           | 212                  | 4 1          | 2.0         |       | 0     | • 1   |
| 1       .7       2.6       5.6       1       .7       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       1       0       1       1       0       1       1       1       1       1       0       1       1       0       1       1       0       1       1       1       0       1       1       1       1       0       1 </td <td>20</td> <td>.7</td> <td>2.6</td> <td>4.8</td> <td>4 1</td> <td>92</td> <td>126</td> <td>218</td> <td>37</td> <td>2.4</td> <td></td> <td>.1</td> <td></td>  | 20     | .7       | 2.6       | 4.8   | 4 1           | 92                    | 126           | 218                  | 37           | 2.4         |       | .1    |       |
| 11       .8       2.8       6.1       2.5       6.4       3.8       2.2.2       3.2       3.6       .3       .2       .1         11       .8       3.0       5.9       2.3       6.0       9.0       2.1.8       2.8       3.2       .3       .2       .1         12       .8       3.4       5.6       2.3       5.3       9.4       2.2.6       2.6       2.8       .2       .2       .1         13       .8       3.4       5.9       1.0.8       5.5       1.5.8       3.9.5       2.4       2.6       .2       .2       .1         14       .8       3.4       6.1       2.1.5       5.9       1.4.8       2.6.6       2.2       2.6       .2       .2       .1         14       1.2       3.4       6.1       1.0.6       5.7       1.3.2       2.4.0       2.1       2.4.4       .2       .2       .1         18       1.2       3.4       5.4       5.4       5.3       1.5       1.7.6       1.9       2.2       .1       .2       .1         10       1.4       3.6       6.4       2.6       3.4.0       2.1       2.2       .1 <td>21</td> <td>.7</td> <td>2.6</td> <td>5.6</td> <td>14</td> <td>591</td> <td>128</td> <td>215</td> <td>16</td> <td>2.0</td> <td></td> <td></td> <td></td>  | 21     | .7       | 2.6       | 5.6   | 14            | 591                   | 128           | 215                  | 16           | 2.0         |       |       |       |
| 11       .8       3.0       5.9       2.3       6.0       9.0       2.1 8       2.8       3.0       .3       .2       .1         14       .8       3.4       5.6       2.3       5.3       9.4       2.2 6       2.6       2.6       2.8       .2       2.2       .1         15       .8       3.4       5.6       2.3       5.5       1.5       8       3.9.5       2.4       2.6       2.2       2.4       2.6       2.2       2.2       .1         10       3.4       6.1       2.1.5       5.9       1.4       8       2.6.6       2.2       2.4       2.6       2.2       2.1       1.1         11       1.0       3.4       6.1       1.0.6       5.7       1.3.2       2.4       2.2       2.2       .1         12       1.4       3.4       5.4       5.3       1.5.8       3.9.5       1.7.6       1.9       2.2.4       2.2       2.1       1.1         12       1.4       3.4       5.4       2.6       3.4.0       2.0       1.1       2.2       1.1         13       1.4       3.4       2.6       3.4.0       2.1       2.6.6   | 22     | .8       | 2.8       | 6.1   | 25            | 64                    | 8.8           | 222                  | 12           | 1.4         |       | .4    |       |
| 14       .8       3.4       5.6       2.3       5.3       9.4       2.2.6       2.6       2.6       2.4       2.2       2.2       1         15       .8       3.4       5.9       1.0.8       5.5       1.5.8       3.9.5       2.4       2.6       2.2       2.4       2.6       2.2       2.2       1         16       .9       3.4       6.1       2.1.5       5.9       1.4.8       2.6.6       2.2       2.6       2.2       2.4       2.2       2.1       1         17       1.0       3.4       6.1       1.0.6       5.7       1.3.2       2.4.0       2.1       2.4       2.2       2.1       1         18       1.2       3.4       6.4       6.4       1.3.4       1.2.8       2.0.0       1.9       2.4       .2       2.1       1         11       1.3       5.4       2.6       3.4.0       2.0       2.0       2.4       .1       .2       .1         12       1.3       5.4       2.6       3.4.0       2.0       2.0       .1       .2       .1         13       1.4       3.6       6.7.9       3.4.0       2.1       6.9.0.1   | 23     | .8       | 3.0       | 5.9   | 23            | 6 0                   | 90            | 218                  | 28           | 12          | 3     | .2    |       |
| 15  | 24     | .8       | 3.4       | 5.6   | 23            | 5 3 1                 | 94            | 226                  | 26           | 28          | .2    | 2     |       |
| 26       .9       3.4       6.1       215       59       148       266       22       2.6       .2       .2       .1         27       1.0       3.4       6.1       106       57       132       240       21       2.4       .2       .2       .1         28       1.2       3.4       6.4       64       134       128       200       19       2.4       .2       .2       .1         28       1.4       3.4       5.4       53       134       152       176       19       2.2       .1       .2       .1         30       1.4       3.6        12       2.66       17.2       20       .1       .2       .1         31       1.3       5.4       2.6       340       200       .1       .2       .1       .2       .1         31       1.3       5.4       2.6       340       200       .1       .2       .1       .2       .1         31       1.3       4.93       31.5       62.9       148       227       69.5       6.73       2.67       0.12       0.12       0.12       0.2       0.2       0.1   | 25     | .8       | 3.4       | 5.9   | 108           | 55                    | 158           | 195                  | 24           | 2.6         | 2     | 2     | ï     |
| 27       1.0       3.4       6.1       1 0 6       5 7       1 3 2       2 4 0       2 1       2.4       2       .2       .1         24       1.2       3.4       6.4       6.4       1 3 4       1 2 8       2 0 0       1 9       2.4       .2       .2       .1         25       1.4       3.4       5.4       5.3       1 5 2       1 7 6       1 9       2.2       .1       .2       .1         20       1.4       3.6       .1       1 2       2 6       1 7 3       2 0       .1       .2       .1         31       1.3       5.4       2.6       3 4 0       20       .1       .2       .1         31       1.3       5.4       2.6       3 4 0       20       .1       .2       .1         31       1.3       5.4       2.6       3 4 0       20       .1       .2       .1         31       1.3       5.4       2.6       3 4 0       2.1 5 6       2 0 1.8       8 2.7       3.8       3.5         Mean       0.65       2.31       4.93       31.5       62.9       148       227       69.5       6.73       2.67       0.12   | 26     | .9       | 3.4       | 6.1   | 215           | 59                    | 148           | 266                  | 22           | 2.6         | .2    | 2     |       |
| 11       1.2       3.4       6.4       6.4       1 3 4       1 2 8       2 0 0       1 9       2.4       .2       .2       .1         12       1.4       3.4       5.4       5.3       1 5 2       1 7 6       1 9       2.4       .2       .2       .1         10       1.4       3.6       .1       1 2       8       1 7 6       1 9       2.2       .1       .2       .1         11       1.3       5.4       2.6       3 4 0       20       .1       .2       .1         11       1.3       5.4       2.6       3 4 0       20       .1       .2       .1         11       1.3       5.4       2.6       3 4 0       20       .1       .2       .1         12       1.3       5.4       2.6       9 7 5.9       1.7 6 1       4.5 7 3       6.9 0 1       2.1 5 6       2 0 1.8       8 2.7       3.8       3.5         Mean       0.65       2.31       4.93       31.5       62.9       148       227       69.5       6.73       2.67       0.12       0.12       0.12         Min       0.2       1.4       3.8       5.4       18   | 27     | 1.0      | 3.4       | 6.1   | 106           | 57                    | 1 3 2         | 240                  | 21           | 2.4         | 2     | 2     |       |
| 25       1.4       3.4       5.4       5.3       152       176       19       2.2       1       .2       1         30       1.4       3.6       .1       12       266       173       20       2.4       .1       .2       .1         31       1.3       5.4       26       340       20       2.4       .1       .2       .1         7561       2.0.2       6.9.3       152.8       975.9       1.761       4.573       6.901       2.156       201.8       82.7       3.8       3.5         Mean       0.65       2.31       4.93       31.5       62.9       148       227       69.5       6.73       2.67       0.12       0.12       0.12         Mean       1.4       3.6       6.4       215       212       395       395       164       22       40       50.2       0.2       0.2       0.2       0.2       0.2       0.2       0.1       0       0.1         Ac-rtt       40       137       303       1.940       3.490       8.670       13.490       4.280       400       164       7.5       6.9         Cat rr       1974 :       Mean   | 2.8    | 1.2      | 3.4       | 6.4   | 64            | 134                   | 128           | 200                  | 19           | 2.4         | .2    | 2     |       |
| 30       1.4       36        12       266       173       20       2.4       .1       2       .1       .1       2       .1       .1       .1       .2       .1       .1       .1       .1       .1       .1       .1       .1       .1       .1       .1<  | 25     | 1.4      | 3.4       | 5.4   | 53            |                       | 152           | 176                  | 19           | 2.2         | .1    | 2     | i.i   |
| 31       1.3       5.4       2.6       3.4.0       2.0       .1       .2         Total       2.3.2       6.9.3       1.5.2.8       9.7.5.9       1.7.6.1       4.5.7.3       6.9.0.1       2.1.5.6       2.0.1.8       8.2.7       3.8       3.5         Mean       0.65       2.31       4.93       31.5       62.9       148       227       69.5       6.7.3       2.67       0.12       0.12         Max       1.4       3.6       6.4       215       212       395       395       164       22       40       50.2       0.2       0.2       0.2       0.12       0.12       0.2       0.2       0.4       1.4       3.8       5.4       1.8       62       164       19       2.2       0.1       0       0.1   | 30     | 1.4      | 16        |       | 12            |                       | 266           | 173                  | 20           | 2.4         | .1    | 2     |       |
| Total         2 3.2         6 9.3         1 5 2.8         9 7 5.9         1.7 6 1         4.5 7 3         6.8 0 1         2.1 5 6         2 0 1.8         8 2.7         3.8         3.5           Mean         0.65         2.31         4.93         31.5         62.9         148         227         69.5         6.73         2.67         0.12         0.12           Max         1.4         3.6         6.4         215         212         395         164         22         40         50.2         0.2         0.2         0.2         0.2         0.12         0.2         0.2         0.1         0 <td>31 .</td> <td>1.3</td> <td></td> <td>5.4</td> <td>26</td> <td></td> <td>340</td> <td>1 Contraction of the</td> <td>20</td> <td></td> <td>.1 j</td> <td>.21</td> <td>·</td>                 | 31 .   | 1.3      |           | 5.4   | 26            |                       | 340           | 1 Contraction of the | 20           |             | .1 j  | .21   | ·     |
| Mate         0.65         2.31         4.93         31.5         62.9         148         227         69.5         6.73         2.67         0.12         0.12         0.12           Max         1.4         3.6         6.4         215         212         395         164         22         40         50.2         0.2         0.2         0.12         0.12         0.12         0.2         0.4         1.4         3.8         5.4         18         62         164         19         2.2         0.1         0         0.12         0.2         0.4         0.1 <td< td=""><td></td><td>222</td><td>601</td><td>1528</td><td>0750</td><td>1161</td><td>1 5 7 3</td><td></td><td></td><td></td><td></td><td></td><td></td></td<> |        | 222      | 601       | 1528  | 0750          | 1161                  | 1 5 7 3       |                      |              |             |       |       |       |
| Max         1.4         3.6         6.4         215         212         395         395         164         22         40         0.12   | Man    | 0.65     | 2 21      | 1 03  | 21 5          | 62.0                  | ) / )         | 0.901                | 2.156        | 201.8       | 0 2.1 | 3.8   | 3.5   |
| Min         0.2         1.4         3.8         5.4         18         62         164         19         2.2         40         0.2         0.2         0.1           Ac-ft         40         137         303         1.940         3.490         8.670         13.490         4.280         400         164         2.2         0.1         0         0.1   | Max    | 0.05     | 2.51      | 6.4   | 31.5          | 212                   | 148           | 22/                  | 69.5         | 6.73        | 2.67  | 0.12  | 0.12  |
| 0.2         1.3         3.3         3.4         18         62         164         19         2.2         0.1         0         0.1           Ac-rt         40         137         303         1.940         3.490         8.670         13.490         4.280         400         164         7.5         6.9           Cal yr         1974         Mean         84.5         Max         2.620         Min         0.1         Ac-rt         61,200           We yr         1975         Mean         46.0         Max         395         Min         0         Ac-rt         33,320         FYHIRIT   | MIN    | 1.4      | 3.0       | 2.0   | 215           | 10                    | 332           | 395                  | 164          | 22          | 40    | 0.2   | 0.2   |
| Call yr         1974 :         Mean         84.5         Max         2,620         Min         0.1         Ac-ft         61,200           We yr         1975 :         Mean         46.0         Max         395         Min         0         Ac-ft         33,320         FYLIRIT   | 4      | 0.2      | 127       | 3.0   | 1 040         | 2 400                 | 0 670         | 104                  | 19           | 2.2         | 0.1   | 0     | 0.1   |
| Cal pr         1974 :         Mean         84.5         Max         2,620         Min         0.1         Ac-ft         61,200           Wir pr         1975 :         Mean         46.0         Max         395         Min         0         Ac-ft         53,320   | Acent  | 40]      | 13/ 1     | 303 1 | 1,940         | 3,490                 | 8,070         | 13,490               | 4,280        | 400         | 164   | 7.5   | 6.9   |
| Wir yr 1975 : Mean 46.0 Max 395 Min O Ac-fi 33,320  | Cal Tr | 1974 : : | Mean 84.5 | Max   | 2,620         | Min                   | 0.1           | Ac-11                | 61,200       |             |       |       |       |
| FYHIRIT   | Wir Ir | 1975 : 2 | Mean 46.0 | Max   | 395           | Min                   | 0             | Ac-ft                | 33,320       |             |       |       |       |
|   |        |          |           |       |               | and the second second |               |                      |              |             |       | FYHIE | IT    |

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#### WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION.--Lat 45°20'11", long 120°03'40", in NWxSW% Sec.3, T.3 S., R.22 E., Gilliam County, on left bank 200 ft (50 m) downstream from county bridge, and 9 mi (14 km) northeast of condon.

DRAINAGE AREA. -- 350 mi<sup>2</sup> (906 km<sup>2</sup>).

PERIOD OF RECORD. -- April 1965 to current year.

GAGE.--Water-stage recorder.

AVERAGE DISCHARGE.--11 years (1965-76), 44.2 ft<sup>3</sup>/s (1.252 m<sup>3</sup>/s), 32,020 acre-ft/yr (39.5 hm<sup>3</sup>/yr).

EXTREMES.--Current year: Maximum discharge, 302 ft<sup>3</sup>/s (8.55 m<sup>3</sup>/s) Apr. 9, gage height, 2.83 ft (0.863 m); no flow at times.

Period of record: Maximum recorded discharge, 12,500 ft $^3$ /s (354 m $^3$ /s) June 8, 1972, gage height, 8.87 ft (2.704 m); no flow at times.

REMARKS .-- Records good.

REVISIONS (WATER YEARS). -- 1972. See 1973 publication.

|        |        |           |                 | Discharge, in | cubic feet pe | r second for | the year end              | ing Septembe | r 30, 1976                |       |         |       |
|--------|--------|-----------|-----------------|---------------|---------------|--------------|---------------------------|--------------|---------------------------|-------|---------|-------|
| Day    | Oct.   | Nov.      | Dec.            | Jan.          | Feb.          | Mar.         | April                     | May          | June                      | July  | Aug.    | Sept. |
| 1      | 0.1    | 2.2       | . 5.9           | 23            | )7            | 36           | 96                        | 51           | 9.5                       | 0.8   | 0       | 4.1   |
| 2 1    | .1     | 2.2       | 6.1             | 18            | 35            | 37           | 90                        | 47           | 9.9                       | .7    | 0       | 3.5   |
| 3 1    |        | 2.4       | 7.7             | 33            | 34            | 34           | 104                       | 44           | 9.5                       | .7    | .1      | 3.6   |
| 6 ]    | .1     | 2.4       | 9.0             | 341           | 17            | 16           | 114                       | 41           | 8.6                       | .6    | .1      | 3.4   |
| 5      | 2      | 2.6       | 9.5             | 371           | 14            | 27           | 145                       | 37           | 8.2                       | .5    | .1      | 3.0   |
| 6 1    | 2      | 3.0       | 9.0             | 33:           | 17            | 30           | 209                       | 32           | 7.3                       | .5    | 2       | 2.8   |
| 7      | .3     | 3.4       | 9.5             | 33            | 20            | 32           | 185                       | 29           | 6.8                       | .5    | 10      | 2.6   |
| 8      | .3     | 3.4       | 9.9             | 106           | 2 5           | 28           | 176                       | 25           | 5.9                       | .4    | 14!     | 2.6   |
| 9      | .)     | 3.4       | 11              | 116           | 25            | 28           | 266                       | 23           | 5.9                       | .4    | 6.8     | 2.2   |
| 10     |        | 4.1       | 10 !            | 82            | 22            | 34           | 203                       | 20           | 5.9                       | .4    | 5.6     | 1.2   |
| 11     | .4     | 4.1       | 9.5 :           | 66            | 20            | 38           | 179                       | 18           | 5.6                       | .)    | 4.6     | .6    |
| 12     | .4     | 4.1       | 9.0             | 37            | 21            | 34           | 173                       | 18           | 5.4                       | .)    | 4.1     | .4    |
| 13     | .4     | 4.1       | 9.0             | 4 4           | 23            | 37           | 176                       | 14           | 4.6                       | 3     | 3.8     | 3     |
| 14     | .4     | 4.1       | 7.7             | 4 5           | 26            | 4 1          | 1 5 2                     | 11           | 4.3                       | 2     | 4.3     | 1.0   |
| 15     | .5     | 4.1       | 7.7             | 74:           | 101           | 4 1          | 138                       | 101          | 4.1                       | 2     | 5.91    | 2.8   |
| 16     | 5      | 4.3       | 8.6             | 167           | 29            | 47           | 130                       | 9.5          | 3.8                       | .2    | 7.3     | 3.6   |
| 17     | .5     | 4.3       | 8.6             | 179           | 4 5           | 94           | 116                       | 9.0          | 3.4                       | 2     | 12      | 3.4   |
| 18 1   | .5     | 4.3       | 8.2             | 152           | 50            | 173          | 114                       | 8.6          | 3.2                       | 2     | 11      | 3.2   |
| 19     | .5     | 4.3       | 8.2 ;           | 112           | 50;           | 202          | 102                       | 8.6          | 3.0                       | .1    | 9.5     | 3.0   |
| 20     | .5     | 4.3       | 7.7             | 8.6           | 40'           | 126          | 108                       | 9.0          | 2.4                       | .1    | 8.6     | 2.8   |
| 21     | .6     | 4.3.      | 7.3             | 68;           | ))            | 110          | 110                       | 9.5          | 2.2                       | .1    | 7.7     | 2.8   |
| 22     | .7     | 4.3       | 7.3             | 59            | 321           | 110          | 94                        | 8.6          | 2.0                       | .1    | 6.8     | 32    |
| 23     | .8     | 4.6       | 7.7.            | 59            | 29.           | 108          | 98                        | 8.2          | 1.7                       | .1    | 6.4     | 12    |
| 24     | .8     | 4.6       | 9.9,            | 51            | 2 8           | 114          | 70                        | 7.3          | 1.7                       | .1    | 8.1     | 3.4   |
| 25     | 1.0    | 4.6       | 11              | 4.3           | 32            | 150          | 84                        | 7.3          | 1.5                       | 0     | 8.2     | 3.4   |
| 26     | 1.6    | 5.1       | 13              | 37            | 41            | 114          | 76                        | 6.8          | 1.5                       | 0     | 7.7     | 3.2   |
| 27     | 2.4    | 6.4       | 45              | 37            | 55            | 102          | 70                        | 6.4          | 1.2                       | 0     | 6.8     | 32    |
| 28     | 2.6    | 6.4       | 45              | 36            | 66            | 98           | 66                        | 6.4          | 1.0                       | 0     | 6.1     | 32    |
| 29     | 2.4    | 6.1       | 40              | 4 4           | 5 5           | 84           | 64                        | 6.4          | .8                        | 0 1   | 5.6     | 3.0   |
| 30     | 22     | 5.9       | 59              | 4 5           |               | 54           | 59                        | 6.8          | .9                        | 0     | 5.1     | 2.8   |
| 31     | 2.0    |           | 50              | 40:           |               | 100          |                           | 7.7          |                           | C     | 4.6     |       |
| Total  | 217    | 1214      | 4 6 7.0         | 2018          | 951           | 2329         | 1767                      | 5461         | 1318                      | 8.0   | 1.8.1.1 |       |
| Mean   | 0.76   | 4.11      | 15.1            | 65.11         | 32.8          | 75 1         | 126                       | 17.6         | 4 30                      | 0.26  | 5 84    | 2 73  |
| Max    | 2.6    | 6.4       | 59              | 179           | 66            | 202          | 265                       | 511          | 9.9                       | -0.01 | -14     | 6.13  |
| Min    | 0.1    | 22        | 5.9             | 18            | 14:           | 27           | 59                        | 6 41         | 0.8                       | 0.0   | 0       | 0.7   |
| Acits  | 47     | 245       | 926             | 4 000         | 1 890         | 4.620        | 7.470                     | 1 080        | 261                       | 16    | 750     | 162   |
|        |        | Lannonel  | and a second de |               |               | the second   | in a second second second | 1,000]       |                           | 101   | 333     | 102   |
| Cal yr | 1975 : | Mean 47.0 | Max             | 395           | Min           | 0            | Ac-ft                     | 34,060       |                           |       |         |       |
| Wir yr | 1976 : | Mean 29.0 | Max             | 256           | Min           | 0            | Ac-ft                     | 21,080       |                           | -     | 1017    | 2     |
|        |        |           |                 |               |               |              | -                         |              | Concernance on the second | -XH   | IRIT    | 2     |
|        |        |           |                 |               |               |              |                           |              |                           | LAII  | 1011 -  |       |
|        |        |           |                 |               |               |              |                           |              |                           | PAC   | F 11    | OF 17 |
|        |        |           |                 |               |               |              |                           |              |                           | IAG   |         | 01    |

#### WATER RESOURCES DEPARTMENT

#### JOHN DAY RIVER BASIN

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, OREG.

LOCATION.--Lat 45°20'11", long 120°03'40", in NWLSWL sec.3, T.3 S., R.22 E., Gilliam County, on left bank

200 ft (60 m) downstream from county bridge and 9 mi (14 km) northeast of Condon.

DRAINAGE AREA .-- 350 m12 (906 km2).

PERIOD OF RECORD. -- April 1965 to current year.

GAGE.--Water-stage recorder.

AVERAGE DISCHARGE.--12 years (1965-77), 41.1 ft<sup>3</sup>/s (1.164 m<sup>3</sup>/s), 29,780 acre-ft/yr (36.7 hm<sup>3</sup>/yr).

EXTREMES.--Current year: Maximum discharge, 112 ft<sup>3</sup>/s (3.17 m<sup>3</sup>/s) April 6, gage height, 2.25 ft (0.686 m); no flow July 16 to Sept. 30.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 8, 1972, gage height, 8.87 ft

(2.704 m); no flow at times.

REMARKS. -- Records good.

REVISIONS .-- 1972, see 1973 publication.

| Day  | Oct.    | Nov.     | Dec.    | Jan.    | Feb.  | Mar.  | April | May    | June  | July | Aug. | Sept. |
|------|---------|----------|---------|---------|-------|-------|-------|--------|-------|------|------|-------|
| 1    | 2.8     | 2.0      | 3.6     | 4.6     | 5.4   | 8.2   | 18    | 4.6    | 6.1   | .2   |      |       |
| 2 ;  | 2.8     | 3.01     | 4.1     | 4.5     | 5.1   | 8.6   | 20    | 4.8    | 6.1   | .2   | i    |       |
| 3 -  | 2.6     | 3.0!     | 4.3     | 4.5     | 5.1   | 9.5   | 20    | 5.4    | 5.6   | .2   | 1    |       |
|      | 2.6     | 3.0      | 4.6     | 4.3     | 5.1   | 9.9   | 37    | 5.4    | 5.6   | .2   |      |       |
| 5    | 2.6     | 3.01     | 4.6     | 3.0     | 5.0   | 9.0   | 64    | 5.6    | 5.1   | .2   |      |       |
| 6 1  | 2.6     | 3.0      | 4.6     | 2.8     | 4.9   | 8.6   | 88    | 5.9    | 4.6   | .2   |      |       |
| 1 1  | 2.6     | 3.0;     | 4.6     | 2.7     | 4.8   | 9.5   | 78    | 7.3    | 3.8   | 2    | 1    |       |
|      | 2.6     | 3.2!     | 4.6     | 2.6     | 4.8   | 11    | 64    | 7.7    | 3.4   | .2   |      |       |
| 3 !  | 2.6     | 3.0      | 4.6     | 2.6     | 4.8   | 16    | 44    | 7.7    | 3.0   | .2   | 1    |       |
| 10 1 | 2.6     | 1        | 4.6     | 2.8     | 4.9   | 18    | 35    | 9.9    | 2.8   | .2   |      |       |
| 1.   | 2.6     | 1.6;     | 4.8     | 1.0     | 5.1   | 17    | 28    | 35     | 2.4   | .1   |      | -     |
| 2    | 2.4     | 3.6      | 4.8     | 3.3     | , 5.4 | 16    | 24    | 35     | 2.4   | .1   |      |       |
| 1    | 2.21    | 3.6      | 4.6     | 3.7     | 5.9   | 16    | 21    | 34     | 22    | .1   | ;    |       |
|      | 2.2     | 1.6      | 4.61    | 4.0!    | 6.4   | 13    | 20    | 26     | 22    | .1   | i    |       |
| 51   | 2.2     | 3.6      | 4.8     | 4.5     | 6.8   | 13    | 17    | 27     | 1.7   | .1   |      |       |
| 61   | 22      | 4.31     | 4.81    | 5.2     | 6.4   | 12    | 16    | 21     | 1.5   | 0    |      |       |
| 1    | 2.2     | 4.3      | 4.8     | 5.9     | 6.1   | 12    | 14    | 19     | 1.3   | 0    | 1    |       |
|      | 2.4     | 4.3      | 4.8     | 5.9     | 6.1   | 12    | 13    | 18     | 1.3   | i l  |      |       |
| ,    | 2.6     | 4.6      | 4.8     | 5.9     | 6.1   | 12    | 12    | 16     | .8    | 0    | 1    |       |
|      | 2.6     | 4.6      | 1.8     | 5.6     | 6.1   | 12    | 11    | 15     | .8    | 0    |      |       |
| 1 :  | 2.6     | 4.81     | 4.8     | 5.4     | 6.4   | 12    | 9.9   | 13     | .8    | 0    |      |       |
|      | 2.4     | 4.8      | 4.6     | 5.4     | 6.4   | 11    | 9.5   | 11     | .7    | 0    |      |       |
| 1    | 2.4     | 4.8      | 5.1     | 5.4     | 6.8   | 12    | 8.2   | 10     | .6    | 0    |      |       |
|      | 2.4     | 4.6      | 4.6     | 5.4     | 6.4   | 14    | 6.8   | 11     | .5    | 0    | 1    |       |
|      | 2.6     | 4.7      | 5.1     | 5.4     | 6.4   | 16    | 6.1   | 11     | .4    | 2    |      |       |
| 5    | 2.6     | 4.8      | 4.8     | 4.6     | 6.4   | 16    | 5.9   | 11     | .)    | 3    |      |       |
| 1    | 2.6     | 4.1      | 4.8     | 4.8     | 6.4   | 17    | 5.6   | 9.5    | .)    | 0    |      |       |
|      | 2.6     | 4.6      | 4.6     | 5.1     | 7.3   | 18    | 5.1   | 9.5    | .3    | 2    |      |       |
|      | 2.8     | 3.61     | 4.8     | 4.8     |       | 18    | 4.8   | 9.0    | .2    | 0    |      |       |
|      | 2.8     | 3.6      | 4.8     | 4.6     |       | 18    | 4.6   | 8.2    | .2    | 0    |      |       |
| -    | 2.8     | 1        | 4.8     | 4.8     |       | 17    |       | 7.3    |       | 0    |      |       |
|      | 7 8.6   | 1 1 6.31 | 1 4 4.0 | 1 3 7.5 | 162.8 | 412.3 | 710.5 | 4 20.8 | 6 7.0 | 2.5  | 0    |       |
|      | 2 54    | 3.88 .   | 4.65    | 4.44    | 5.81  | 13.3  | 23.7  | 13.6   | 2.23  | 0.08 | 0 1  |       |
|      | 28      | 4.8 .    | 5.1     | 5 9     | 2 3   | 18    | 88    | 35     | -511  | -027 | -01  |       |
| 1    | 2.2     | 3.0      | 3.6     | 2.6     | 1 0   | 8 2   | 4.6   | 4.6    | 0.2   | 0.2  | 0    |       |
| 11   | 156     | 231 1    | 286     | 273     | 323   | 818   | 1 410 | 835    | 1771  | 501  | 0 :  |       |
|      | 130     |          |         |         | 323   | 010]  | 1,410 | 035    | 1331  | 3.01 |      |       |
| r 19 | 76 : Me | 28.3     | Max     | 266     | Min   | 0     | Ac-ft | 20,530 |       |      |      |       |

scharge, in cubic feet per second for the year ending September 30, 1977

EXHIBIT 3 PAGE 12 OF

#### JOHN DAY RIVER BASIN

#### 14047400 ROCK CREEK ABOVE CAYUSE CANYON, NEAR CONDON, 1753.

LTCATION.--Lat 45/20/11", long 120/03/40", in NWUSH's sec.3, T.3 S., R.22 E., Gilliam County, on left bank

200 ft (60 -' downstream from county bridge and 9 mi (14 km) nontheast of Concto.

2511WAGE AREA -- 352 =12 (906 km2).

FIRIOD OF RECORD.--April 1965 to current year.

3-35.--Water-stage recorder.

AVERAGE DISCHARGE.--13 years (1965-78), 41.2 ft3/s (1.167 m3/s), 29,850 acre-ft/yr (36.5 m3/yr).

EVIREMES.--Current year: Maximum discharge,478 ft<sup>3</sup>/s (13.5 m<sup>3</sup>/s) Feb. 7, gage heiptt. 3.18 ft (0.969 m); no flow Oct. 1-19.

Period of record: Maximum recorded discharge, 12,500 ft<sup>3</sup>/s (354 m<sup>3</sup>/s) June 3, 1972, gage height, 8.87 ft (2.704 m); no flow at times.

RENARKS.--Records good except for August which are fair.

REVISIONS.--1972, see 1973 publication.

| Day    | Oct.   | Nov.           | Dec.              | Jan.    | Feb.  | Mar.  | April           | May     | June  | July  | Aug. | Sept. |
|--------|--------|----------------|-------------------|---------|-------|-------|-----------------|---------|-------|-------|------|-------|
| 1      | 5      | 0.3            | 28                | 8.4     | 64    | 145   | 74              | 66      | 1.    | 4.3   | 0.7  | 1 1.4 |
| 2 1    | 0      | .3             | 23                | 9.9     | 66    | 124   | 96              | 55      | 7.7   | 4.6   | .2   | 1.3   |
| 3      | 0      | 3              | 29                | • 13    | 64    | 108   | 76              | 1 48    | 5.4   | 7.3   | .2   | 1 1.2 |
| 4      | 0      | .3             | 28                | 26      | 72    | 106   | 68              | 44      | 1 7.3 | . 10  | .2   | 1 1.2 |
| 5      | C      | .4             | 23                | 82      | 80    | 104   | 64              | 43      | 5.4   | 9.9   | .2   | 1 1.3 |
| 6      | 0      | 4              | 19                | 90      | 1 135 | 112   | 62              | 40      | 5.1   | 7.7   | .2   | 1.4   |
| 7      | 0      | .4             | 17                | 62      | 218   | 118   | 70              | 36      | 1 5.1 | 6.1   | .2   | - 1.5 |
| 8      | 0      | 1.5            | 1 16              | 59      | 365   | 152   | 66              | 29      | 4.0   | 8.0   | .2   | 1.6   |
| 9      | 0      | .5             | 14                | 114     | 240   | 298   | 53              | 27      | 4.3   | 13    | .2   | 1.6   |
| 10     | 0      | .5             | 13                | 170     | 194 . | 246   | 45              | 28      | 1 41  | 9.5   | 2    | 1.5   |
| 11 1   | 0      | .6             | 13                | 142     | 150   | 203   | 40              | 27      | 4 -   | 7.3   | 2    | 1.5   |
| 12     | 0      | .6             | 13                | 135     | 118   | 185   | 37              | 25      | 4.3   | 6.4   | 2    | 1.5   |
| 12     | õ      | .7             | 18                | 142     | 120   | 164   | 36              | 25      | 4 5   | 5.4   | 2    | 1.5   |
| 14     | Ő      | .7             | 130               | 188     | 106   | 142   | 35              | 24      | 51    | 4.6   | 2    | 1.6   |
| 15     | ñ      | 8              | 185               | 310     | 104   | 126   | 33              | 37      | 5.6   | 3.8   | 1 2  | 1 7   |
| 16     | 0      |                | 118               | 335     | 84    | 116   | 35              | 40      | 1 51  | 1 3.6 | 2    | 1 1 7 |
| 17     | ő      | 9              | 80                | 282     | 80    | 110   | 37              | 30      | 1 4.5 | 3.6   | .2   | 1.8   |
| 18     | 0      | 12             | 55                | 197     | 84    | 110   | 35              | 26      | 43    | 3.4   |      | 2.2   |
| 19     | 0 .    | 1.4            | 37                | 182     | 102   | 102   | 32              | 23      | 1 3.5 | 3.0   | .2   | 2 2   |
| 20     | .1     | 11             | 28                | 158     | 135   | 96    | 29              | 19      | 3.2   | 2.5   | .2   | 2.2   |
| 71     |        | 1.4            | 25                | 132     | 140   | 90    | 28              | 17      | 1 15  | 22    | 10   | 22    |
| 72     | 1      | 1.5            | 24                | 124     | 135   | 86    | 27              | 16      | 10    | 1 1 8 | 4.0  | 2.2   |
| 23 1   | 1      | 1.6            | 23                | 102     | 138   | 84    | 28              | 18      | 1.8   | 1 1 6 | 3.0  | 2.0   |
| 74     | 1      | 2.8            | 23                | 82      | 140   | 106   | 28              | 17      | 3.0   | 1 1 4 | 2.0  | 2.0   |
| 25     | 1      | 9.8            | 24                | 76      | 164   | 90    | 26              | 17      | 3.6   | 1 12  | 1.0  | 2.0   |
| 26     | 1 1    | 56             | 26                | 62      | 170   | 76    | 71              | 17      | 3.5   | 1 10  | 1.4  | 2.0   |
| 27     | 2      | 44             | 24                | 68      | 194   | 66    | 170             | 16      | 3.4   | 1.0   | 1.0  | 2.0   |
|        | 2      | 35             | 22                | 66      | 161   | 50    | 122             | 16      | 2.8   | 1 .   | 1    | 2.0   |
|        | 2      | 29             | 22                | 64      | 101   | 53    | 94              | 15      | 1 12  | 1 .3  |      | 2.0   |
| 20     | 2      | 32             | 21                | 70      |       | 50    | 76              | 13      | 1 7 2 |       |      | 2.0   |
| 30     |        | 36             | 1 10              | 68      |       | 50    |                 | 12      | 1.6   |       | 1.0  | - 2.0 |
|        |        |                |                   | 00      |       |       | Carlos Constant | 16      |       | .6    | 1.5  |       |
| Total  | 1.8    | 225.9          | 1,140             | 3,619.3 | 3,823 | 3,677 | 1,694           | 862     | 151.3 | 135.3 | 20.4 | 52.6  |
| Mean   | 0.06   | 7.53           | 36.8              | • 117   | 137   | 199   | 56.5            | 27.8    | 5.05  | 4.37  | 0.66 | 1.76  |
| Max    | 0.3    | 56             | 185               | 335     | 365   | 298   | 170             | 66      | 1 13  | 13    | 4.0  | 2.2   |
| Min    | 0      | 0.3            | 13                | 8.4     | 64    | 50    | 26              | 12      | 1 1.0 | 0.2   | 0.2  | 1.2   |
| Acatt  | 3.6    | 448            | 2,260             | 7,180   | 7,580 | 7,290 | 3,360           | 1.710   | 300   | 268   | 40.5 | 104   |
| men    |        |                |                   |         |       |       |                 |         |       |       |      |       |
| Cal yr | 1977 : | Mean<br>Mean 4 | 8.99 Ma<br>2.2 Ma | 18      | 5 MI  | n 0   | Ac-             | a 6,510 |       |       |      |       |

Discharge, in cubic feet per second for the year ending September 30, 1275

EXHIBIT <u>3</u> PAGE 13\_OF 13\_

# JOHN DAY RIVER BASIN

STATE OF OREGON WATER RESOURCES DEPARTMENT SALEM, OREGON

November 1986



### WILLIAM H. YOUNG, DIRECTOR

WATER RESOURCES COMMISSION

Members:

JOE B. RICHARDS, CHAIRMAN JACK A. HOFFBUHR, VICE-CHAIRMAN HADLEY C. AKINS WILLIAM R. BLOSSER WILLIAM D. CRAMER LORNA J. STICKEL



#### SECTION IX

#### LOWER SUBBASIN

#### A. LOCATION AND DESCRIPTION

The Lower Subbasin (see Figure 35) drains an area of about 2,030 square miles below Clarno and is located in Wheeler, Gilliam, Sherman, Morrow, and Wasco Counties. It is an area which is physiographically different from the upstream subbasins. The subbasin generally lacks the mountainous terrain and elevations which accumulate significant snowpack. Elevations range from about 200 feet at the mouth of the John Day River, to over 5,700 feet south of Heppner. The Lower Subbasin is a nearly level to rolling, loess covered plateau of Columbia River Basalt which is deeply dissected by the John Day River and its tributaries. Unlike the rest of the basin, it is a major dryland farming area and includes some large scale irrigation, using ground water.

The Lower Subbasin has a well developed transportation network. Interstate 84 and a rail line in the extreme north parallel the Columbia River. State routes 19, 206, and 218 connect subbasin communities such as Fossil, Condon, and Arlington. The Columbia River provides the Port of Arlington with a transportation route to the Pacific.



Small streams, such as Rock Creek, are important water sources in the dry Lower Subbasin.



#### 1. CLIMATE

The climate is semiarid. Precipitation is low and the subbasin exhibits small daily ranges in both summer and winter temperatures. The length and character of summer and winter extremes are influenced by the rain shadow effect of the Cascade Mountains, and the wind tunnel effect of the Columbia River Gorge.

Precipitation ranges from slightly more than 9 inches annually at Arlington and 13 inches at Condon, to about 40 inches in the mountains. Annual average temperatures are 54° F at Arlington and 48° F at Condon.

#### 2. LAND OWNERSHIP

Like the Middle Mainstem Subbasin, the predominance of private land ownership sets the Lower Subbasin apart from the other subbasins. Federal ownership (mostly BLM) accounts for only about 11 percent of the land area (see Figure 36). BLM-managed lands are concentrated along the John Day River canyon, and in Hay and Thirtymile Creeks. About 40 square miles of Umatilla National Forest lands are located in the uplands around Kinzua in Wheeler County. The Corps of Engineers manage a small amount of land near the mouth of the John Day River along the Columbia River.

The 100 miles of the John Day River between Clarno and Tumwater Falls are part of the designated State Scenic Waterway. The John Day River State Wildlife Refuge, from the mouth upriver for 84 miles to Thirtymile Creek, provides a resting area for ducks and geese and provides habitat for various raptor species and other wildlife.

#### 3. LAND COVER AND LAND USE

Rangeland comprises about 57 percent of the subbasin area (see Figure 36 and Table 60). Most range is in private ownership although there is extensive use made of public range allotments on BLM land. There are 636,765 acres of private rangeland in Wheeler County alone. According to the SCS, deteriorated range is a major resource problem in Wheeler County, with 80 percent of privately owned range in poor (222,868 acres) or fair (286,544 acres) condition. The BLM has rated the majority of the public range in the Lower Subbasin as fair to poor. The condition of private rangeland is similar. Only 20 percent of privately owned range is in good or excellent condition.

About 30 percent of the subbasin is cropland, but less than 1 percent of the subbasin is irrigated. Dryland wheat farming is practiced on over 350,000 acres of loessal plateau soil. Loess is a materail formed from deposits of wind-transported silt. Loessal soil can be eroded easily by both wind and water. Conservation tillage practices such as contour plowing, terracing, no-till, and crop residue management have been encouraged to minimize erosion. The practice of clean cultivation during the fallow year continues to contribute to erosion and sedimentation. Erosion hazard for these plateau soils range from slight to severe with annual soil losses ranging from 2.5 to 15 tons per acre.

EXHIBIT \_\_\_\_\_ PAGE \_3\_\_OF \_

Figure 36



LOWER SUBBASIN LAND OWNERSHIP AND LAND COVER

Riparian areas make up less than 1 percent of subbasin area, yet are often the most heavily used for recreation, grazing, agriculture, and wildlife habitat. A riparian inventory conducted on public land by the BLM in 1981 indicates that most areas under its management are in stable condition. Only a small fraction of riparian areas are deteriorating.

| Ta | bl | le | 60 |  |
|----|----|----|----|--|
|    |    |    |    |  |

| LOWER | SUBBASIN<br>(acres) | LANDCOVER |
|-------|---------------------|-----------|
|       |                     |           |

| Туре  | Acres  |
|---|--|
| Range and Pasturelands<br>Forestland (grazed)<br>Forestland (not grazed)<br>Cropland<br>Other | 758,911<br>116,600<br>0<br>405,740<br><u>54,400</u><br>1,335,651 |

Source: Department of Agriculture Small Watershed Reconnaissance Study, 1984.



McDonald Ferry is 1,475,500 acre-feet. Peak flow for the period of record occurred on December 24, 1964, when discharge reached 42,800 cfs. On other occasions, such as in 1966, 1973, and 1977, the river ceased flowing. There are also gages on Rock Creek, Lone Rock Creek, and Butte Creek.

Peak discharge occurs from late March to early June, with 22 percent of runoff occurring in April and 21 percent in May. Low flows occur from July through November.

The Lower Subbasin can be characterized as an area that receives water, as opposed to one that produces it. Most streams in the subbasin are nearly ephemeral, almost ceasing to flow in summer.

Of the three gaged streams, Rock Creek is the largest. The mean monthly flows range from 120 cfs in March to less than 1 cfs in September. Both Butte Creek and Lone Rock Creek (a tributary of Rock Creek) average less than 1 cfs from July through October. Mean monthly minimum flows average 0.2 cfs or less on Butte Creek throughout the entire year. On Rock and Lone Rock Creeks, mean monthly minima drop to zero July through September.

All three streams have stopped flowing completely at times. Lone Rock Creek stopped flowing at some time at least 10 out of the 13 years between 1966 (first year of record) and 1978 (last year of published record). Rock Creek's flow stopped at some point nine years of the same period. Butte Creek dropped to zero flow four of the seven years between 1972 (first year of record) and 1978. Generally, no-flow conditions last from August through September. In especially dry years, flows can stop as early as July and do not resume until October.

#### 2. GROUND WATER

Columbia River Basalt, Alkali Canyon Formation, Clarno Formation, and Quaternary Alluvium are the major hydrogeologic units in the subbasin. The Columbia River Basalt Group is a sequence of basalt flows more than 3,000 feet thick in the vicinity of the Columbia River. Data from 57 wells producing from basalt in Sherman County west of the John Day River show a range of production between 4 and 300 gpm. Usable data from 38 wells producing from basalts within Gilliam County indicate wells yielded from less than 1 to 1,500 gpm. Pump tests from 13 large-diameter wells (greater than 12 inches in diameter) in the northeastern part of Gilliam County showed well yields to be from 50 to 2,000 gpm. These deep, large-diameter wells may more accurately represent the hydrologic potential of the basalt. However, it is not known if recharge is adequate to sustain a great number of these wells.

The Alkali Canyon Formation occurs to the south and west of Arlington. Negligible data are available from wells pumping from the formation. Nearly all wells drilled in the area penetrate through the formation and tap the Columbia River Basalt. The Alkali Canyon Formation is not considered an important aquifer.

EXHIBIT \_\_\_\_\_ PAGE \_\_\_\_ OF 6

The extensive environmental quality monitoring activities around the Chem-Security Systems, Inc., hazardous waste storage site near Arlington have identified no pollution problems for surface or ground water. Outside of this area, ground water quality is unknown due to lack of water quality data.

#### Table 64

#### LOWER SUBBASIN SEWAGE TREATMENT PLANTS

| Source    | Type<br>of<br>Facility                       | Year<br>Built | Design<br>Population | Connected<br>Population | Design<br>Flow<br>(MGD) | Connected<br>Flow<br>(MGD) | Current<br>Raw<br>Waste (#POD)<br>Load (Day) | Current<br>Treated<br>Waste (#HOD)<br>Load (Day) | Current<br>Permitted<br>Waste (#POO)<br>Load (Day)             |
|-----------|--|---------------|----------------------|-------------------------|-------------------------|----------------------------|--|--|--|
| Arlington | Activated<br>Sludge<br>and<br>Sand<br>Filter | 1974          | 1000                 | 455                     | 0.125                   | 0.04                       | 62   | 4  | 31, discharge<br>to Columbia<br>River.                         |
| Condon    | Activated<br>Sludge<br>and<br>Lagoon         | 1971          | 1200                 | 950                     | 0.15                    | 0.10                       | 160  | 40   | 25, discharge<br>to Thirty Mile<br>Creek via Condon<br>Canyon. |
| Fossil    | Trickling<br>Filter                          | 1952          | 1000                 | 535                     | 0.15                    | 0.05                       | 90   | 20   | 38, discharge<br>to Butte Creek.                               |
| Moro      | Lagoon                                       | 1970          | 430                  | 250                     | 0.045                   | 0,035                      | 43   | No<br>Discharge                                  | No discharge,<br>irrigation<br>near Barnum<br>Canyon Creek.    |

Source: Department of Environmental Quality, 1985.

#### D. WATER USE AND CONTROL

#### 1. WATER RIGHTS

Irrigation accounts for about 87 percent of the appropriated water in the Lower Subbasin. Over 40 percent of the irrigation water use is in the Rock Creek drainage. Municipal uses by the communities of Condon, Fossil, and Arlington also are important. Table 65 summarizes water rights in the subbasin.

Regulation of water use by the watermaster normally begins in May and June. The Rock Creek drainage, until recently, was the area of most intensive regulation. In the last 10 years, many Rock Creek water users have begun pumping from newly drilled wells for use as supplemental irrigation water supplies, reducing the need for regulation by the watermaster. Generally, streams tributary to the John Day are already dry or nearly dry by the time regulation for minimum flows is required. As a result, use of tributary waters generally is not affected by regulation for minimum streamflows.



Hydrology Report # 1

# WATER AVAILABILITY FOR OREGON'S RIVERS AND STREAMS: VOLUME 2; Technical Guide and Appendixes.

By

E. George Robison





Water Resources Department

William H. Young Director

0F 3

PAGE /

May 1991

## Appendix B; Table 5: (Contd.)

TOTAL COLOR

· · · · · · · ·

| N. FK. John D<br>Located in th | e NU di | at Monu | nent #1 | 046000<br>guart | (F)<br>er of | sec. 2   | town.  | 9s and r  | ange 2  | 7e . |      |      |  |
|--------------------------------|---------|---------|---------|-----------------|--------------|----------|--------|-----------|---------|------|------|------|--|
| FLOWS                          | Jan     | Feb     | Маг     | Apr             | May          | Jun .    | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 573     | 810     | 1313    | 2013            | 2563         | 1119     | 238    | 95        | 100     | 138  | 186  | 314  |  |
| 50% Exceed.                    | 1233    | 1578    | 2528    | 3358            | 3962         | 1890     | 439    | 148       | 135     | 173  | 303  | 635  |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |
| John Day R. a                  | t Serv  | ice Cr. | #14046  | 500 (F)         | )            |          |        |           |         |      |      |      |  |
| Located in th                  | e NW q  | uarter  | of the  | NE quart        | ter of       | sec. 18, | town.  | 9s, and   | range   | 23e  |      |      |  |
| Flows                          | Jan     | Feb     | Mar     | Арг             | May          | Jun      | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 1034    | 1390    | 2048    | 2848            | 3381         | 1566     | 288    | 87        | 116     | 284  | 419  | 626  |  |
| 50% Exceed.                    | 1973    | 2536    | 3883    | 4890            | 5460         | 2681     | 619    | 193       | 194     | 363  | 608  | 1079 |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |
| Butte Cr. nea                  | r Foss  | il #140 | 47100   | (LT)            |              |          |        |           |         |      |      |      |  |
| Located in th                  | e SE q  | uarter  | of the  | SE quart        | ter of       | sec. 13, | town.  | 7s, and   | range   | 21e  |      |      |  |
| Flows                          | Jan     | Feb     | Маг     | Арг             | May          | Jun      | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 0.3     | 0.6     | 0.9     | 0.9             | 0.7          | 0.5      | 0.3    | 0.2       | 0.1     | 0.1  | 0.1  | 0.2  |  |
| 50% Exceed.                    | 0.9     | 1.8     | 2.7     | 2.7             | 1.7          | 1.0      | 0.6    | 0.3       | 0.2     | 0.2  | 0.2  | 0.4  |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |
| Lone Rock Cr.                  | near    | Lone Ro | ck #140 | 47380 (         | (F)          |          |        |           |         |      |      |      |  |
| Located in th                  | e SE q  | uarter  | of the  | NE quart        | ter of       | sec. 36, | town.  | 5s, and   | range   | 23e  |      |      |  |
| Flows                          | Jan     | Feb     | Маг     | Арг             | May          | Jun      | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 8.8     | 15.5    | 21.2    | 16.5            | 5.4          | 1.3      | 0.1    | 0.0       | 0.0     | 0.2  | 1.0  | 3.4  |  |
| 50% Exceed.                    | 26.6    | 41.0    | 52.3    | 40.9            | 12.2         | 2.7      | 0.5    | 0.1       | 0.0     | 0.6  | 2.7  | 8.8  |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |
| Rock Cr. abov                  | e Whyt  | e Park  | near Co | ndon #14        | 047390       | (LT)     |        |           |         |      |      |      |  |
| Located in th                  | e NE q  | uarter  | of the  | SW quart        | ter of       | sec. 36, | town.  | 3s, and   | range   | 22e  |      |      |  |
| Flows                          | Jan     | Feb     | Mar     | Apr             | May          | Jun      | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 18.7    | 28.6    | 53.9    | 33.1            | 8.7          | 2.9      | 0.5    | 0.1       | 0.7     | 0.9  | 5.3  | 13.2 |  |
| 50% Exceed.                    | 60.2    | 107.3   | 139.6   | 87.5            | 29.0         | 7.4      | 1.8    | 0.7       | 2.3     | 2.6  | 10.6 | 31.9 |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |
| Rock Cr. abov                  | e Cayu  | se Cany | on near | Condon          | #14047       | 400 (LT  | )      |           |         |      |      |      |  |
| Located in th                  | e NW q  | uarter  | of the  | SW quart        | ter of       | sec. 3,  | town.  | 3s, and i | range a | 22e  |      |      |  |
| Flows                          | Jan     | Feb     | Mar     | Арг             | May          | Jun      | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 27.7    | 43.9    | 61.9    | 40.2            | 13.9         | 3.2      | 0.5    | 0.2       | 1.0     | 0.7  | 2.6  | 7.3  |  |
| 50% Exceed.                    | 78.5    | 110.6   | 146.9   | 100.2           | 32.4         | 8.8      | 1.7    | 0.7       | 1.7     | 1.8  | 6.4  | 19.9 |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |
| John Day R. a                  | t McDo  | nald Fe | rry #14 | 048000          | (F)          |          |        |           |         |      |      |      |  |
| Located in th                  | e NE q  | uarter  | of the  | NW quart        | ter of       | sec. 11, | town.  | 1n, and   | range   | 19e  |      |      |  |
| Flows                          | Jan     | Feb     | Маг     | Apr             | May          | Jun      | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 1114    | 1579    | 2152    | 2890            | 3373         | 1646     | 302    | 74        | 96      | 268  | 433  | 656  |  |
| 50% Exceed.                    | 2208    | 3009    | 4264    | 5174            | 5671         | 2893     | 680    | 195       | 180     | 360  | 625  | 1163 |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |
| Buckhorn Cr.                   | near L  | one Roc | k (Hist | orical n        | nisc. m      | easureme | nt sit | e)        |         |      |      |      |  |
| Located in se                  | c. 8,   | town. 6 | s, and  | range 24        | ie           |          |        |           |         |      |      |      |  |
| FLOWS                          | Jan     | Feb     | Маг     | Apr             | May          | Jun      | Jul    | Aug       | Sep     | Oct  | Nov  | Dec  |  |
| 80% Exceed.                    | 4.0     | 6.1     | 7.6     | 6.2             | 2.7          | 0.9      | 0.1    | 0.0       | 0.0     | 0.3  | 0.8  | 1.9  |  |
| 50% Exceed.                    | 10.7    | 14.9    | 17.7    | 14.6            | 5.9          | 1.9      | 0.6    | 0.1       | 0.1     | 0.6  | 1.9  | 4.5  |  |
|                                |         |         |         |                 |              |          |        |           |         |      |      |      |  |



# Appendix F; Table 5. Water availability analysis for selected sites in the John Day basin.

### John Day R. at McDonald Ferry (Applic)

|                     | Jan  | Fcb  | Mar  | Apr  | May  | Jun  | Jul | Aug | Sep | Oct | Nov | Dec  |
|---------------------|------|------|------|------|------|------|-----|-----|-----|-----|-----|------|
| Gaged 80% Ex. Flow  | 1114 | 1580 | 2152 | 2891 | 3374 | 1647 | 303 | 75  | 97  | 269 | 434 | 657  |
| Gaged 50% Ex. Flow  | 2208 | 3010 | 4265 | 5175 | 5672 | 2893 | 681 | 196 | 180 | 361 | 626 | 1163 |
| Instream Wat. Right | 20   | 20   | 20   | 20   | 20   | 20   | 20  | 20  | 20  | 20  | 20  | 20   |
| 80% Ex. Flow W.A.   | 1094 | 1560 | 2132 | 2871 | 3354 | 1627 | 283 | 55  | 77  | 249 | 414 | 637  |
| 50% Ex. Flow W.A.   | 2188 | 2990 | 4245 | 5155 | 5652 | 2873 | 661 | 176 | 160 | 341 | 606 | 1143 |

#### Rock Cr. above Cayuse Canyon near Condon (Cert)

|                     | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|---------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Gaged 80% Ex. Flow  | 28  | 44  | 62  | 40  | 14  | 3   | 0   | 0   | 1   | 1   | 3   | 7   |
| Gaged 50% Ex. Flow  | 78  | 111 | 147 | 100 | 32  | 9   | 2   | 1   | 2   | 2   | 6   | 20  |
| Instream Wat. Right | 34  | 57  | 57  | 57  | 57  | 34  | 34  | 34  | 34  | 34  | 34  | 34  |
| 80% Ex. Flow W.A.   | -6  | -13 | 5   | -17 | -43 | -31 | -34 | -34 | -33 | -33 | -31 | -27 |
| 50% Ex. Flow W.A.   | 44  | 54  | 90  | 43  | -25 | -25 | -32 | -33 | -32 | -32 | -28 | -14 |

#### Rock Cr. above Whyte Park near Condon (Applic)

| Jan | Feb                                | Mar  | Apr  | May  | Jun  | Jul   | Aug  | Scp   | Oct  | Nov   | Dec  |
|-----|------------------------------------|--|--|--|--|---|--|---|--|---|--|
| 19  | 29                                 | 54   | 33   | 9  | 3  | 1   | 0  | 1   | 1  | 5   | 13   |
| 60  | 107                                | 140  | 88   | 29   | 7  | 2   | 1  | 2   | 3  | 11  | 32   |
| 34  | 57                                 | 57   | 57   | 57   | 34   | 34  | 34   | 34  | 34   | 34  | 34   |
| -15 | -28                                | -3   | -24  | -48  | -31  | -33   | -34  | -33   | -33  | -29   | -21  |
| 26  | 50                                 | 83   | 31   | -28  | -27  | -32   | -33  | -32   | -31  | -23   | -2   |
|     | Jan<br>19<br>60<br>34<br>-15<br>26 | Jan         Feb           19         29           60         107           34         57           -15         -28           26         50 | Jan         Feb         Mar           19         29         54           60         107         140           34         57         57           -15         -28         -3           26         50         83 | Jan         Feb         Mar         Apr           19         29         54         33           60         107         140         88           34         57         57         57           -15         -28         -3         -24           26         50         83         31 | Jan         Feb         Mar         Apr         May           19         29         54         33         9           60         107         140         88         29           34         57         57         57         57           -15         -28         -3         -24         -48           26         50         83         31         -28 | Jan         Feb         Mar         Apr         May         Jun           19         29         54         33         9         3           60         107         140         88         29         7           34         57         57         57         57         34           -15         -28         -3         -24         -48         -31           26         50         83         31         -28         -27 | Jan         Feb         Mar         Apr         May         Jun         Jul           19         29         54         33         9         3         1           60         107         140         88         29         7         2           34         57         57         57         57         34         34           -15         -28         -3         -24         -48         -31         -33           26         50         83         31         -28         -27         -32 | Jan         Feb         Mar         Apr         May         Jun         Jul         Aug           19         29         54         33         9         3         1         0           60         107         140         88         29         7         2         1           34         57         57         57         57         34         34         34           -15         -28         -3         -24         -48         -31         -33         -34           26         50         83         31         -28         -27         -32         -33 | Jan         Feb         Mar         Apr         May         Jun         Jul         Aug         Sep           19         29         54         33         9         3         1         0         1           60         107         140         88         29         7         2         1         2           34         57         57         57         57         34         34         34         34           -15         -28         -3         -24         -48         -31         -33         -34         -33           26         50         83         31         -28         -27         -32         -33         -32 | Jan         Feb         Mar         Apr         May         Jun         Jul         Aug         Sep         Oct           19         29         54         33         9         3         1         0         1         1           60         107         140         88         29         7         2         1         2         3           34         57         57         57         57         34         34         34         34         34           -15         -28         -3         -24         -48         -31         -33         -34         -33         -33           26         50         83         31         -28         -27         -32         -33         -32         -31 | Jan         Feb         Mar         Apr         May         Jun         Jul         Aug         Sep         Oct         Nov           19         29         54         33         9         3         1         0         1         1         5           60         107         140         88         29         7         2         1         2         3         11           34         57         57         57         34         34         34         34         34         34           -15         -28         -3         -24         -48         -31         -33         -34         -33         -33         -29           26         50         83         31         -28         -27         -32         -33         -32         -31         -23 |

Note: The actual flow was based on record extension of the entire record to the 1967-1986 period.

#### John Day R. at Service Cr. (Cert)

|                     | Jan  | Fcb  | Mar  | Apr  | May  | Jun  | Jul | Aug | Sep | Oct | Nov | Dec  |
|---------------------|------|------|------|------|------|------|-----|-----|-----|-----|-----|------|
| Gaged 80% Ex. Flow  | 1034 | 1390 | 2049 | 2848 | 3382 | 1566 | 289 | 87  | 117 | 284 | 419 | 627  |
| Gaged 50% Ex. Flow  | 1974 | 2537 | 3883 | 4891 | 5461 | 2681 | 619 | 194 | 195 | 364 | 608 | 1079 |
| Instream Wat. Right | 30   | 30   | 30   | 30   | 30   | 30   | 30  | 30  | 30  | 30  | 30  | 30   |
| 80% Ex. Flow W.A.   | 1004 | 1360 | 2019 | 2818 | 3352 | 1536 | 259 | 57  | 87  | 254 | 389 | 597  |
| 50% Ex. Flow W.A.   | 1944 | 2507 | 3853 | 4861 | 5431 | 2651 | 589 | 164 | 165 | 334 | 578 | 1049 |

#### N. Fk. John Day R. at Monument (Applic)

|                     | Jan  | Feb  | Mar  | Apr  | May  | Jun  | Jul  | Aug | Sep | Oct | Nov | Dec  |
|---------------------|------|------|------|------|------|------|------|-----|-----|-----|-----|------|
| Gaged 80% Ex. Flow  | 573  | 810  | 1314 | 2013 | 2564 | 1119 | 2.39 | 96  | 101 | 138 | 186 | 3147 |
| Gaged 50% Ex. Flow  | 1234 | 1578 | 2528 | 3359 | 3962 | 1891 | 440  | 149 | 136 | 173 | 304 | r35  |
| Instream Wat. Right | 235  | 235  | 380  | 380  | 380  | 235  | 175  | 175 | 175 | 175 | 235 | 235  |
| 80% Ex. Flow W.A.   | 338  | 575  | 934  | 1633 | 2184 | 884  | 64   | -79 | -74 | -37 | -49 | 79   |
| 50% Ex. Flow W.A.   | 999  | 1343 | 2148 | 2979 | 3582 | 1656 | 265  | -26 | -39 | -2  | 69  | 400  |



| 0°12<br>0°26<br>0°26<br>0°33<br>102<br>35°8<br>38°0<br>38°0<br>0°22<br>0°52<br>0°52 |             | Ĵ         | и., R.20 E, | op<br>op<br>op<br>op<br>op<br>op<br>op<br>op<br>op<br>op | otag ሂምዝ<br>ይዩን ይገለታለያ | Oct. 28, 1976<br>Dec. 23, 1976<br>June 9, 1976<br>June 22, 1976<br>June 24, 1976 |
|---|-------------|-----------|-------------|--|------------------------|---|
| DISCHARGE   | CAGE-HEIGHT |           |             | NOITADOJ   | 1314 (113              | 3740  |
| тииор<br>Mbffff2  | )<br>E      | <i>4E</i> | Y RIVER     | SOTOTI<br>SOTOTI<br>SOTOTI                               | han                    | ROCK Creek  |

| MISCELLANEOUS<br>MEASUREMENT No. BO<br>Rock Creek  | AM DY 17070204 20<br>John Day River  | 5 <sup>3</sup><br>GII |   |
|--|--|-----------------------|---|
| DATE   | LOCATION   | GAGE-HEIGHT<br>FEET   | SECOND.FEET   |
| Dec. 23, 1975<br>Jan. 27, 1976<br>Feb. 25, 1976<br>Mar. 23, 1976<br>May 6, 1976<br>June 7, 1976<br>June 22, 1976<br>July 27, 1976<br>July 27, 1976<br>Aug. 24, 1976<br>Dec. 23, 1975<br>Jan. 27, 1976<br>Feb. 25, 1976<br>Mar. 23, 1976<br>May 6, 1976<br>May 26, 1976<br>June 6 | NWWWANEW sec.10, T.1 S., R.21 E.<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do |                       | 6.49<br>41.2<br>134.7<br>114<br>33.2<br>13.6<br>6.22<br>2.96<br>0.40<br>5.09<br>4.32<br>37.6<br>31.7<br>108<br>32.4<br>9.65 |

|   | MISCELLANEOUS B STRE                       | DY John Day River   | 61111 | am Co.                   |
|---|--|---|-------|--------------------------|
| : | NOCK OF COM                                | LOCATION  | FEET  | DISCHARGE<br>SECOND-FEET |
|   | Apr. 28, 1931<br>May 24, 1934              | At Condon<br>Bl springs .5 mi ab West's Dam, 2.3<br>mi ab mouth, nr Klondike                |       | 14.1                     |
|   | May 24, 1934<br>June 1948<br>Nov. 10, 1965 | 300 yds ab West's dam<br>At mouth, nr Rock Creek station<br>SW1NW1 sec.32, T.1 S., R.22 E., | 35    | 4.33                     |
|   | Mar. 8, 1966                               | NE4SW4 sec. 36, T.J S., R.22 E. ab<br>Heppner Condon Hwy                                    |       | 5 <b>7</b> .]t           |
|   | Mar. 8, 1966                               | Dry Cr., nr Dam site (Condon)   |       | 21.5                     |
|   | Mar. 8, 1966                               | nr Condon   |       | 19.9                     |
|   | do   | ft bl barn  |       | 18.2                     |
|   | do   | NEANWA sec.24, T.1 N., R.20 E., ab<br>Rock Cr, 2.5 mi.                                      |       | 17.8                     |
|   | do   | SW4NE4 sec.15, T.1 N., R.20 E.,<br>Rock Creek, 30 ft ab bridge                              |       | 35.5                     |

EXHIBIT \_\_\_\_\_6 PAGE \_\_\_\_ OF \_\_\_

| DATE                           | LOCATION  | GAGE-HEIGHT | DISCHARGE<br>SECOND-FEET |
|--------------------------------|---|-------------|--------------------------|
| Mar. 10, 1966                  | SE4SW4 sec.15, T.2 S., R.22 E.,                       | •           | 153                      |
| Oct. 25, 1966                  | Sec.36, T.3 S., R. 22 E., ab bridge                   |             | 3.47                     |
| Oct. 26, 1966                  | Sec.6, T.4 S., R.23 E., at Murtah                     |             | 0.67                     |
| Dec. 6, 1966                   | Sec.26, T.2 S., R.22 E., bl Dry Cr.                   |             | 51.6                     |
| Dec 7 1070                     | bl Wolf Hohlow Br.                                    |             | 50.1                     |
| Dec. 3, 1970<br>Mar 25, 1971   | $NE_{L}^{1}$ sec.10, T.1 S., R.21 E.                  |             | 13.1<br>284              |
| Mar. 25, 1971                  | SELSW sec.15, T.2 S., R.22 E.                         |             | 260<br>277               |
| Mar.26, 1971<br>May 25, 1971   | SELSWI sec.15, T.1 N., R.20 E.                        |             | 245<br>9.34              |
| do                             | NW1NE1 sec.10, T.1 S., R.21 E.                        |             | 9.28                     |
| Oct. 28, 1975<br>Nov. 25, 1975 | NWANEA sec.10, T.I S., R.21 E. at<br>Hwy brdg at Olex |             | 0.52                     |
|                                | 0   |             |                          |
| STATE PRINTING SUTIO           | but   |             |                          |

|  | LOCATION   | FEET | DISCHARGE<br>SECOND-FEET   |
|--|--|------|--|
| June 6, 1976<br>June 22, 1976<br>Aug. 24, 1976<br>Oct.28, 1975<br>Dec. 23, 1976<br>Jan. 27, 1976<br>Feb. 25, 1976<br>Mar. 23, 1976<br>May 6, 1976<br>May 6, 1976<br>June 9, 1976<br>June 22, 1976<br>June 22, 1976<br>July 27, 1976<br>Aug. 24, 1976 | do<br>do<br>do<br>SWIANEIA Sec.24, T.1 N., R.20 E., 6<br>mi nw of Olex<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do |      | 0.77<br>0.77<br>2.21<br>0.38<br>0.51<br>38.0<br>31.5<br>107<br>20.8<br>0.20<br>2.0<br>1.19<br>0.51<br>0.43 |
| ar   |  |      |  |

|                | TRIBUTARY TO OR DIVERTING FROM     |             | COUNTY                   |
|----------------|------------------------------------|-------------|--------------------------|
| MISCELLANEOUS  | DL 17070201                        | Quent       | 50                       |
| 94             | John Day River                     | Grand       | 00                       |
| Rock Craek     | U.VIII. III.                       | GAGE-HEIGHT | DISCHARGE<br>SECOND.FEET |
| DATE           | LOCATION                           |             |                          |
|                | Mouth, 6 mi northwest of Dayville  |             | 0 8 Est                  |
| Sept. 17, 1949 | Mouth                              |             | 0.36                     |
| Aug. 31, 1951  | Mouth, in Et soc.18, T.12 S., R.20 |             | 0.83                     |
| Aug. 23, 1951  | Housin, in 12                      |             | 0.05                     |
| Aug.4, 1952    | de                                 |             | 20.4                     |
| Auly 15, 1953  | 40 9                               |             | 2.15                     |
| Cont 8 1953    | do                                 |             | * 1.5 Es                 |
| 50pt. 0, 1055  | do A (N X)                         |             |                          |
| July 21, 1999  | Drainage area, 292                 |             | 1 0.03                   |
|                | o f mi sho mouth                   |             | 76 0                     |
| Sept. 18, 1950 | U.S IIII abo motor                 |             | 10.0                     |
| July 16, 1957  | At mouth                           |             | 3.30                     |
| 18 1959        | do                                 |             | 2.19                     |
| Aug. 10, 1))/  | NEL sec. 21. T.12 S., R.25 E.      | L           |                          |
| Aug. 12, 1960  | ME4 800.18, T.12 S., R.26 E., 0.5  | np          | 7 07                     |
| July 18, 1961  | NET Sec.ic, Dauville(292 sq mi Dr. | Ar.)        | 1.01                     |
|                | horthwest of Day ville (-)-        |             | 7.65                     |
| 1117 24 1962   |                                    |             | 7.22                     |
| Aug. 21, 1063  |                                    |             | 38.0                     |
| July 20, 190)  |                                    |             | 32.6                     |
| Jan. 6, 1964   |                                    |             | 1                        |
| Feb. 11, 1964  |                                    |             |                          |



| Name             | Priority | Acres  | CFC        | Creek Flow | Approximate Average<br>Cut-off Date |
|------------------|----------|--------|------------|------------|-------------------------------------|
| Marick *         | 1868     | 45.6   | 1.14       | 1 74       | August 1                            |
| West *           | 1868     | 12.6   | 0.32       | 1.46       | August 1                            |
| V. O. West       | 1869     | 11.6   | 0.29       | 1.75       | July 15                             |
| West *           | 1879     | 126.7  | 3,17       | 1 92       | June 22                             |
| Crum             | 1880     | 12.8   | 0.32       | 5 24       | June 20                             |
| Marick *         | 1883     | 46.4   | 1.16       | 6.4        | June 15                             |
| Marick *         | 1884     | 2.8    | 0.07       | 6.47       | June 14                             |
| West/Marick      | 1884     | 9.6    | 0.24       | 6.71       | June 13                             |
| Įrby             | 1884     | 19.7   | 0.49       | 7.2        | June 12                             |
| Childs *         | 1886     | 131.0  | 3.28       | 10.48      | June 8                              |
| West *           | 1888     | 19.6   | 0.49       | 10,97      | June 7                              |
| H. Weatherford   | 1890     | 48.1   | 1.2        | 12.17      | June 6                              |
| V. O. West       | 1890     | 17.5   | 0.14       | 12.61      | June 5                              |
| Pettyjohn        | 1893     | 51.0   | 1.28       | 13.89      | June 3                              |
| Olson            | 1893     | 10.2   | 0.26       | 14.15      | June 3                              |
| Marvel           | 1893     | 31.1   | 0.78       | 14.93      | June 2                              |
| Bettencourt      | 1894     | 93.1   | 2.33       | 17.26      | May 29                              |
| West *           | 1894     | 69.6   | 1.74       | 19.00      | May 25                              |
| Bettencourt      | 1895     | 29.0   | 0.73       | 19.73      | May 25                              |
| Ries             | 1895     | 15.5   | 0.39       | 20.12      | May 24                              |
| Wheelhouse       | 1895     | 54.2   | 1.36       | 21.48      | May 22                              |
| Pettyjohn        | 1896     | 58.3   | 1.46       | 22.94      | May 20                              |
| Davis *          | 1896     | 37.7   | 0.94       | 23.88      | May 18                              |
| Welner           | 1897     | 17.4   | 0.44       | 24.32      | May 18                              |
| Brooks *         | 1900     | 30.1   | 0.75       | 25.09      | May 17                              |
| V O Wort         | 1900     | 36.7   | 0.92       | 25.99      | May 15                              |
| V. U. West       | 1903 .   | 10.5   | 0.26       | 26.25      | May 14                              |
| Childe           | 1905     | 13.3   | 0.33       | 26.58      | May 13                              |
| H Westhenford    | 1905     | 17.4   | 0.44       | 27.02      | May 13                              |
| Welp             | 1910     | 90.4   | 2.41       | 29.43      | May 12                              |
| West             | 1917     | 12 5   | 0.41       | 29.84      | May 12                              |
| Pettviohn        | 1913     | 51.    | 1 28       | 31 43      | May 12                              |
| Welp             | 1914     | 15.26  | 0.38       | 31 81      | May 11                              |
| H. Weatherford   | 1914     | 167.1  | 4.18       | 35.99      | May 10                              |
| Bill West        | 1922     | 35.    | 0.44(1/80) | 36.43      | May 10                              |
| D'Albero         | 1936     | 24.    | 0.5 (1/80) | 36,93      | May 10                              |
| Bettencourt      | 1951     | 34.22  | 0.86(1/80) | 37.79      | May 9                               |
| , E. Weatherford | 1951     | 120.2  | 1.5 (1/80) | 39.29      | · May 9                             |
| Irby             | 1952     | 5.6    | 0.14(1/80) | 39.43      | May 8                               |
| Bemaer           | 1953     | 152.2  | 2.0 (1/80) | 41.43      | May 8                               |
| Irby             | 1966     | . 81.2 | 2.03(1/80) | 43.36      | May 7                               |
| D'Albero         | 1967     | 23.8   | 0.6        | 44.06      | May 6                               |
| Litte Brooke     | 1967     | 18.3   | 0.46       | 44.52      | May 6                               |
| Ries             | 1971     | 15.2   | · Q. 38    | 44.9       | May 5                               |
| Welp             | 1973     | 34.7   | 0.5 (1/80) | 45.4       | May 5                               |
| Ries             | 1975     | 3.     | 0.08       | 45.48      | May 5                               |
| H. Weatherford   | 1975     | 75.    | 1.9        | 47.38      | May 5                               |
| E. Weatherford   | 1975     | /1.4   | 1.9        | 49.18      | May 5                               |
| Trby             | 2/6/76   | 20.2   | 0.51       | 49.69      | May 4                               |
| Wilcke           | 2/19/76  | 52.4   | 1.56       | 51.25      | May 4                               |
| V. O. West       | 3/1/76   | 0.     | 0.15       | 51.4       | May 3                               |
| D'Albero         | 3/8/76   | 22.1   | 0.55       | 51.92      | May 3                               |
| Ries             | 6/28/76  | 10 11  | 0.35       | 52.5       | May 3                               |
| H. Weatherford   | 7/8/76   | 20.4   | 0.40       | 52.90      | May 3                               |
| Bettencourt      | 12/1/76  | 20.0   | 0.95       | 53.91      | May 2                               |
|                  | 11/1/10  | 20.0   | 0.12       | 54,03      | May 2                               |

EXHIBIT 7 PAGE 0F

Subject to Stipulation

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ROCK CREEK WATERSHED IMPROVEMENT PLAN

- Martin

Sponsored By:

Gilliam County Soil and Water Conservation District P.O. Box 106 Condon, OR 97823

Morrow County Soil and Water Conservation District P.O. Box 127 Heppner, OR 97836

Wheeler County Soil and Water Conservation District P.O. Box 425 Fossil, OR 97830



#### INTRODUCTION

### History

The Rock Creek region was settled between 1860 and 1885 by cattle ranchers. As settlement expanded in the region, sheepraising supplemented cattle. By the early 1900's the number of sheep greatly exceeded cattle. Sheep grazed grasses that replaced the depleted native bunchgrass stands and were easier to trail to mountain areas for summer pasture. Shortly after the depression, numbers of other livestock built steadily and began to exceed sheep.<sup>1</sup> Today livestock grazing, from traditional Hereford to newly-developed breeds, is standard throughout the watershed,

The broad, rolling plateau of Rock Creek Watershed supported dryland wheat production while irrigation developed in canyon bottoms. Surface irrigation systems included diversion structures along the mainstem and in tributary streams. These structures provided flood irrigation for a variety of crops; currently the primary crop is alfalfa. Many gravity-flow diversion systems do not appear to be in use. Numerous stock ponds, small impoundments, and mill ponds have been built over the years. Many of these structures for surface irrigation and storage have fallen into disrepair or washed out entirely. Late season baseflow has become unreliable and, in fact, is nonexistent through much of the summer.<sup>2</sup>

The headwaters areas consist of timber and grassy prairies (meadows). Historically, the headwaters have been managed for timber production and livestock grazing. Forest timber includes Douglas-fir, ponderosa pine and tamarack. The remains of logging mills are seen at Cone Mill, on Buckhorn Creek, and at Spoo Mill, on the Middle Fork of Rock Creek.

Rock Creek Watershed has a history of extensive flooding and streambank erosion. Residents along Rock Creek, particularly the lower end, have individually and collectively made many attempts to alleviate problems. A Rock Creek Water Control District (RCWCD) was formed in 1965 and pursued construction of a reservoir for flood control, for irrigation water, and recreation.<sup>3</sup> Due to rising costs and lack of a consensus among affected parties, no reservoir was built.

<sup>1</sup>Ray W. Chapin, <u>Soil Conservation Survey of the Rock</u> <u>Creek Project</u>. (Region 11: USDA, Soil Conservation Service, 1939), p. 5.

<sup>2</sup>Joe Irby, Olex resident, discussion about Rock Creek. November 15 1990.

<sup>3</sup>Minutes of RCWCD, February 24, 1965.

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The movement of water through the watershed is a function of characteristics of land cover, soils and geology.<sup>8</sup> As indicated by hydrographs in Appendix A, water passes through the watershed in the winter and early spring months. Over 70% of runoff occurs in the three months of January, February, and March. According to numerous landowners, flooding most commonly occurs in two situations: (1) rapid runoff on frozen ground during winter months; and, (2) sudden localized storms in summer months.

The location of numerous springs is a function of the <u>geology</u> and soil characteristics of the region. The intermittent characteristics of flow in the main channel of Rock Creek is related to the geology and soil deposits in the valley floor. For example, near the mouth of Rock Creek a spring in the streambed produces flow continuously, whereas except for several springs, no water may be found upstream until above the town of Olex. In numerous wider canyon bottoms, where the soils are deeper and widespread, as the canyon narrows, flow surfaces. These areas are found on the major tributaries and mainstem at the following locations: T5S R24E Sec 2, 5; T4S R24E Sec. 36; T5S R23E Sec. 10.

#### Soils

Soil types and depths vary within the watershed. On the uplands, soils are generally a shallow to deep, well drained, silt loam complex. Associations include Ritzville, Mikkalo, Lickskillet, Wrentham, Condon, Valby,<sup>9</sup> Rhea, Morrow and Bakeoven.<sup>10</sup> The wind-deposited soils on the Plateau are also found in the intercanyon range county between the Plateau and creek bottoms. Winds predominately from the southwest deposit soils to a greater depth on north-facing slopes. In the broader valley bottoms such as in the Lonerock area the silt loams range to a cobbly or stony loam. Associations here include the Waha, Gwinly, Rockly, Tubs, Simas, Ukiah, and Waterbury.<sup>11</sup>

Upper Basin rangeland soil associations include Waterbury, Waha and Rockly. In forested areas, soils are generally very shallow over a rock complex. Associations here include Hankins, Klicker

<sup>8</sup>Ray K. Linsley and others, <u>Hydrology for Engineers</u>, (New York: McGraw-Hill series in water resource and environmental engineering, 1975), p. 224.

<sup>9</sup>Richard E. Hosler, <u>Soil Survey of Gilliam County</u>, <u>Oregon</u>, (Washington, D.C.: USDA, Soil Conservation Service, 1984), p. 173.

<sup>10</sup>Richard E. Hosler, <u>Soil Survey of Morrow County Area</u>, <u>Oregon</u>, (Washington, D.C.: USDA, Soil Conservation Service, 1983), p. 226.

<sup>11</sup>Hosler, <u>Soil Survey of Gilliam County, Oregon</u>, p. 173.

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over a rock complex. Associations here include Hankins, Klicker and Boardtree. Mountain prairies or meadows, however, are composed of a poorly-drained fine loam/clay/ash complex of considerable depth.

#### Climate

The climate is typical for central Oregon. <u>Average annual</u> precipitation varies from 8 to 25 inches as elevation increases. The greatest portion of the precipitation occurs in the winter and spring months from storms approaching from the south and southwest. Sudden severe convectional storms in summer months can lead to extreme localized flood peaks. Temperatures have ranged from summer highs of over 100 °F to winter lows of less than minus 25 °F.<sup>12</sup>

#### Plant Communities

Plant species evolved in this region in relation to soils and climate described above. The grasses, forbs, shrubs, and trees within the headwaters, uplands, and riparian areas play a vital role in soil and water conservation. A common listing of native, introduced and non-desirable vegetation is shown in Appendix B. Douglas-fir, ponderosa pine, tamarack, aspen, and alder are found in the headwaters.

The rangelands are a true grassland. The potential native vegetation is approximately 90% composed of bluebunch wheatgrass, Idaho fescue, and Sandberg bluegrass.<sup>13</sup> Riparian areas show an extensive growth of alder with some willow and wetland plants such as sedges, rushes, grasses, cattails and other forbs.

#### Fishery Habitat

Rock Creek and tributaries have historically supported anadromous fish and resident native trout.<sup>14</sup> Warmwater species have been introduced in some areas.<sup>15</sup> During inventory along Rock Creek, observed accumulations of algal growth in isolated pools indicates warm water temperatures which

<sup>12</sup>Chris L. Wheeler, <u>An Engineering Report of the Rock</u> <u>Creek Watershed</u>, (Salem: State Engineer of Oregon, 1968), p. 3.

<sup>13</sup>Hosler, <u>Soil Survey of Gilliam County, Oregon</u>, p.70.

<sup>14</sup>Errol Claire, Fisheries Biologist, Oregon Department of Fish and Wildlife, discussion in John Day, August 13, 1990.

<sup>15</sup>Shaun P. McKinney, Fisheries Biologist, Umatilla National Forest, Heppner Ranger District, discussion in headwaters, December 4, 1990.
Lack of stable streamflow/summer flows. Summer flows for irrigation and instream use is minimal to nonexistent. Stream hydrographs shown in Appendix A reinforce what irrigators know: during much of the summer, there is no water available in Rock Creek. Alternatives discussed among the RCPG include:

- Thin fir thickets
- Juniper thinning
- Structures in creek
- Flood irrigation versus sprinkler
- Spring developments to utilize range
- Riparian management
- July rains
- stock ponds

<u>Too much water in winter - flooding.</u> Noted damaging floods have occurred in 1914, 1954, 1956, 1964 and 1965.<sup>20</sup> Floods can affect a specific part of the watershed or can be widespread, as when overbank flows occur.

Widespread flooding occurs during sudden warming coupled with rain on frozen soil or snow. With frozen soils an impervious layer seriously reduces the water retention capability of the watershed. Surface runoff becomes concentrated and flooding develops in Rock Creek. Ice and debris carried by high flood waters jam in bridges and compound problems associated with flooding. Damage to buildings, roads, utility lines and loss of crop ground and livestock are results of flooding.

Localized convective summer storms also create damaging floods. For example, in late August 1990, a storm dropping 4 to 6 inches of rain in the lower end of Rock Creek watershed produced flooding in several draws, resulting in soil loss, cutbanks and property damage.

<u>Field washing - soil loss from cropland.</u> Soil loss from cropland has occurred in dryland areas and on irrigated bottoms. Alternatives discussed among the RCPG include:

- Conservation tillage
- Terraces
- Don't farm next to creek
- Plant grasses next to bank
- Check dams in creek
- CRP plant grasses
- Subsoiling frozen ground or stubble
- Rotations with grasses
- Flood irrigate versus sprinkler
- Crop residue

<sup>20</sup>Gilliam County Soil and Water Conservation Service and others, <u>Watershed Work Plan Rock Creek Watershed</u>, (USDA, Soil Conservation Service, 1975), p. 36.

EXHIBIT 8 PAGE 5 OF 7

- Grazing management
- Early seeding fall versus s
- Type of crops

Distribution of stock water. Livestock grazing is practiced throughout the watershed. Grazing areas include rangelands, riparian areas, wheat stubble, and forestlands. Water availability is a strong limitation to the effective use of grazing areas. Alternatives discussed among the RCPG include:

- Spring developments
- Water impoundments
- Fencing
- Put water in correct places
- Haul water in
- Pipelines
- Drill wells

Lack of vegetation. Forage for livestock is limited in season and location. Diversity of grasses on the bottoms is limited. Great variability of grasses is found with changes in soil, slope and orientation. The inventory of range, as noted by the SCS, shows poor to excellent conditions. Rangeland condition is poorest on the valley bottoms and is excellent higher up on slopes.

Water conservation and management. Rock Creek watershed yield can vary considerably year to year. Streamflow records indicate approximately 20,000 to 40,000 acre-feet annually (see Appendix A). The pattern of release is such that water passes through the watershed during winter and early spring months. Water is not available in the creek during summer months. The emphasis was stressed to <u>capture</u>, <u>store</u>, <u>and safely release</u> water where it reaches the ground surface. This implies land treatment alternatives and solutions. Alternatives discussed among the RCPG include:

- Replant trees in upper watershed
- Build ponds or water basins
- Plant grass along roadsides
- Slow the water down in streams
- Install check dams
- Plant buffer strips along drainageways (grassed waterways)
- Encourage trashy fallow/residue
- Install more diversion ditches
- Practice subsoiling
- Use single shank on frozen soils on planted fields
- Improve grazing management
- Extend Conservation Reserve Program
- Develop upland water storage reservoirs
- Eliminate water use through noxious weed control
- Contour seeding
- Grass seeding on stream banks
- Improve construction of logging roads

EXHIBIT 8 PAGE 6 OF 7

grasses in the timber understory and along tributaries. Proper grazing practices include leaving one half a years growth and using rotation and deferred/rotation patterns of grazing.<sup>25</sup> To provide options in water supply for livestock it is recommended to extensively pursue out of stream stock tanks (OOSST).

Tributaries in these areas could also be important for fish spawning.<sup>26</sup> Improvements to fish habitat, primarily through construction of small instream checks, will create more spawning pools. This will also help regulate water releases from the forestlands, falling within all three watershed objectives mentioned earlier. Unlike headcutting found in higher elevations, the primary soil loss in these reaches is through streambank erosion. Small checks in conjunction with vegetation will slow water down through these tributary streams. Locations for instream checks and OOSST are shown in Appendix H.

#### Upper Basin Rangelands

Continuing down the watershed it is appropriate to describe the rangeland and major tributaries from the forest/rangeland transition to the junction of Lonerock Creek with the mainstem. This area includes the following watercourses: the mainstem below Anson Wright Park, Rood Canyon, Middle Fork, Juniper Fork, Buttermilk Canyon, and Lonerock Creek. These areas are valuable for livestock grazing; they also contain important fish habitat. A future vision suggests management practices to improve livestock distribution. In general, livestock should be brought up off the bottoms. However, in some cases livestock density is too high around water source and feed areas on the Plateau.

Areas of juniper trees, particularly in the Lonerock Creek watershed, should be thinned and used as riprap in tributary streams. Mechanical treatment of rangeland and seeding to perennial grasses should be pursued in areas of heavy grazing pressure, on bottoms, and along abandoned roads. Noxious weed control should be actively pursued through existing programs (Gilliam and Morrow Weed Agents and Rock Creek Range Conservation Corporation). Although the tributary streams mentioned above dry up in summer months there are several perennial springs that could be developed for livestock use or as groundwater recharge (subirrigated). This would improve grass production in these areas, cool surface water, and improve baseflow. These springs include several areas on the left side of Lonerock Creek, Wick Creek and along the mainstem near Hardman.

<sup>25</sup>Allen Koester, Gilliam District Conservationist, SCS, discussion of November 13, 1990.

<sup>26</sup>McKinney, discussion in headwaters, December 4, 1990.



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| 0-192a-1 | -1-26, | ·**2/*2 | -      | <br>F    | THIRIT                | .9            |  |           | 1. 19 - 14 - 44 |          | 54 E 2              |                | OF   | FICE           | OF ST       | OR    | EGON           | SINEER    |                           | 14047                    | We we                    | HG.  | File No. State   | G. S           | 50   |
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|          |        |         |        | P        | AGE 2                 | - OF          | 13 .                                     | •         |                 | · ·····  |                     |                |  | Water          | Resourc     | D     | epartn         | nent      | in in a                   | B                        | al al                    |  |                  |                |  |
| Daily G  | age I  | Ieight  | , in I | eet, a   | nd Discha             | rge, in       | Second-f                                 | eet, of . | · Lo            | CK       | Creek               | ç              |  | at-            | Rock        | 10    | reel           | K, Ori    | g for the                 | year ending Sep          | L. 80, 192 5             | Table of use: H  | alf tenths       | tt. to         | ft.  |
| -        |        | . D     | rainag | e area . |                       |               | quare mile                               | a.        | (               | Mrs      | J.M.Y               | lest           | , Obser  | Ter) (         | Dage read   |       | Hund           | edtha     |                           | noo a day                |                          | Used rating tabl   | e dated _ 4-     | 16-2           | 6  |
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| nd-fe    |        |         | Â      | height   | Discharge             | beight        | Discharge                                | Gage      | Discharge       | Gage     | Discharge           | Gage<br>height | Discharge  | Gage<br>height | Discharge   | Day   | Gage<br>height | Discharge | Gage<br>height Discharge  | Gage<br>height Discharge | Gage<br>height Discharge | e height Discharge   | height Discharge | A +            | SH &   |
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| Dis      |        |         | 8      |          |                       |               |  |           | 1               |          |                     |                |  |                |             | 8     | 2.90           | 54        | 2.00 3.5                  | 2.55 33                  | 1.95 1.6                 | 2.00 3.5   | 2.15 .11 -       | 8 8            | Chert  |
| NS       |        |         | 9      |          |                       |               |  |           |                 | 12       |                     |                |  |                | 4           | 9     | 2.70           | 42        | 2.00 3.5                  | 2.50 30                  | 2.00 3.5                 | 2.00 3.5   | 2.30 19          | 0 -            | JUN  |
| Xt       |        |         | 10     |          |                       |               |  | -         |                 |          |                     |                |  |                |             | 10    | 2.75           | 45        | 2.05 5.8                  | 2.35 22                  | 2.00 . 3.5               | 2.00.3.5   | 2.00 3.5         | 10 \$X         | C RY   |
| ap of    |        |         | 11     |          | •                     |               |  |           |                 |          |                     |                | 1  |                |             | 11    | 2.50           | 30        | 2.05 5.8                  | 2.35 22                  | 2.00 3:5                 | 2.00 3.5   | 195 1.6          | 11             | 141  |
| 10       |        |         | 12     |          | 1.                    |               |  |           |                 |          |                     |                |  |                |             | 12    | 2.50           | 30        | 2.00 . 3.5                | 230 19                   | 2.00 3,5                 | 2.00 3.5   | 2.00 3.5         | 12 6           | 1.1.0  |
|          | 2      | 1 4.    | 18     | 1.2.2    | 1. 1                  | 1000          | -  |           |                 | • =      |                     | -              | 1. 1. 1. 1   |                | · · · · · · | 18    | 2.60           | 36        | 205 : 58                  | 2.20 14                  | 1195 1.6                 | 2.00 3:5   | 2.45 27-         | 18 -           | 1,3  |
|          |        | 1.      | 14     |          | N                     |               | ·  |           | -               |          |                     |                | *****<br>**  | -              | 1           | 41    | 2.40           | 24        | 205 5.8                   | 2.30 19                  | 1.95 1.6                 | 2.00 3.5   | 2.30 -19         | 14 64          | C.T.   |
| i. i     | :      |         | 15     |          | 8.14                  |               |  | 100       |                 | 1.00     | SAN HERE            | 18.1           | 1  |                | 3           | 25    | 2.40           | 24        | 2.04 15.3                 | 2:15 511:                | 2:00 3.5                 | 2.10 8.0   | 2.00 3.5         | 15 :           |  |
| 5 5      |        | 1       | 16     |          |                       | N GVE         | 1.1°                                     |           | -               | 1        |                     | 15             | 1. 2.1.2   |                | 1. 26       | B     | 2.55           | 33:       | 2.00 3.5                  | 2.15 11                  | 2:00 13.5                | 2.10 8.0   | 2.00 . 3.5       | 10-            |  |
|          | 1.     |         | 17     | 14.30    | Photo and             |               |  |           |                 | 1 24     | 1.1                 | · · ·          | ·  | 2.85           | 51          | 17    | 2:50           | 30        | 2.00 3.5-                 | 2.01 4.0                 | 2.00 3.5                 | 2.10 8.0   | 1.80 0           | 17 5           | Per la companya de la |
|          |        |         | 18     | . Court  |                       |               |  |           |                 | -        | 191. 191            | 13.43          | 14201  | 2.92           | 34          | Lis ( | 2.65           | 39:       | 2.00 3.5.                 | 2.00 3.5                 | 2.00 3.5                 | 2.10 8.0   | 2.00 3.5         | 15 1           | the state  |
|          | 1      |         | 19     | * 12     |                       | ** _          | -  | -         |                 | -        | 1.41 2              | -              | 4  | 291            | 54          | 19    | 2.65           | 39.       | 2.00 3.5                  | 2.00 3.5.                | 2.00 3.5                 | 2.10 8.0   | 2.00 3.5         | 19             | 1 1'   |
|          |        | i       | 20     |          | -                     |               |  |           |                 |          | 1 1                 |                | 1 21.4   | 290            | - 54        | 20    | 3.20           | . 13      | 2.10 .8.0                 | 2.00 3.5                 | 2.00 3.5                 | 2.10 8.0   | 2.00 3.5         | 20 3           | 50   |
| ot at    |        | 1.7     | 21     | and it   | ng bi a la            |               |  |           | •               |          | and and a           |                | Section.   | 3.20           | . 13.       | 21    | 3:08           | 67-       | 2.65 .39                  | 2.00 .3.5                | 2.00 3,5                 | 2.15 11.0  | 2.00 3.5         | 21 -           | 2 1 - 2  |
| 1 - 10   |        | PP Ste  | 22     | 25 SPA   | ter have              | 三日本           |  |           |                 | 1.1.1.   | aligi que contra la | A WAR          | AN TOP TAKEN TO  | 90ge           | 063         | 22    | 2.95           | ~5/1      | 4.00 126                  | 2.00 3.5                 | 2.01 4.0                 | 2.15 11.0  | 2.00 3.5         | 22 22          | 104  |
| 00       |        | 12      | 23     | - 2      | Section of Long       | in the second |  |           | ** 31k          | 1.000.21 | cathe refrect       | 1000           | and the second s | 225            | 164         | 23    | 0.00           | 160       | 3.50 92                   | 2.00 3.5                 | 2.0 40                   | 2.0/ 4.0   | 2.00 3.5         | 23 -           | 40   |
| 10       |        | 되는      | 24     | がなると     | なたのでは                 | 2611          | 226321<br>6565-6                         | 12.25     | - Antoniek      | 44.5     | 201444120           | 311.31         | 414 + 3 + 1<br>15 \$ 19 1  | 2.20           | 971         |       | 2.05           | EAG.      | 3,50 32.                  | 2,00                     | 2-01 4.0                 | 2.00 3.5.  | 2.00 3.54        | 24 8           | 物中的学   |
| ETT.     | 女生     | - 24    | 1 20   | YERANA.  | ADDI Maker            | 2432          |  |           | 1. 1.           | 13.52    | We let              |                | 144743/4415  | 200            | .4:001      | 20    | 000            | 10-       | 3.20 . 73                 | 2.00 3.3                 | 2.01-4.0                 | 2:00 3.5   | 2.00 3.5         | 25 -           |  |
| 17       |        | 計画      | 26     | 7452.4   | State and             | 空心局           | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 | 7         |                 | 19994    | 24 11.424           | 3-5            | HATEF  | 3.94           | 6.01        | 部     | 210            | 1421      | 3.20 13                   | 2.00 0.5                 | 2.0/ 4.0                 | 2.15 11  | 2.00 3,5         | 25             |  |
| age age  | 1      | 31.4    | 27     | A.M.     | the the second second | 2 - 17 14     |  | Part      |                 | -        |                     | 1.9 Cal-       | No. of the second  | 194            | 57          | 127   | 2.60           | .36       | 2.90 54                   | 2.00 3.0                 | 2.0/ 4.0                 | 215 11   | 2.00 3.5         | 27             | 1 1  |
| E E      | 1      |         | 28     | 1.014    |                       | -             |  |           |                 | -        | -                   |                |  | 8 05           | 64          | 28    | 2.60           | 25        | 184 51                    | 2.00 2.5                 | 2.00 2.5                 | 2.15 11  | 2.13 11          | arter<br>arter |  |
| xfmt     | 1H     |         | 29     |          |                       | 12            |  |           | -               | -        |                     |                |  | 292            | .54         | 20    | 130            | 00        | 290 .54                   | 200 35                   | 2.00 0.5                 | 2.15 11  | 2.15 11          | 20 8           | а. н.<br>в. н.   |
| Mit      | NO     | 1       | 1 20   |          |                       |               |  |           |                 |          |                     |                |  | 2.92           | .54         | 81    |                |           | 282 48                    |                          | 200 3.5                  | 120 10   | 2.00 . 0.5       | 30             | -Period  |
|          | -      | Total   | Tor    | 45-0     |                       | 1.00          |  |           | No.             |          |                     |                |  |                | .975        |       |                | 294       | 916.8                     | 570.5                    | 1039                     | 2120   | 2181             | 51             | 42903  |
|          | Mean   | TOTAL   | 1      | 1        | 1.1                   | 1             |  |           |                 |          |                     |                |  | 15 da          | 1)65.0      | -     | 1.14           | 431-      | 29.6                      | 19.0                     | 3.35                     | 6.84   | . 7.27           | 15 -           | 7,290.5  |
| - 1      | Run-of | in acre | oft    |          | in the                | ·             |  |           | 1.15            | 6.5      |                     |                | 1.4  |                | 1930        | N.    | 6- 2           | 565       | 1820                      | 1130                     | 206                      | 420  | 433              |                | 8520   |
| 1        | Maxim  | am      |        | 1        |                       | 1             |  |           |                 | 2        |                     |                |  |                | 86 !        |       |                | 73        | 126                       | 73.                      | 4.0                      | 22   | 27               |                |  |
| 1        | Minim  | m       | -      | 111      | 27                    | -             | 14                                       |           |                 |          |                     |                |  |                | 51          | 2.    | 2              | 22        | 3.5                       | 3,5                      | 1.6                      | 3.5  | 0.               |                | 0  |
|          |        | -       | -      | 1.4.     | 5 1.0                 |               | -  | -         |                 | -        |                     |                |  | 1000           | Ar Ar Ar    | tre : | 1.11.41        |           | All and the second second |                          |                          | and the second s |                  | See. Com       |  |

| An and a general  |        | EX<br>PA  | HIBIT      | 9<br>. OF . | 13          |         | • • •                                    |           | 1 150 2 10 1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | 14 .   | OF              | FICE      | OF ST<br>Resource | ATI  | EGON<br>E EN<br>eparti | GINEER    | 2      | 15 · ·    | <        | 404       | 1000      | 2000      | ing:   | i.           | File       | No. {U.S.<br>State | 2    | 50               |
|-------------------|--------|-----------|------------|-------------|-------------|---------|--|-----------|---|--------|-----------------|-----------|-------------------|------|------------------------|-----------|--------|-----------|----------|-----------|-----------|-----------|--------|--------------|------------|--------------------|------|------------------|
| Daily Gage Height | , in i | Feet, a   | nd Discha  | rge, in     | Second-f    | eet, of |  | Coch      | K Cre   | ek     |                 | near      |                   | T    | Roc                    | KCr       | eek    | for the   | year end | ing Sep   | L 80, 191 | 2.6_      | Table  | of use: He   | alf tenths | 1-                 | tt t | tt.              |
|                   | I      | ge area   | 0.000      |             | square mile | a.      | (  | Trs       | IN.W  | est    | , Obse          | rver)     | Gage read         | to   |                        | hundr     | redth  | 2.5_ on   | ce a day |           |           |           | Used   | rating table | dated      | 4-                 | 10-  | - 26             |
| feet              | Day    | Gage      | Discharge  | Gage        | Discharge   | Gage    | DEC.                                     | Gage      | JAN.  | Gage   | FEB.            | Garo      | MAR,              | - 10 | Gage                   | APR,      | Gare   | AY ·      | JU       | NE        | Gage 1    | ULY       | Gage   | AUG.         | GAge       | PT.                | N    | CA S             |
| cond              | -      | actene    |            | neight      | 15 incharge | height  | Discharge                                | height    | Discharge   | height | Discharge       | height    | Discharg          | Ë Å  | height                 | Discharge | height | Discharge | height I | Discharge | height    | Discharge | height | Discharge    | height     | Discurree          | -    | 1237             |
| 8 8               | 1      |           |            | 100         | -           |         |  |           | -   | -      |                 |           | i                 | 1    | 2.3                    | 19.       | 2.00   | 3.5       | 1.95     | 1.6       | 1.95      | 1.6       | 2.00   | 3.5          | 2.1        | 8.0                | 1    | 3.0              |
|                   | -      |           |            | -           |             |         |  |           |   | -      |                 | -         |                   | 2    | 2.5                    | 30        | 2.0    | 3.5       | 2.00     | 3.5       | 1.95      | 1.6       | 200    | 3.5          | 2.1        | 8.0                | 2    |                  |
| NC                | -      |           |            |             |             |         | -  |           |   |        |                 |           |                   | 8    | 2.55                   | 33        | 1.95   | 1.6       | 2.00     | 3.5       | 1.96      | 1.6       | 200    | 3.5          | 2.1        | 8.0                | 3 6  |                  |
| 11                | 5      |           |            |             |             |         |  |           |   |        |                 | -         |                   | 4    | 2.65                   | 39        | 1.95   | 1.6       | 1.95     | 1.6       | 1.93      | 1.6       | 2.00   | 3.5          | 2.1        | 8.0                | 4    |                  |
|                   | -      |           |            |             | -           |         |  |           |   | -      | -               |           |                   | 5    | 2.75                   | 45        | 2.00   | 3.5       | 1.95     | 1.6       | 1.95      | 1.6       | 2.00   | 3.5          | 2.1        | 8.0                | 5    |                  |
| Arge              | 7      |           |            |             | -           |         |  |           |   |        |                 | -         |                   | 0    | 3.1                    | 67        | 2.00   | 3.5       | 1.95     | 1.6       | 1.95      | 1.6       | 2.00   | 3.5          | 2.1        | 8.0                | 6    |                  |
| Unich             | -      |           |            |             |             |         |  | -         | -   | 4      |                 | 1.        |                   | 7    | 295                    | 51        | 2.00   | 3.5       | 1.95     | 1.6       | 2.00      | 3.5       | 200    | 3.5          | 2.1        | 8.0                | 7    | the de la contra |
|                   | 9      |           |            |             |             |         | -  |           |   |        |                 | -         |                   | 8    | 2.0                    | 40        | 2.00   | 3.5       | 1.95     | 1.6       | 2.00      | 3.5       | 2.00   | 3.5          | 2./        | 8.0                | 80   | 8 8              |
|                   | 10     |           | -          |             |             |         |  |           |   |        |                 |           |                   | 9    | 20                     | 40        | 2.00   | 3.5       | 2.02     | 4.4       | 2.00      | 3.5       | 2.00   | 3.5          | 2.1        | 0.0                | 9 -  | CILE             |
| .2.               | 11     | 14        |            |             |             |         |  | -         |   | Y      | **<br>· · · · · |           |                   | 10   | 2.9                    | 34        | 2.00   | 3.5       | 2.00     | 3,5       | 2.00      | 3.5       | 2.00   | 0.5          | 2.1        | 0.0                | 10 7 | PR 5             |
| 18-               | 12     |           | -          | -           |             | 1       |  | -         |   | 1      |                 |           |                   | 11   | 2.0                    | 40        | 2,00   | 35        | 2.00     | 3.5       | 2.00      | 3.5       | 2.00   | 3.5          | 2.1        | 8.0                | 11 2 | 3-47             |
| 7.2.              | 18     |           | 14 - m     | 11          |             |         |  | 6         |   | 4      |                 |           |                   | 12   | 3.0                    | 110       | 2.00   | 3.3       | 2.00 .   | 3.0       | 1.95      | 1.6       | 2.00   | 3.5          | 2.1        | 0.0                | 12 - | al               |
| 120               | 14     | 19.18     | 14 - 2     | •           | •           | 1 14    |  |           |   | 1. 14: | c 11            | 1.        | 10                | 18   | 816                    | 70        | 2.00   | 85        | 2.00     | 85.       | 1:90      | 1.6       | 2.00   | 3.5          | 2./        | 8.0                | 13 2 |                  |
| E. I.             | 15     | A         | 18. AL     | 14.25       | 194 A       |         |  |           | 104   | 151    | 1 12            | 10.00     | Litter a          | 11   | 8 00                   | -60       | 2.00   | 3.5       | 2.00 .   | 35        | 0.00      | 1.6       | 200    | 85           | 2.1        | 0.0                | 14 - |                  |
| 5 5               | 16     | 1.00      | stat in    |             | A           | 1. 15   |  |           |   |        | 1 4             | 1         |                   | 110  | 28                     | 18        | 2.00   | 35        | 2.00     | 9.6       | 2:00      | 5.0       | 2.00   | 3.5          | 2.1        | 0.0                | 15 1 |                  |
|                   | 17     | 1.00      | 4 5 Jako 8 | 24.         | -17 - 1     | 1.00%   |  |           |   | A.C.   | ALC: YOU        |           |                   | 16   | 200                    | . 19      | 2.00   | 3.5       | 2.00     | 3.5       | 2.1       | 3.5       | 2.00   | 8.5          | 2.1        | 0.0                | 16 - | 1 2 .            |
| · · · · · ·       | 18     | * 1.1M    | 44.204     | 8. C.       | 11114       | • 1     |  | 100       | 1.4.2   | 1 1719 |                 | Degener - | 11.139            | 11   | 26                     | 36        | 1.95   | 1.6       | 19       | 0.0       | 2.00      | 35        | 200    | 35           | 2.1        | 80                 | 17 1 | abech<br>in .    |
|                   | 19     |           |            | 1           | 1           |         | *.                                       |           | 1.14  | 191 3  | 2. N.           | 1.00      |                   | 10   | 28                     | 48.       | 195    | 1.6       | 19       | 0         | 200       | 35        | 2:00   | 35           | 01         | 80                 | 18 8 | 1 4 4            |
|                   | 20     |           | 1-121      | -           |             |         |  |           |   | . 1    | A               | 11.4      |                   | 20   | 2.5                    | 30        | 1.95   | 1.6.      | 19       | 0+        | 200       | 3.5       | 200    | :3.5         | 21         | 80                 | 19 - |                  |
|                   | 21     | in.       | 13. 31     | 12          |             | +       |  |           | 1   | 1.1    |                 |           |                   |      | 194                    | .24       | 195    | 10        | 19       | at        | 0.00      | 35        | 200    | 35           | 21         | 80                 | 20 1 | CH'N             |
| feet              | 22     | Sec. 4    | 法情况和       | A Marca     |             |         |  | - 124     | · Contractor  | 1.28   | St - a fail     | 12.       | . 1.5             | 22   | 24                     | 24        | 1.95   | 1.6       | 1.9      | 0.0       | 2.00      | 3.5.      | 2.00   | 3.5          | 01         | 80                 | 21 - | 1 A VI           |
|                   | 23     |           | The State  | + 1.96      |             |         |  | 1         | t   | 1      | 1 . AL !        | 277       | 049               | 25   | 235                    | 22        | 2.00   | 35        | 1.9      | 03        | 200       | 35        | 200    | 3.5          | 21         | 180                | 2 8  | 3-8              |
| 總統附部等             | 24     |           | 法はない       | 林田谷:        | Waters      | 12.245  | 407-0251                                 | and the   | Sources   | 143423 | 和武武和            | 消伤        | UN STATE          | 22   | 2.35                   | 122 181   | 2.00   | 3:50.     | 2:00 2   | 3.51      | 2.00      | 3.5.4     | 2:00   | 3'5          | 21         | 80                 |      | an work          |
| 3.0               | N      | 1         | REC SI     | 語           | al.,24.     | . Dr    | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 |           | 約44支  | いけに    | 第二百姓!           | 192       | きい                | 日本   | 2.3                    | 19        | 2.00   | 3.5       | 2.00 3   | 3.5       | 2.00      | 3.53      | 2.00   | 3.5          | 21         | 8.0                | an A | the die          |
| 学校を見た             | 26     | <b>拉林</b> | 海道感        | 國際          | 心白いる        | 4.1%    | 4.4                                      | 和思想       | 机制作用  | 總透     | ·=***           | mag:      | 1.12              | 100  | 2:25                   | 1/6 01    | 2:00   | 3,5%      | 2:05 :   | 5.8       | 200       | 3.5       | 2.00   | 3.5 5        | 21         | 80                 | -    |                  |
| E e A             | 27     | 語の        | ちんか        | C.          | Karan Pa    | 1.15    | 16                                       | the start | で学校が  | 100.00 | 中午の計            | A         | 1 24              | 14   | 2.2                    | 314 3     | 1:95   | 1.6%      | 2.05     | 5.8       | 2.00      | 3.5       | 2:00   | 3.5          | 21         | 80                 | 20 - | -                |
| stag              | 28     |           | 1          | 1           | 140         |         |  | -4        | 1. 11   | * 48 Q | -Y 1121         |           | 1. 1.2            | 1 25 | 2.1                    | \$8.0     | 1.95   | 1.6       | 2.00 3   | 3.5       | 2.00      | 3.5       | 2.00   | 3.5          | 2.1        | 80                 | 21   | 11.              |
| H04 ::            | 29     | * •       | ,          | 14          |             | *       |  | 10.00     |   |        |                 |           |                   | 29   | 2.1                    | . 8.0     | 1.95   | 1.6       | 1.95     | 1.6       | 2.00      | 3,5       | 2.00   | 3.5          | 21         | 80                 | S S  | a de se          |
| the the test      | 30     |           | -          |             |             |         |  |           | -   |        |                 |           |                   | 30   | 2.05                   | 5.8       | 1.95   | 16        | 1.95     | 1.6       | 2.00      | 3.5       | 2.00   | 3.5          | 2.1        | 80                 | 20   | 0.1              |
|                   | 31     |           |            |             |             |         |  |           |   | • • •  | * • •           |           |                   | 81   |                        |           | 1.95   | 1.6       |          |           | 2.00      | 3.5       | 2.05   | 5.8          |            |                    | 81   | Period           |
| Total             |        |           | 3          |             | 1           | int.    |  |           |   | 1.00   |                 | -         | 45 :              |      |                        | 1205.8    | 84     | 5.7       | 70       | 4.3       | 9         | 959       | 110    | 2.8          | 2          | 40.0               |      | 1.812.5          |
| Mean              | -      | -         |            | 3           | 1.1         | -       |  | 1 5       | 1   |        | 1 1             |           |                   |      | • . •                  | 40.27     | 2.     | 76        | 2.5      | 48        | 3.        | 09        | З.     | 57           |            | 8.0                | 11   |                  |
| Bun-off in acre   | a      |           |            | 14          |             | •       | -  | • • •     |   | 1      | - 1             | _         | .1. 11            | -    | 1.1.1                  | 2390      | . 17   | 0         | 14       | -         | 13        | 20        | 22     | 0            | 4          | 76                 | (    | ;3,600           |
| Maximum           |        | 1         | · 24+      | 2.4         |             | -       |  | 1.5       | -   |        |                 | -         |                   | -    | 1. 1                   | 112       |        | 3.5       | -        | 5.0       |           | 8.0       |        | 5.8          |            | 8.0                |      |                  |
| Minimum           |        | -         |            | -           |             | 2       |  |           |   |        |                 |           |                   | 5    |                        | 5.8       |        | 1.6       |          | 0         |           | 1.6       | 5      | .5           |            | 8.0                |      | ÷.               |

|       | Contraction of the |           |      | the second second |         |           | Oregon | , for the     | year en | ding Sept | lember | 30, 1965  | -    |      |           | Wat  | er Resourc | es Dep | artment                   |      | Ci        | Used | rating table |          |                  |       |
|-------|--------------------|-----------|------|-------------------|---------|-----------|--------|---------------|---------|-----------|--------|-----------|------|------|-----------|------|------------|--------|---------------------------|------|-----------|------|--------------|----------|------------------|-------|
| Drain | nage ar            | ca        | 1    | Square Mile       | s. Gage | staff     | gage   |               |         |           |        |           | -    | (    |           |      | Alvin A.   | West   | -                         | , Ob | server)   |      | Ga           | ge heigt | hts used to      | hundr |
|       | . 00               | TOBER     | NO   | VEMBER            | DE      | CICAGBER  | 34     | WIANT         | 70      | BRUARY    | ,      | AJICH     |      |      | PRIL      | 1    | MAY        |        | JUNE                      |      | JULY      |      | UGUST        | 523      | PTEMBER          |       |
| TAG   | Gare               | Discharge | Gage | Discharge         | Gage    | Discharge | Gage   | Discharge     | Gage    | Discharge | Gage   | Discharge | DAY  | Gage | Discharge | Gage | Discharge  | Gage   | Discharge                 | Gage | Discharge | Gare | Discharge    | Gare     | Discharge        | DAT   |
|       |                    |           |      |                   | -       |           | -      |               |         |           | 1      |           |      |      |           | 207  | 51         |        | -                         |      |           | -    |              | 1        |                  | 1     |
| 1     | -                  |           |      |                   |         |           | 1      |               | 1       |           |        |           |      |      |           | 2.02 | 46         |        |                           | 1    |           |      |              |          |                  | 2     |
| 4     |                    |           | 1    |                   |         |           | 1      | COLUMN STREET | 1       |           | 1      |           | 11   |      |           | 1.96 | 41         |        |                           |      |           |      |              |          |                  | 3     |
| 1     |                    | 7         | 1    |                   | 1       |           |        |               |         |           | 1      |           | 11   |      |           | 1.86 | 34         |        |                           |      |           |      |              |          |                  |       |
| 5     |                    |           | 1    |                   | 1       |           |        |               |         |           |        |           | 5    |      |           | 1.82 | 31         |        |                           |      |           |      |              |          | and an and a set | . 5   |
| 6     |                    |           |      | annennen          |         | homeun    |        |               |         |           |        |           | 1 6  |      |           | 1.78 | 29         |        |                           |      |           |      |              |          |                  | 6     |
| 7     |                    |           |      |                   |         |           |        |               |         |           |        |           | 7    |      |           | 1.76 | 28         |        | -                         |      |           |      |              |          |                  | 7     |
|       |                    |           |      |                   |         |           |        |               |         |           |        |           | 8    |      |           | 1.72 | 26         |        |                           | . 73 | 20.9      |      | -1           |          |                  | 8     |
|       |                    |           |      |                   |         |           |        |               |         |           |        |           | 9    |      |           | 1.70 | 25         | .86    | 1.2                       |      |           | . 66 | 0.5          |          |                  |       |
| 10    |                    |           |      |                   |         |           |        |               |         |           |        |           | 10   |      |           | 1.60 | . 20       |        |                           |      |           |      |              |          |                  | 10    |
| 11    |                    |           |      |                   |         |           |        |               | 1       |           |        |           | 11   |      |           | 158  | 16         |        |                           | 1    |           |      |              |          |                  | 11    |
| 12    |                    |           |      |                   |         |           |        |               | -       |           | 1      |           | 12   |      |           | 1.00 | 3.0        |        |                           |      |           |      |              |          |                  | 12    |
| 13    |                    |           | -    |                   |         |           | -      |               |         |           | -      |           | 13   | 236  | 97        | 1.00 | 3.0        |        |                           |      |           |      |              |          |                  | 13    |
| 14    |                    |           | -    |                   | -       |           |        |               | -       | -         |        |           | 14   |      | 1         | .90  | 2.1        | -      |                           |      |           |      |              |          | 47               | 14    |
| 15    |                    |           |      |                   |         |           | -      |               |         |           |        |           | 15   |      |           | .90  | 2.1        |        |                           |      |           |      |              | .64      | PA 03            | 15    |
| 16    |                    |           |      |                   |         |           |        | -             |         |           | 1      |           | 16   |      |           |      |            |        | -                         |      |           |      |              |          |                  | 16    |
| 17    |                    |           | 2.00 |                   |         |           |        |               | -       |           | -      |           | 17   |      |           |      |            |        |                           |      |           |      |              |          |                  | 17    |
| 18    |                    |           |      | -                 | -       |           |        |               |         |           |        |           | 18   |      | 100       |      |            |        |                           |      |           | -    |              |          |                  | 18    |
| 19    | -                  |           |      | -                 |         |           |        |               | -       |           | 1      |           | 19   | 2.92 | 109       |      |            |        |                           |      |           | -    | -            |          |                  | 19    |
| 20    |                    |           |      |                   | -       |           |        |               |         | -         | -      |           | 20   | 254  | 137       |      |            |        |                           |      |           |      |              |          |                  | 20    |
| 21    |                    |           | -    |                   | -       |           | -      |               | -       |           |        | -         | 21   | 2.56 | 141       |      |            | 1.10   | 4 51                      |      |           |      | -            |          |                  | 21    |
| 22    | -                  |           |      | -                 | -       |           |        |               | -       |           |        |           | 22   | 2.56 | 141       |      |            | 1.18   | - 2.4                     |      |           | -    |              | ·        |                  | 22    |
| 23    | -                  |           |      | 1 1               |         |           |        |               |         |           |        |           | 23   | 2,24 | 127       |      | -          |        |                           | -    |           |      |              |          |                  | - 23  |
| 24    | -                  |           | -    | -                 | -       |           |        |               | -       |           | 1-     |           | 24   | 6.56 | 121       | 124  | 2 00       | -      |                           |      |           | -    |              | -        |                  | 26    |
| 25    |                    |           |      |                   |         |           |        |               |         | -++       | 1      | -         | 25   | 2.26 | 10        | 1.34 | 9,5        | -      | -                         |      | 8 7       |      |              |          |                  | - 25  |
| 26    | -                  | -         | -    | -                 | -       |           | -      |               | -       |           | -      |           | 26   | 201  | 2 71      |      |            | -      |                           | . 60 | - 13      |      | -            |          | -                | - 26  |
| 27    | -                  |           | -    |                   |         |           |        |               |         |           | 1.     |           | 27   | 211  | 67        |      |            |        | A CONTRACTOR OF THE OWNER |      |           |      |              | -        |                  | 27    |
| 28    | -                  |           | -    |                   | -       |           | -      |               |         |           | 1      |           | 28   | 210  | 54        |      |            | -      |                           |      | *         | -    |              |          |                  | - 28  |
| 29    | -                  |           | -    |                   |         |           | 1      | 1.            |         |           | -      |           | - 29 | 2.04 | 53        | -    |            | -      |                           |      |           |      |              | -        |                  | - 29  |
| 30    | -                  |           | -    | -                 |         |           | -      |               |         |           | -      |           | - 30 | 2.07 |           |      |            |        |                           |      |           | 1    |              |          |                  | - 30  |
| 31    | -                  | -         |      |                   |         |           |        | .1            |         |           |        |           | - 31 | 10   |           |      |            |        |                           |      |           |      |              |          |                  | 318   |
| 1     | TOTAL              |           | -    | -                 |         |           |        | -             | -       |           | +      |           | H    | Id   | BC        | 366  |            | 6      | . 6                       | 1.   | 2         |      | .5           |          | .3               | -     |
| Me    | cond-feet          | -         |      |                   |         |           |        |               |         |           |        |           |      | 1    |           |      |            | -      |                           | -    |           |      |              |          |                  |       |
| Ru    | m-off in           |           |      |                   |         |           |        |               |         |           |        | -         |      |      |           |      |            | 10     |                           |      |           |      |              |          |                  |       |

| in C | Lubic F   | eet per See    | cond, of | (                     |        | KOCK (    | Oregon | , for the y | ear en                | ding Sept | ;<br>ember | 30, 1973   | -    | 191/1                | Jaris     | Wat  | OF ST        | ATE I | ENGINE    | ER    |           | Used | rating table          |  | File NO.        |        |            |
|------|-----------|----------------|----------|-----------------------|--------|-----------|--------|-------------|-----------------------|-----------|------------|--|------|----------------------|-----------|------|--------------|-------|-----------|-------|-----------|------|-----------------------|--|-----------------|--------|------------|
| Drai | nare ar   | 483            |          | Square Mile           | . Gare |           | staff  | gage        |                       |           |            |  | 1    | (                    | pi        |      |              |       |           | Obse  | rver)     |      | G                     | ge heigh   | ts used to h    | undred | iths.      |
|      |           | -              | NO       | WENDER.               | DI     | THEFT     | 1      | MILANY      |                       | BUARY     | Γ.         | ABON   | T    |                      | PRIL      | 1    | MAY          |       | JUNE      | ,     | ULY       |      | UCUST                 | SEP  | TEMBER          |        | the second |
|      |           | TOBLK          | 1        | TEADER                |        | LADEN     |        |             |                       |           | -          | I  | -    |                      |           |      | 1            | -     |           |       |           |      |                       |  |                 |        | £          |
| DAY  | Gare      | Discharge      | Gare     | Discharge             | Gage   | Discharge | Gage   | Discharge   | Gage                  | Discharge | Gage       | Discharge  | DAY  | Gage                 | Discharge | Gare | Discharge    | Gage  | Discharge | Gage  | Discharge | Gate | Discharge             | Gage   | Discharge       | M      | n l        |
|      |           |                |          | -                     |        | -         |        |             |                       |           |            |  | -    |                      | -         | -    |              | -     |           |       | -         | 010  | 1                     | 1  | -               | H-     | -          |
| 1    |           |                |          |                       |        |           | -      |             | mirmus                |           |            |  | - 1  |                      |           |      | *****        |       |           | 0.50  | 9 03      | 0.00 | 1 0.9                 | 5.57   | 0.4             | 1      | 1          |
| 2    |           |                |          |                       |        |           |        |             |                       |           |            |  | - 2  | -                    |           |      |              |       |           | 20    |           | 1.00 | 4                     | - 57   | 1 .4            | 2 -    | -          |
| 3    |           |                |          |                       |        |           |        |             |                       |           | -          |  | - 3  |                      |           |      |              |       |           | 1207  | 7 - 7     | 10   | 4                     |  | -4              | 3 1    | É .        |
| 4    |           |                |          |                       |        |           |        |             |                       |           |            |  | - 4  |                      |           |      |              |       |           | .205  | 1 2       | 100  | .4                    | 60   | -4              | 9-     | -          |
| 5    | -         |                | -        |                       |        | -         |        |             |                       |           | -          |  | 5    | -                    |           |      |              |       |           | 730   | 1.4       | .60  | .4                    |  | .4              | 1 3    | 1          |
| 6    |           |                |          |                       |        |           |        |             |                       |           |            |  | - 6  |                      |           |      |              |       |           | 130   |           | 17   | -4                    |  | .4              | 97     |            |
| 7    |           |                |          |                       |        |           |        |             |                       |           |            |  | - 7  |                      |           |      |              |       |           | .005  | 2 2       | :02  | 100                   |  | 4               | 7_     | -          |
| 8    |           |                |          |                       |        |           |        |             |                       |           |            |  | - 8  |                      |           |      |              |       |           | .005  | 3 .6      | 10%  |                       | - 20   | 4               | 8 5    | Q.         |
| 9    |           |                |          |                       |        |           |        |             |                       |           |            |  | . 9  |                      |           |      |              |       |           | .80   |           | He.  | 1.6                   | 125  | 4               | 9 2    | 12         |
| 10   |           |                |          | 1                     | -      |           | -      |             | -                     |           | -          | -  | 10   |                      | -         |      |              |       |           | .30   | 1.4       | .62  | 4.                    | .28  | .4              | 10 1   | 1          |
| 11   | -         | -              | -        |                       | -      |           |        |             |                       |           |            |  | - 11 |                      |           |      |              |       | A         | .50   | 3 .2      | -62  | .6                    | 258  | 4               | 11 F   | N          |
| 12   | · ·       |                |          |                       |        |           |        |             |                       |           | 1          |  | 12   |                      |           |      |              |       |           | _50%  | -Z.       | 67   | .6                    | -58  | 4               | 12 3   |            |
| 13   |           |                |          |                       | -      | -         |        |             |                       |           | 1          |  | 13   |                      |           |      |              |       |           | .50   | .Z,       | .62  | 6                     | -5B  | A               | 15 4   |            |
| 1    | 1         |                | -        |                       |        |           |        |             |                       |           | +          |  | 14   |                      |           |      |              |       |           | .50   | .2        | 67   | 16                    | .58  | A               | 14 F   |            |
| 15   |           |                |          |                       |        |           | -      | -           | -                     |           | 1          | -  | 15   |                      |           |      | . 41         |       |           | .50-0 | 1.2.      | 52   | 80 .6                 | .58  | A               | 15 6   | - 1        |
| 16   |           |                |          |                       |        |           |        |             |                       |           | 11-        |  | 16   |                      |           |      | in which the |       | -         | .50   | 5 .Z      | .62  | a .6                  | .58  | 1               | 16 +   | Ez         |
| 17   | 1 2 -     | 1. 1. 1. 1. 1. | 1057     | 4                     |        |           |        | - : 155 -   | 1234                  |           | 1          |  | 17   |                      |           | -    |              | 260   | NZ 20     | ,50 1 | . 2       | 62   | 1.6                   | :58  | 4               | 17     | the state  |
| 18   |           |                | -        |                       |        |           |        |             |                       |           | 1          |  | 18   |                      |           |      |              | .60   | AZ 20     | .60 t | 11-1.6    | .62  | .6                    | .58  | A               | 18     | 4          |
| 19   | -         |                |          |                       |        |           |        |             |                       | 1.1.      | 1          |  | 19   |                      |           |      |              | .60   | 20        | .60   | 5 .4      | .67  | 6                     | .58  | A               | 19 6   | 0          |
| 20   |           |                |          |                       |        |           |        | -           | -                     | -         | 1          |  | 20   |                      |           |      |              | .60   | 20        | 60 -  | 4.6       | .62  | .6                    | ,58,   | 7. 14           | 20 2   | 10         |
| 21   |           |                |          |                       | -      |           |        |             | -                     |           | 1          |  | 21   |                      | -         |      |              | .60   | 12 2.0    | .60   | -6        | .62  | 6                     |  |                 | 21 2   | 0          |
| 22   |           |                |          |                       | -      |           | -      |             |                       |           | 1          |  | _ 22 |                      | -         |      |              | .60   | #1 1.5    | .60   | 6_6       | .62  | 6                     |  | -               | 22 6   | (A)        |
| 123  |           |                |          |                       |        | -         | -      |             | -                     |           | 1          |  | 23   |                      | -         |      |              | 60    | 1.5       | 60    | 7.5       | _62  | 6                     |  |                 | 22 ]   |            |
| 24   |           |                |          | -                     | -      |           |        |             |                       |           |            |  | - 24 |                      |           | -    |              | .62   | 1.5       | .60   | 1 :5      | .62  | 1.6                   | .56  | 7 .3            | 24     |            |
| 25   |           |                |          |                       |        |           | 1      |             | -                     |           |            |  | 25   |                      |           |      |              | .52   | tel 15    | 60    | 1.5       | .62. | et its                |  |                 | 25 F   |            |
|      | 1         | 1. 1. 1. 1.    |          | 14                    | 10.    |           | 1      | 1.1.1       | 2242                  | 24.3      | 1.         | \$5  | 28   |                      |           |      | 1            | .50   |           | .60-  | 1 5       | 10   | 5                     |  |                 | 20 6   |            |
| 1.   |           | . *            |          | 1                     |        |           |        |             | 1 W .A                |           | 11-        | 12   | 27   |                      |           | -    |              | .50   | E. a      | .00-  | s A       | .59  | 4                     |  |                 | 27 .   |            |
| 1.   |           |                | -        | 1                     |        |           |        |             | 1.1                   |           | 1          | 1 1  | 28   |                      |           |      |              | 50    | 23        | .201- | S A       | 59   | .4                    | i  |                 | 20     | 18         |
| -    |           |                | 1        |                       |        |           | 1      |             | 12363                 | 2         | 1          |  | 29   |                      | 4         |      |              | -50   |           | 61    | 8 .5      | .59  | .4                    |  | 1               | 29 6   | 0          |
| -    |           |                |          |                       |        | -         | -      |             |                       |           | 1          |  | 30   |                      |           |      |              | .50   | 401 .3    | ,60   | .4        | ,59  | 4                     |  | -               | 30     |            |
| 1.   |           |                |          |                       |        |           | -      |             |                       |           |            |  | 31   |                      |           | -    |              |       |           | .60   | 5 .7      | ,59  | 1 4                   |  |                 | 31 80  | INT        |
| -    | TOTAL     |                |          |                       |        |           |        |             |                       |           |            |  |      |                      |           |      |              |       |           |       |           |      |                       |  |                 |        |            |
| +    |           |                |          |                       |        |           |        |             |                       |           | 1:         |  |      |                      |           |      |              |       |           |       |           |      |                       |  |                 |        |            |
| - 14 | ean       |                | 1-       |                       | 1      |           |        |             | -                     |           | 1          |  |      |                      |           |      |              |       |           |       |           |      |                       | -  |                 |        | -          |
| -1   | per et. m |                | 1        |                       |        |           |        |             | 1                     |           |            |  | T    |                      |           |      |              |       |           |       |           |      |                       |  |                 |        |            |
| -17  | loches _  |                | -        |                       |        |           |        |             |                       |           | 1-         |  | 1    |                      |           |      |              |       |           |       | -         |      |                       |  |                 | YUI    | DIT        |
| 1    | A LANG    |                |          | and the second second |        |           |        |             | And Address of Street |           | -          | And other Designation of the local division of the local divisiono | -    | A COLUMN TO A COLUMN |           |      |              |       |           |       |           |      | and the second second | A DESCRIPTION OF THE OWNER OWNER OF THE OWNER OWNER OF THE OWNER OWNE | A DECK OF THE R | LUA-   | DII        |

Daily Gage Height, in Feet, and Discharge, in Cubic Feet per Second, of

No Bate STATE OF OREGON No. RCCOR OFFICE OF STATE ENGINEER Water Resources Department Oregon, for the year ending September 30, 19\_

Ploie

Used rating table

West Dry Ou Case fingles

File No. 14-0474.9

|     | 00      | TOBER       | NO     | THEFT      | DE   | THEFT     | JAL  | NUARY     | 1 12  | BRUARY    |          | ARCH     |      |        | APRIL     |      | MAY       | 1 3   | JUNE      |       | ULY       |      | UGUST     | 803  | TEMBER    |      | 2         |
|-----|---------|-------------|--------|------------|------|-----------|------|-----------|-------|-----------|----------|----------|------|--------|-----------|------|-----------|-------|-----------|-------|-----------|------|-----------|------|-----------|------|-----------|
| DAY | Gare    | Discharge   | Gage   | Discharge  | Gare | Discharge | Gare | Discharge | Gage  | Discharge | Gare     | Discharg | AVC  | Gage   | Discharge | Gaze | Discharge | Gage  | Discharge | Gage  | Discharge | Gare | Discharge | Gage | Discharge | AVG  | 2<br>P    |
|     |         |             |        |            |      |           |      |           | 1.11  |           | inengint |          | 1    | neight |           |      |           |       | 1         |       | -         |      |           |      |           | +    | £         |
| 1   |         |             |        |            |      |           |      |           | 1.16  | 35        | 1.24     | 44       | - 1  | 1.65   | 98        |      |           | A.70  | 02 5.0    | 260   | or 0.5    | 0.70 | 30 0.3    | -    |           | 1    | 1         |
| 2   |         |             |        |            |      |           |      | *****     | 114   | 34        | 1.20     | 39       | - 2  | 1.50   | 80        |      |           | JO.   | 5.0       | _60   | 57 5      | 10   | .3        |      |           | 2    | 2         |
| 3   |         |             |        |            |      |           | 110  |           | 110   |           | 1.10     | 30       | - 3  | 1.50   | - 80      |      |           | .12   | 6.0       | 160   | 28 .4     | 110  | 1.3       |      |           | 3    | E         |
| 4   |         |             |        |            |      |           | 110  | 30        | 1.00  | 28        | 1.10     |          | - 4  | 1.00   | 98        |      |           | .14   | 7.0       | -10   | 51 1.2    | -10  | 20 3      |      |           | 4    | -         |
| 2   |         |             |        |            |      |           | 110  | 30        | 1 An  | 11        | 101      |          | - 5  | 1.00   | 114       | 199  | 2 21      | 10    | 5.0       | 10    | 07 1.5    | 10   | 17 .4     |      |           | 1 9  | 3         |
| 6   |         |             |        |            |      |           | 110  | 30        | an an | 11.       | 109      | 25       | - 0  | 020    | 201       | 410  |           | 100   | 7.0       | 70    | 10 1.0    | 10   | 1 1       |      |           | G    | Bus       |
| -   |         |             |        |            |      |           | 1.20 | 20        | 95    | 1/2       | 100      |          | - 7  | 200    | 212       |      |           | 15    | 1 20      | 70    | 10 1.0    | .10  | 1 1       |      |           | 7    |           |
| °   |         |             |        |            |      |           | 1.90 | 114       | 1.06  | 77        | 108      |          | - "  | 27     | 307       |      |           | 01    | 1 20      | -1/0  | 11 4      | 70   | 1 1       |      |           |      | 1 miles   |
| 10  |         |             |        |            |      |           | 1.70 | 118       | 1.01  | 25        | 1.0      | 20       | 1.   | 2.33   | 307       |      |           | 15    | 125       | -15   | 0 9       | 74   | 10 11     |      |           | 1.1  | - 11      |
|     | 1       |             | 1      |            |      |           | 1.51 | RA        | 1.00  | 75        | :110     | - 30     | - 10 | an     | -21       |      | 314       | 45    | 25        | 70    | 4 9       | -10  | 18 .4     |      |           | 10   | 1         |
|     |         |             |        |            |      |           | 1.50 | 80        | 1.00  | 25        | 1.10     |          | -1"  |        |           |      |           | in    | 20        | 70    | a 8       | -10  | 1 7       |      |           | 11   | -         |
| ,   |         |             |        |            |      |           | 1.40 | 64        | 1.04  | 25        | 1.15     | 28       | 1.   |        |           |      |           | 67    | 1.0       | 70    | 7 8       | .70  | A         | -    |           | 12   | 1         |
|     |         |             |        |            |      |           | 1.30 | 51        | 1.03  | 28        | 1.16     | 35       |      |        |           |      |           | .64   | 2.0       | 70    | 4 7       | .70  | 4         |      |           | 11   | 2         |
| 5   |         |             |        |            |      |           | 17.8 | 49        | 1.40  | 30        | 1.20     | 39       | 15   |        |           |      |           | 15    | 40        | 70    | 4 7       | 70   | 11 4      |      |           | 14   | ES        |
|     |         |             | 1      | And Street |      |           | 230  | 780       | 1.10  | 30        | 1,70     | 39       | 1.   |        |           |      |           | .60   | .9        | .70   | 14        | TA   | 17 5      |      |           | 15-  | 1.        |
| 7   |         | 1999 C      | 100 CV | 1 - F      | -    |           | 250  | 470       | Y.m   | 30        | 174      | 44       | 17   | 1.     |           |      |           | (A)   | 9         | 704   | 0 6       | -70  | 1 5       |      | -         | 16   | the state |
|     |         |             |        |            |      |           | 2.40 | 314       | 1.26  | 46        | 1.62     | 102      | 18   |        |           |      |           | .60   | 9         | .70   | 6 6       | 70   | 5         |      |           | 17   | P A       |
|     |         |             |        |            | -    |           | 2.10 | 218       | 1.22  | 44        | 2.58     | 380      | 19   |        |           |      |           | ,60   | 9         | .70 - | 16 6      | .70  | 5         | 0/2  | 16 0.2    | 1.1- | -         |
| 0   |         |             | *      |            |      |           | 1.50 | 140       | 1.24  | 44        | 204      | 201      | 20   |        |           |      |           | .60   | .9        | .25   | 7 4       | .70  | .5        | 62   | 2         |      | Line I    |
| 1   |         |             |        |            |      |           | 1.50 | 80        | 1.18  | 37        | 1.85     | 159      | 21   |        |           |      |           | .60   | 12 9      | 18    | 7 4       | .70  | 17 5      | .67  | 2         |      | ++        |
| 2   |         |             |        |            |      |           | 1.40 | 64        | 1.10  | 30        | 1.70     | 118      | 12   |        |           |      |           | .61   | 2 19      | .68   | \$ .3     | .70  | 16 .6     | .62  | 7         |      | N         |
| 3   |         | 1. 1. 1. 1. |        |            | 0.50 | 5         | 1.40 | 64        | 1.14  | 1:34      | 1.70     | 118      | 23   |        |           |      |           | .60   | 8. I      | 65    | \$ .3     | .70  | 16 .6     | 62   | .2        |      | 2 2       |
|     |         | an mark     |        | -          |      |           | 1.34 | 56        | 1.10  | 30        | 150      | 80       | 14   |        |           | 1.D  | I .2      | .60   | 13 18     | .68   | 1.3       | :18  | ic A      | .62  | ,z        |      | 1         |
| 5   |         |             | 256    | 5. 29      |      |           | 124  | 44        | 1.13  | 3.133     | 1.90     | 164      | 25   |        |           | .50  | .2        | .607  | 4. 7      | 13    | 4.3       | 96   | 11        | 62   | .2        |      | 1         |
| 8   | -       |             | 100    | 1.1.       | 1    |           | 124  | 44.       | 118   | 37        | 7.70     | 118      | 28   |        |           | .50  | .2        | .60   | 4 .7      | 168   | 2 ,2      | .90  | 8.0       | ,62  | .2        | 1    | E         |
| 7   |         |             |        |            |      | 120       | 1.4  | 38        | 1.28  | 49        | 1.68     | 114      | 27   |        |           | .70  | 4.5       | 1600  | 5.6       | THE   | 3         | 188  | 17.0      | .62  | .2        |      |           |
|     | 060     | A 0.4       |        |            |      |           | 1.18 | 37        | 1.30  | 51        | 140      | . 98     | 28   |        |           | 68   | 3.5       | .60   | 5.6       | .65   | .2        | .84  | 6 50      | -63  | .Z.       | -    |           |
| i   |         |             |        |            |      |           | 1.18 | 37        | 1:40  | _64       | 1.50     | 91       | 29   |        |           | .70- | 3 4.5     | .60 1 | 6 6       | -65   | 1 .2      |      |           | 62   | 2         | 7    | 6 0       |
|     |         |             |        |            |      |           | 1.20 |           |       |           | 140      | _64      | 30   |        |           | 1720 | z 6.0     | 60 1  | 2.6       | .70   | .3        |      |           | 62   | 5. 31     | 1    |           |
| 1   |         |             |        |            |      |           | 1.18 | 37        |       |           | 1.48     | 77       | . 31 |        |           | The  | 2 6.0     |       |           | .70   | 0 ,3      |      |           |      |           | 11   | ear       |
| T   | DTAL    | -           |        |            |      |           |      |           |       |           |          |          |      |        |           |      |           |       |           |       |           |      |           |      |           |      |           |
| -   | -       |             |        |            |      |           |      |           |       |           |          |          | -    |        |           |      |           | -     |           |       |           | -    |           |      |           | 1    |           |
| per | nd-teet |             |        |            |      |           |      |           |       |           |          |          | -    |        |           |      |           |       |           |       |           |      |           | -    |           |      |           |
| Inc | thes    |             |        |            |      |           |      |           |       |           |          |          |      |        |           |      |           |       |           |       |           | -    |           |      |           |      |           |
| ACT | eff in  | 1 march     |        |            |      |           |      |           |       |           | -        |          | -    |        | (         |      |           |       |           |       |           |      |           |      |           | EVI  | 1101      |

Rectard A70 Sec. at Jan 17 Matholican and Sec. an many days

|            |           | ne    | ar Rock     | Creek   |           | Oregor    | , for the 3    | ear er | iding Sept | ember | 30, 1965  | _    |      |                       | Wat    | er Resourc | es Dep | artment   | TPA   | Rad       | Used           | rating tabl | e        | 1           |        |
|------------|-----------|-------|-------------|---------|-----------|-----------|----------------|--------|------------|-------|-----------|------|------|-----------------------|--------|------------|--------|-----------|-------|-----------|----------------|-------------|----------|-------------|--------|
| Drainage ( | Irea      |       | Square Mile | s. Gage | stat      | Cf_gag    | 70             |        |            |       |           |      | (    | C                     | harles | P. Mars    | cel    | -         | , Obr | erver)    |                | Ģ           | ge heigt | its used to | hundre |
|            | CTOBER    | NO    | VEMBER      | DE      | CEMBER    | 31        | NUARY          | TE     | BRUARY     | 1     | MARCIE    | T    |      | IMIL                  |        | MAY        |        | JUNE      |       | JULY      |                | UGUST       | 523      | TEMBER      |        |
| AVG Migh   | Discharge | Gage  | Discharge   | Gage    | Discharge | Gase      | Discharge      | Gage   | Discharge  | Gage  | Discharge | AAd  | Gage | Discharge             | Gage   | Discharge  | Gage   | Discharge | Gage  | Discharge | Gage           | Discharge   | Gage     | Discharge   | DAY    |
| 1          |           |       |             |         |           |           | 1              |        |            |       |           | 1    |      |                       | 1.54   | 38         | 0.88   | 5.0       | 0.60  | 0.1       |                | 0           | 0.65     | -A 0.2      |        |
| 2          |           |       |             |         |           |           |                |        |            |       |           |      |      |                       | 1.54   | 38         | . 76   | 2.0       | . 54  | 0         |                | 0           | .65      | 1 .2        | 2      |
| 3          |           |       |             |         |           |           |                |        |            |       |           |      |      | and the second second | 1.56   | 39         | . 72   | 1.1       |       | 0         |                | 0           | 65       | .2          | 3      |
| 4          | -         |       |             |         |           |           |                |        |            | -     |           |      |      |                       |        | a 36       |        | a 2.2     | 54    | 0         |                | 0           | .65      | 12          | 1      |
| 5          | -         |       |             |         |           |           |                |        |            |       |           |      |      |                       | 1.48   | 33         | .82    | 3.4       | .42   | 0         |                | 0           | 56       | ,0          | 5      |
| 6          |           | -     |             |         |           |           |                |        |            |       |           | - 0  |      |                       | 1.40   | 27         | . 68   | .5        | .60   |           |                | 0           | 56       | 0           | 6      |
| 7          |           | -     |             | -       |           |           |                |        |            |       |           | - 7  |      |                       | 1.42   | 28         | . 60   | ./        | AO    | 0         |                | 0           | 56       | .0          | 7      |
| 8          | -         |       |             | -       |           |           |                |        |            |       | -         | - 1  |      |                       | 1.40   | 27         | . 64   | J. 3      | 42    | 0         |                | 0           | ,56      | 0           | 8      |
| 9          | -         |       |             |         |           |           |                |        |            |       |           | - 1  |      |                       | 1.30   | 21         | . 68   | .5        | A6    | 0         |                | 0           | 154      | 0           | 0      |
| 10         |           | -     |             | -       |           |           |                |        |            | -     |           | - 10 |      |                       | 1.28   | 20         | . 68   | .5        | 92    | 0         |                | 0           | 36       | 0           | 10     |
| 11         | -         | -     |             | 1.000   |           | Constants |                |        |            |       |           | - 11 |      |                       | 1.28   | 20         | .66    | .4        |       | 0         |                | 0           | 36       | 0           | 11     |
| 12         |           |       |             |         |           |           |                |        |            |       |           | - 12 |      | V 101                 | 1.20   | 16         | ,00    | .5        | 1000  | 0         |                | 0           | 39       | 0           | 12     |
| 13         | -         |       |             | -       | -         | 1000000   |                |        |            |       |           | - 13 | 2.00 | 101                   | 1.18   | 10         | .10    | -6        |       | 0         |                | 0           | 34       | 0           | 13     |
| 14         |           | -     |             | -       |           |           |                |        |            |       |           | - 14 |      |                       | 1.10   | 16         | 70     | .6        |       | 0         |                | 0           | .57      | 0           | 14     |
| 15         |           |       |             |         |           |           |                | -      |            |       |           | - 15 |      |                       | 1.00   | 7.0        | 70     | .0        | -     | 0         |                | 0           | .30      | 10          | 15     |
| 16         |           | 10.00 |             | -       | -         | -         | 1 L.           | 2      |            | •     |           | 16   |      | -                     | 90     | 83         | 158    | AI        |       | 0         |                | 0           | 20       | 0           | 16     |
| 17         |           |       |             | 141     |           |           | -112           |        |            |       | -         | - 17 |      |                       | 1.07   | 9.7        | 1.36   | 25        |       | 0         | and the second | 0           | 56       | 0           | 17     |
| 18         |           |       | - 17 (F)    |         | -         |           |                |        |            | 10    |           | 10   | 2.07 | 116.                  | 1.04   | 10         | 1.24   | 18        |       | 0         |                | 0           | 62       | 1           | 16     |
|            |           |       |             |         |           |           |                |        | -          |       |           | 20   | 208  | 119                   | 1.06   | 11         | 1.20   | 16        |       | 0         |                | 0           | .54      | 0           | 10     |
|            |           | -     |             |         |           |           |                |        |            |       |           | 1,1  | 2.00 | 101                   | 1.14   | 14         | .98    | 8.3       |       | 0         |                | 0           | .54      | 0           | -      |
|            |           |       |             |         |           |           |                | -      |            |       |           | 22   | 2.12 | 128                   | 1.18   | . 16       | . 82   | 3.4       |       | 0         | 922            | 148         | : 52     | 0           |        |
| 23         |           |       |             |         | 1.4       |           | 1 1            | + + -  |            |       |           | 23   | 2.02 | 105                   | 1.24   | 18         | . 60   | ./        |       | 0         | -              | 1 128       | 54       | 0           |        |
| 24         |           |       |             |         |           |           |                |        |            |       |           | 24   |      | a 98                  | 1.16   | 15         | . 58   | .1        |       | 0         | .90            | 1 4.7       | .56      | 0           | 24     |
| 25         |           |       |             |         |           |           |                | - 94.2 | 1 m m      |       |           | 15   | 1.94 | 90                    | 1.12   | 3. 13      | . 46   | 0         | -     | 0         | .94            | 5.8         | 54       | 0           | 25     |
| 26         | *         | -     |             | 1.0     | -         |           |                | 1      |            |       |           | 26   | 1.86 | 76                    | 1.10   | 17.        | .68    | .5        |       | 0         | 88             | 4.2         | :60      | 1           | 26     |
| 27         | -         |       | -           |         |           |           |                |        |            |       |           | 27   | 1.80 | 67                    | 1.00   | 9.0        | .68    | .5        | 1.28  | .20       | 68             | A           | ,62      | :I:         | 27     |
| 28         |           |       |             |         |           |           |                |        |            | 1     |           | 28   | 1.74 | 59                    | .94    | 6.9        | . 64   | .3        | 88    | 5.0       | .56            | 0."         | .66      | 51          | 28     |
| 29         |           | -     |             |         | -         |           |                |        |            |       |           | 29   | 1.60 | 43                    | .74    | 1.5        | .62    | .2        | .70   | 6         | .60            | -1          | :64      | 1Z          | 29     |
| 30         |           |       |             |         |           |           |                | •••    |            | -     |           | _ 30 | 1.58 | 91                    |        | a 2.7      | 3      | 0         | .58   | .1        | .56            | 0           | .62      | 1. 1.       | 30 P   |
| 31         |           |       | ••••        | -       |           | -         |                | •••    | ••••       | -     | 2         | 31   |      | ••••                  | _84    | 3.9        | •••    | ••••      |       | d         | .64            | 23 0        |          |             | 31 Y   |
| TOTAL      |           |       |             |         |           |           |                |        |            | 1     |           | +    |      |                       | -      | 539.6      |        | 132.3     |       | 25.9      |                | 291.2       |          | 1.6         |        |
| Mean       |           |       |             |         |           |           |                |        |            |       |           | 1    |      |                       |        | 17.4       |        | 4.41      |       | 0,84      |                | 9.39        |          | .053        |        |
| Second-fe  | et        |       |             |         | -         |           |                |        |            |       |           | -    |      |                       |        |            |        |           |       |           |                |             |          |             |        |
| Run-off is |           | 1     |             |         |           |           | and the second |        |            |       |           |      |      |                       |        |            | -      |           |       |           |                |             | -        |             |        |

| Drain | LASC AD    | ca          |       | Square Mile | L Gage | •         | 1    |           | 1     |  | -    |           | -    | (        |           | 1    |           | 1    |           | , Ob | server)   | 1    |          | Gage he | ights used to | hundre | 6       |
|-------|------------|-------------|-------|-------------|--------|-----------|------|-----------|-------|--|------|-----------|------|----------|-----------|------|-----------|------|-----------|------|-----------|------|----------|---------|---------------|--------|---------|
|       | 00         | TOBER       | NON   | VEMBER      | DE     | CENER     | 34   | NUARY     | -     | BRUARY   | 1    | KARCH     |      |          | PRIL      |      | MAY       | -    | JUNE      | -    | JOLY      | -    | lucust   |         | EPTEMBER      | - +    | Tour    |
| DAI   | Gage       | Discharge   | Gage  | Discharge   | Gage   | Discharge | Gare | Discharge | Gage  | Discharge  | Gage | Discharge | IVG  | Gage     | Discharge | Gare | Discharge | Gage | Discharge | Gare | Discharge | Gare | Dischars | te Gag  | ht Discharg   | DA     | PIC     |
| 1     |            |             |       |             |        |           |      |           |       |  | -    |           | - 1  |          |           |      |           |      |           | 0.98 | 19 0.9    | 0.99 | 10 0.    | 41.0    | 47 0.         | 5 1    | Percent |
| 2     |            |             |       |             |        |           |      |           |       |  |      |           | 2    |          |           |      |           |      |           | -20  | 9         | -90  | 100      | 1.10    | 1 .0          |        | -       |
| 3     |            |             |       |             |        |           | 1    |           |       |  |      |           | 13   |          |           |      |           |      |           | 96   | 104 8     | a    | 00       | 4 10    | 1 1 1         |        | E.      |
| 5     |            |             |       |             |        |           | 1    |           |       |  | 1    |           | 5    |          |           |      |           |      |           |      |           | 98   | al .     | 3       | 1             | 5      |         |
| 6     |            |             |       |             |        |           |      |           |       |  |      |           |      |          |           |      |           |      |           |      |           | .98  | 1        | 3       |               | 6      | arter   |
| 7     |            |             |       |             | -      |           | -    |           | -     |  | 1    |           | 7    |          |           |      |           |      |           | .98  | +04 .9    | .97  | 1 .      | 3       | -             | 7      | á       |
| 8     |            |             |       |             |        |           | 1    |           |       |  | ļ    |           |      |          |           |      |           |      |           |      | .9        | .98  | 1        | 3 10    | 3-08          | 1 .    | 5       |
| 9     |            |             |       |             | -      |           |      |           |       |  | -    |           | 9    |          |           |      |           |      |           | .98  | 104 .9    | .99  | of a     | 4 1.00  | 21            | - 9    | Ł       |
| 10    |            |             |       |             |        |           | -    |           | -     |  | -    |           | 10   | -        |           |      |           |      |           | 1.58 | 17        | 1.00 | 07 -     | 9 184   | 21 -          | 10     | E       |
| 11    |            |             |       |             |        |           |      |           |       |  |      |           | - 11 |          |           |      |           |      |           | 1.24 | _ 5.7     | 1.02 |          | 5 8     | 6 .           | _ 11   | £       |
| 12    |            |             |       |             |        |           |      |           | 1     |  | 1    |           | 12   |          |           |      |           |      |           | 126  | 1 20      | 100  |          | 6 00    | 51            | - 12   | tend    |
| 13    |            |             |       |             |        |           |      |           | -     |  | 1    |           | 13   |          |           |      |           |      |           | 614  | 01 -50    | 1.01 | 0        | 20      | 2222          | - "-   | 4       |
| 14    | 100        |             | -     |             | 1      |           |      |           | 1     |  | 1    | -         | 1.   |          |           |      |           |      |           | 1.0  | 13        | LAD  | 4        | 3 8     | 6.7           |        | E       |
| 1.0   |            |             |       |             |        |           |      |           |       | 1.4.4  | -    |           | 1.   |          |           |      | -         | 1.00 | 10        | 1.02 | 13 .7     | 100  | 08       | 31 .8   |               | 1.     |         |
| 17    | 2000       | a service a | de la | 1           | •      |           |      |           | 1 200 | 1.15   | 1    | *         | 17   | * 33 V   |           |      |           | 102  | 1.2       | .91  | 08 .4     |      |          | 8       | 51 1          | 17     | ł       |
| 18    |            |             |       |             |        |           |      | -         |       |  | 1    |           | 18   |          |           |      |           | 1.00 | 1.0       | .92  | .2        | 1.04 | 18 .     | 6 8     | 6 1           | 18     | 8       |
| 19    |            |             | -     |             |        |           |      |           |       | · · · ·  | 15   |           | 19   | -        |           |      | here and  | 1.00 | 1.0       | .91  | sq ,2     | 1.06 | 18 1     | 7_8     |               | 19     | £       |
| 20    |            |             |       |             |        | -         | -    | -         |       |  | 1    |           | 20   | -        |           |      |           | 1.00 | 3 1.0     | -    | -         | 1.04 | 19 13    | 5 .B    | 307 1         | 1 20   | ž       |
| 21    | -          |             | -     |             |        |           |      |           |       |  |      |           | 21   |          |           |      |           |      |           | 41   | PH .2     | 1.02 | 1 -      | 4       | -             | 21     | I.      |
| 22    |            |             | 1.000 |             | 1000   |           |      |           |       |  | 17   |           | 22   |          |           |      |           | a    | ~ 9       | -94  | 1 14      | 1.04 | 1        | 2       |               | - 22   | 4       |
| 23    | 1000000000 |             |       |             |        |           |      |           |       | and the second s | 1    |           | 1    | - Terrer | -         |      |           | 98-  | 1 9       | 12   | 1 3       | in   | 07 -     | J A     | ray -         | _ 23   | I       |
| 24    |            |             |       |             |        |           | 1    |           | 1     |  | 1    |           | 115  |          | +         |      |           | 98   | 1.9       | 91   | 4         | 101  | 10       | 4       | chap          | 24     | -       |
| 2     |            |             |       | · .         |        |           |      |           |       |  | T.   | 1.1.1     | 26   |          |           |      |           | 98   | 9         | 99   | 7         | 103  | To I     | 41      |               | 17     | E       |
| 26    |            |             |       |             |        |           |      |           | 1     | 1.1.1  | 1    | 1 1       | 27   |          |           | 5    |           | .98  | 9         |      | and d     | 102  | 1        | 3       | -             | - 29-  |         |
| 28    |            | -           |       |             |        |           |      |           |       | · Anna   | 1    |           | 28   |          |           |      |           | .93  | 9         | .97  | 04. 4     | 1.03 | 4        | 1 14    | 3506 1        | 1.     | and an  |
| 29    |            |             |       | -           |        |           |      |           |       |  | 1    |           | 29   | -        |           | *    | - '       | .98  | 9         | .97  | a. 4      | 1.02 | 1        | 3 A     | 211           | 29     | å       |
| 30    |            |             |       | -           |        |           |      |           |       |  | 1    |           | 30   |          |           |      |           | ,98  | 19 .9     | 1.00 | 1.6       | 1.02 | 10 .3    | B A     | 2-06 1        | 30     |         |
| 31    | -          |             |       |             |        |           | -    |           |       |  |      |           | 31 • | ••       |           |      |           | •••  |           | 100  | 14 .6     | 104  | -09 .5   | 5       |               | 31     | ¥ea.    |
| T     | OTAL       |             |       |             |        |           |      |           |       |  |      |           |      |          |           | in   |           | 12.  | 4         | 4    | 4.2       | 12   | 1        |         | 4.5           |        |         |
|       |            |             |       |             |        |           |      |           |       |  |      |           |      |          |           |      |           |      |           |      |           |      | -        |         |               | 1      |         |

| D | rain | te area | 460    |        | Square Mile | s. Gar | sta           | Oregon<br>ff gag | , for the g  | year en | ding Sept                              | ember      | 30, 19 76 |             |           | Wat  | er Resourd | res Dep | artment   | , Ob | server)    | Used | rating table | ge heigh | its used to          | hundr |
|---|------|---------|--------|--------|-------------|--------|---------------|------------------|--|---------|--|------------|-----------|-------------|-----------|------|------------|---------|-----------|------|------------|------|--------------|----------|----------------------|-------|
| F | 4    | осто    | BER    | NON    | TEMBER      | DZ     | CINGER        | 34               | NUARY  | 170     | BRUARY                                 |            | ARCH      | T           | APRIL     | 1    | MAY        |         | JUNE      |      | JULY       |      | UGUST        | SEP      | TEMBER               |       |
| · | AV C |         | - 10.1 | Gare   | Discharge   | Gage   | Discharge     | Gare             | Discharge  | Gage    | Discharge                              | Gare       | Discharge | Gare height | Discharge | Gage | Discharge  | Gage    | Discharge | Gage | Discharge  | Gare | Discharge    | Gage     | Discharge            | AVG   |
| ŀ | -    | 1 00    | 1      |        |             |        |               | 100              | 2.17   | 1       |  |            |           |             |           | -    |            | Vad     | 47        | -    |            | -    |              |          |                      | t d   |
|   | 10   | 88-0    | 1      | 415    |             | -      |               | 1.68             | 1 80   | 200     | 46                                     | 1          |           | 1           |           | 1    |            | 1.31    | 7.2       | 1    |            |      |              |          |                      | 1 2   |
|   | ;    | 99.0    | 3      | 1      |             |        |               | 180              | 3 13   | 1       | ************************************** |            |           | 1.2.6       | 105       | 1    |            | 1.32    | 6.6       |      |            |      |              |          |                      | 3     |
|   |      |         |        |        |             |        |               |                  |  | 1.50    | 13                                     | - Stations |           |             |           |      |            | 1.37    | 8.1       |      |            |      |              |          |                      |       |
|   | 5    |         |        |        |             |        |               |                  |  |         |  | 1.86       | 34        | 5           |           |      | 07         | 1.37    | 8.1       |      |            |      |              |          |                      | 5     |
|   | 6    | .96-0   | .2     |        |             |        |               | 1                |  |         |  | 188        | 36        | 03.52       | 217       | 1.86 | 34         |         | 14/ 6     |      |            |      |              |          |                      | 6     |
|   | 7    | .96     | 2      |        |             |        |               | -                |  |         |  |            |           | 7           |           |      |            | 1.30    | - 6.0     |      |            |      |              |          |                      | 7     |
|   | 8 .  | .96     | .2     |        |             | 1      | 1 -           | 1                |  | 100     | 20                                     | 1.00       | - /       | 13.30       | 188       |      |            | 1.04    | - H.L.    |      |            | 011  | 11           |          | Contemportation St.  | 8     |
|   |      | .96     | - 2    | 1      |             | 1.68   | 3/1 5.9       |                  |  | 150     | 30                                     | 1.00       | 36        | 02.81       | 260       |      |            | 123     | 37        |      |            | 2.16 | 61           |          |                      | 0     |
|   | 10   | .96     | 12     | -      |             | -      |               |                  |  | -       |  | 1          |           | 10 3.40     | 201       |      |            | 1.20    | 3.0       |      | -          | 178  | 54           |          |                      | 10    |
|   | 11 . | 36      | 12     |        |             | 170    | 1 4           | 200              | 1 10   | 1       |  |            |           | 11 310      | 163       |      |            |         |           |      |            | 1.17 | 18           |          |                      | 11    |
|   | 12   | 36      | 2      | 1.20   | 11.5        | 110    | - 1911 - 10re | 12.50            | 1 10   | 1.70    | 23                                     | 1          |           | 11 2.10     | 100       | -    |            |         |           |      |            | 1.10 |              |          |                      | 12    |
|   | 13   | acon    | 1.2    | have   | an is       | 1      |               |                  | and the second | 1       | and the second                         | 1.9%       | 42        | 14 5,10     | 163       |      |            | 124     | 42        |      |            |      |              |          |                      | 14    |
|   | 15   | 98      | 2      | 1.34   | \$ .6       |        |               | 2.38             | 16 63  | 1.84    | .33                                    | 200        | 46        | 15          |           |      |            | 1.13    | 2.0       |      |            |      |              |          | and the state of the | 15    |
|   | 16   | 96      | .2     |        | · · · · ·   | 1.62   | 34 64         | 3.50             | on 155   | X.84    | 33                                     | 11         | 1         | 10 2.90     | 139       |      |            |         |           |      |            |      |              |          | -                    | 16    |
|   | 17   | ,981    | .2     | 1.48-5 |             | 1.65   | -9 75         | 3.78             | 2 237  | 1 11    |  | 1          |           | 17          | 1 1       | 122  | 3.6        | 1.10    | 1.5       | -    |            | 1.38 | . 8.4        |          | E                    | 17    |
|   | 18   | .96-1   | 2.2    |        |             | 1      |               | -                |  | 1       |  | 320        | 175       | 18          |           | 1.22 | 3.6        | 1.15    | 2.2       |      |            | 182  | 31           |          |                      | 18    |
|   | 19   |         | 1      |        |             |        |               | 2.86             | -19  | 216     | 61                                     | 320        | 201       | 19          |           | 129  | 3.0        |         |           |      | the second | 136  | 66           |          |                      | 19    |
|   | 20   | ,9870   | 2, 2   |        |             | -      |               | -                |  | 300     | 46                                     | 1          |           | 20          |           | 1.22 | 6.6        |         |           |      |            |      |              |          |                      | 20    |
|   | 21   | Lager,  | 3      |        |             | 1. 24  | 1. 1.         |                  |  |         |  | 270        | 115       | 21          |           |      |            | Im      | 120       |      |            |      |              |          | 1                    | 21    |
|   | 22   | 100     | 4      | 1100   | A T         | 142    | 2 11          | 201              | 71   |         |  | 2.68       | 113       | 22          |           |      |            | 171     | 12        |      |            |      |              |          |                      | 22    |
|   | 23   | 1 ng    | 5      | PATE   | 43          | 4.11   | 26            | 216              | 61   | 1.82    | .31                                    | 1          |           | 24          |           |      |            | 1.21    | 3.3       |      |            | 17/0 | 10           |          | 1940 - 1940 -        | 23    |
|   | 24   | A       | 5      | KHE    | 9           | 1.     |               | 1                | 1  | 1.84    | HH:33 .                                | 270        | 115       | 25          |           | KELS | 4.8        | 1.18    | 2.7       |      |            |      |              |          |                      | 25    |
|   |      |         |        | 11     | 11 1-       |        | • •           | 2.00             | 1 Ale  | -1:0    | 1.6%                                   | 2.70       | 115       | 28 232      | 77        | 1.50 | 13         |         |           |      |            | 142  | 9.8          | 1.000    | Set 4                | 26    |
|   | 27   |         |        |        | -           | -      |               | 1.94             | 8 4  | 2.20    | 165                                    | 2.80       | 105       | 27          |           |      |            |         |           | .94  | 16 0.4     |      |              | •        |                      | 27    |
|   | 28   | 1.11    | 1,5    | 1      |             |        |               | 1.90             | 37   | 332     | 67                                     | 3          |           | 28 2 22     | - 69      | 1.37 | 87         |         |           |      |            |      |              | -        |                      | 28    |
|   | 29   |         |        | -      |             |        |               | 1.98             | 44   |         |  | 1          | OF        | 29          | <u> </u>  | 1.37 | 8.1        |         |           |      |            |      |              |          |                      | 29    |
|   | 30   |         |        | 1.65   | # 30        |        |               | 2:08             | -22  | 1       |  | 220        | 65        | 30          |           | 13/  | 0.1        |         |           |      |            |      |              |          |                      | 30    |
|   | 31   |         | 1.6    | •••    |             |        | 01            |                  | 00.1   |         |  | 2.00       | 1.0.5     | 31          | 507       | 1.20 | 140        |         |           |      | 4          |      |              | • • •    | ••••                 | 31    |
|   | TO   | TAL     | 5.9    | 6.     | L           | 4      | 61            | 10               | 93.4   | -       | 181                                    | 12         | 23        |             | 200       | 10   | 1.3        | 44      | . 4       |      | 1          | 9    | 1.8          | -        | -                    |       |
| _ | Mean |         |        |        |             |        |               |                  |  |         |  | +          |           |             |           |      |            |         |           |      |            |      |              |          |                      | -     |
| - | per  | eq. mi  |        |        |             |        |               |                  |  |         |  | +          |           |             |           |      |            |         |           |      |            |      |              |          |                      |       |
| - | Inci | ici in  |        |        |             |        | -             |                  |  |         |  |            |           |             |           |      |            |         |           |      |            |      |              | -        |                      | -     |

|      |                          |                       |      |             |         | ·····,    | Oregon | , for the y     | ear en  | ding Sept | ember | 30, 19 65  | ·    |      | OF             | Wat           | er Resource | ATE Dep | artment   | ER   | Shur      | Used | rating table |          | /             | _        |         |
|------|--------------------------|-----------------------|------|-------------|---------|-----------|--------|-----------------|---------|-----------|-------|------------|------|------|----------------|---------------|-------------|---------|-----------|------|-----------|------|--------------|----------|---------------|----------|---------|
| Drai | inage are                |                       |      | Square Mile | s. Gage | staff     | f gage |                 | Les     | t Fla     | ng a  | 2.41 2     | . 1  | (    |                | Da            | vid R. B    | hird    |           | , Ob | server)   |      | Ga           | ge heigh | its used to l | hundre   | edu     |
|      | 00                       | TOBER                 | NOT  | TEMBER      | DEC     | CEMBER    | JA     | NUARY           | m       | RUARY     | ,     | ARCH       | T    |      | PRIL           |               | MAY         |         | JUNE      |      | JULY      | 1    | UGUST        | SZP      | TEMBER        |          | ouro,   |
| DAY  | Gare                     | Discharge             | Gage | Discharge   | Gage    | Discharge | Gare   | Discharge       | Gage    | Discharge | Gage  | Discharge  | DAY  | Gage | Discharge      | Gare          | Discharge   | Gage    | Discharge | Gage | Discharge | Gare | Discharge    | Gage     | Discharge     | TAG      | hird Te |
| -    |                          |                       |      |             |         |           | 1      |                 |         |           |       |            | -    |      |                | 1.01          | 50          | 100     | 12        |      | 1 38      |      | 1 0.8        | 1.12     | 101 15        |          | 4       |
| 1    |                          |                       |      |             |         |           |        |                 |         |           |       |            | 1    |      |                | 1. 11         | a 48        | 1.00    | a 11      | 0.78 | 3.6       | 160  | .8           | .62      | 1.5           | 1        | Secon   |
|      |                          |                       |      |             |         |           |        |                 |         |           |       |            | 1,   |      |                | 1.37          | 45          | .96     | 9.7       | .80  | 4.0       | .60  | .8           | .62      | 1.5           | 3        | E       |
| 4    |                          |                       | 1    |             |         |           |        |                 |         |           |       |            | 4    |      |                | 1.32          | 39          | . 92    | 7.9       |      | a 3.5     | .55  | .9           | .60      | ter 1.3       |          | Ę       |
| 5    |                          | and the second second |      |             |         |           |        |                 |         |           |       |            | - 5  | -    | and section in | 1.31          | 38          | . 90    | 7.0       |      | q 3.0     | - 58 | .7           |          | a 1.2         | 5        |         |
| 6    |                          |                       |      |             |         |           |        |                 |         |           |       |            | 6    |      |                | 1.30          | 37          | 73      | 2.6       | .72  | 2.4       | .56  | .5           | ,58      | tos .9        | 6        | unte    |
| 7    | -                        |                       |      |             |         |           |        |                 |         |           |       |            | 7    |      |                | 1.31          | 38          | .75     | 3.0       | .72  | 7 2.4     | 56   | .5           | 56       | 1.7           | 7        | a       |
| 8    |                          |                       |      |             |         |           |        |                 |         |           |       |            | 8    |      |                | 1.30          | 37          | . 78    | 3.6       | .7/  | 2.2       | 58   | .7           | .58      | +03 ,9        | B        | £       |
| 0    | -                        |                       |      |             |         |           |        |                 |         |           |       |            | - 9  |      |                | 100           | 9 34        | .13     | 1.4       | . 14 | 2.8       | .62  | 1.0          | 66       | 104 2.0       | P        | S.      |
| 10   | -                        |                       |      |             |         | -         |        |                 | -       |           |       |            | 10   |      |                | 128           | 30          | .16     | 1.4       | .67  | 1.9       |      | 1.6          | .66      | 2.0           | 10       | hird    |
| 11   | -                        |                       | -    |             |         |           |        |                 |         |           |       |            | - 11 |      |                | 1.20          | 29          | 16      | 3.2       | 1.   | 2.0       | 14   | 1.4          | 29       | 19            | 11       | 4       |
| 12   |                          |                       |      |             | -       |           | -      |                 |         |           |       |            | 12   | 170  | 100            | 1.10          | 22          | 72      | 24        | ·/   | 20        | 10   | 1.4          | 18       | q 1.7         | 12       | -       |
| 13   |                          |                       |      |             |         |           |        |                 | -       |           |       |            | 13   | 110  | 100            | 1.04          | 15          | 77      | 24        | 7.   | 20        | .67  | 1.0          | . 68     | 24            | 13       | ġ       |
| 14   | -                        |                       | -    |             |         |           |        |                 |         |           |       |            | 14   |      |                | 1.05          | 15          | To      | 20        | 73   | 20        | .69  | 19           | 1        | 2 27          | 14       | H       |
| 15   |                          |                       | -    | +           |         | ••        |        |                 |         |           |       | 1. A. A.   | 1.   |      |                | 1.02          | 13          | 68      | 18        | .7:  | 20        | .78  | 20           | .70      | 1 78          | 15       |         |
| 16   | 14                       | -                     |      |             |         |           |        | States therein  |         | 1         |       |            | 17   |      | 1              | 1.01          | 12          | 1.48    | 160.      | .7   | 20        | .65  | 1.4          | .18      | 2.4           | 10       | arter   |
| 1.   | -                        | 121                   |      |             |         | line .    |        |                 |         |           |       |            | 18   |      | -              | 1.            | a 12        | 1.20    | 27.       | .7   | 2.0       | .58  | .7           |          | a 24          | 18       | 8       |
| 19   |                          |                       |      |             |         | •         |        |                 |         | -         | 1     |            | 19   | 1.80 | 123            | 1.02          | 13          | 1.30    | 37        | .7   | 2.0       | .58  | .7           |          | 1 2.4         | 19       | ¢       |
| 20   | 2                        |                       |      |             |         |           |        |                 |         |           |       |            | 20   |      | a 112          | 1.12          | 20          |         | 120       | .7   | 2.0       | .60  | ,8           | .68      | M 24          | 20       | Four    |
| 21   | 1                        |                       | -    | -           |         |           |        |                 |         |           |       |            | 21   | 1.70 | 100            | 1.13          | 21          | -       | 9.15      | .71  | 2.0       | .58  | .7           | .LA      | 1.8           | 21       | 2       |
| 22   | -                        |                       | 100  |             |         | -         | -      |                 |         |           |       | -          | 22   | 1.80 | /23            | 1.11          | 19          | .94     | 8.8       |      | q 1.0     | 280  | 1290         | . 166    | 2.0           | 22       | Ē       |
| 23   |                          |                       | -    | 1           | -       |           | -      |                 |         |           |       |            | 23   | -    | 2 105          |               | a 16        | . 90    | 7.0       | ,53  | .3        | 175  | dig.         |          | 2 2.2         | 23       | T       |
| 24   | -                        |                       | -    |             | -       |           |        |                 | -       |           | -     |            | 24   | 1.61 | . 82           | 1.01          | 14          | . 90    | 7.0       | . 55 | .3        |      | 4.96 8.8     | .68      | 2.4           | 26       | ě       |
| 25   | 1                        |                       | 1.14 |             |         |           | -      |                 | 1.1.1.1 | - 144     | -     |            | 25   | 1.62 | 87             | 1.02          | 13          | . 90    | 7.0       |      | a .3      | .70  | +++ 2.8      |          | 1 2.4         | 25       | E.      |
| 26   | -                        |                       | -    | -           |         |           | -      |                 |         | 1         |       | the second | 26   | 100  | 80             | 1.01          | 12          | .90     | 7.0       | 112  | ABL.      | . 69 | 104 2.4      |          | 2.4           | 26       | -       |
| 27   | -                        | -                     |      |             |         |           | -      |                 |         |           | -     |            | 27   | 1.55 | 16             | ·a/           | 07          | 90      | 1:0       | -193 | 18.       | ~    | 4 2.4        | 168      | 124           | 27       | ŧ       |
| 28   |                          |                       | -    | • •         |         |           |        | (). () () ()    |         |           | -     |            | - 28 | 1.49 | 63             | 10            | a 10        | 80      | 40        | 21   | 15        | 18   | 24           | 168      | 1.9           | 28       | Quan    |
| 29   | -                        | -                     |      |             |         | 14 m m    |        | -               |         |           |       |            | - 29 | 1.42 | 52             | 99            | 11          | .80     | 4.0       | . 12 | 1.0       | .18  | 1 2.4        | -66      | 1 2.0         | 29       | -       |
| 30   | -                        |                       |      |             |         |           |        |                 |         |           |       |            | 31   |      |                | 100           | 12          |         |           | :61  | .9        | .00  | a 2.0        | 00       | 17.0          | 30 1     | Peri    |
| 31   |                          | -                     |      |             |         |           | -      |                 |         |           |       | 1          |      |      |                | -lastic Means | 711 7       |         | 2021      | -    | 1090      |      | 150 0        |          |               | 311      |         |
| -    | TOTAL                    |                       | -    |             |         |           | -      |                 |         |           | -     |            |      |      | -              |               | 116.1       |         | 673.4     |      | 101.7     |      | 450.0        |          | 51.6          | -        | _       |
| - 14 |                          |                       | -    |             | -       |           |        |                 |         |           |       | -          | +    |      |                |               |             |         | 2.18      |      | 3,55      |      | 14.5         | -        | 1.92          | -        | _       |
| - 50 | cond-fect<br>per sq. mi. |                       |      |             | -       |           | -      | m o Hun Harting |         |           |       | -          | +    |      | +              |               | -           | -       |           | -    |           |      |              |          |               |          |         |
| - 1  | inches                   |                       | -    |             |         |           | -      |                 |         |           |       |            | 1    |      |                |               | 1470        |         | 587       |      | 218       |      | 802          | -        |               |          | -       |
| - Ku | cre-seet .               | 1                     | 1    |             |         |           |        |                 |         |           |       |            | -    |      |                |               | 1140        |         | 201       |      | -10       |      | 010          |          | 114           | 1 Sector |         |

| -    |                |                |                           | near Co           | ndon    |           | Oregor | , for the 3    | year en | ding Sept | ember | 30, 1965  | 1      |      |           | Wat  | er Resourc | es Dep | artment   | 5.   | 1         | Used | rating table  |          |               | -         |
|------|----------------|----------------|---------------------------|-------------------|---------|-----------|--------|----------------|---------|-----------|-------|-----------|--------|------|-----------|------|------------|--------|-----------|------|-----------|------|---------------|----------|---------------|-----------|
| Dra  | inage ar       |                |                           | iquare Mile       | s. Gage | Btaff:    | gage.  | readings       |         |           |       |           |        | (    |           | ٧.   | Obristo    | phera  | n         | , Ob | server)   |      | Ga            | ge heigt | hts used to h | undr      |
| Γ    | 00             | TOBER          | NOT                       | TEMBER            | DD      | CEMBER    | 31     | NUARY          | 10      | BRUARY    | ,     | ARCH      | Π      | 4    | APRIL.    |      | MAY        |        | JUNE      |      | JULY      |      | UGUST         | 523      | TIMBER        |           |
| DAY  | Gare           | Discharge      | Gage                      | Discharge         | Gage    | Discharge | Gage   | Discharge      | Gage    | Discharge | Gage  | Discharge | DAY    | Gage | Discharge | Gare | Discharge  | Gage   | Discharge | Gage | Discharge | Gage | Discharge     | Gage     | Discharge     | DAY       |
| 1    |                |                |                           |                   |         |           | -      |                |         |           |       |           |        | _    |           | 1.98 | .55        | 1.98   | 17        | 127  | 47        | 1    |               | -        |               |           |
|      |                |                |                           |                   | 1       |           | -      |                |         |           | -     |           |        |      |           | 1.95 | 52         | 1.47   | 12        | 1.23 | 3.7       |      |               |          |               |           |
| 1:   |                |                |                           |                   |         |           | 1      |                |         |           | -     |           |        |      |           | 1.94 | 50         | 1.46   | 11        | 1.22 | 3.4       |      |               |          |               | 1 1       |
|      |                |                |                           |                   |         |           |        |                |         |           | 1     |           |        |      |           | 1.88 | 44         | 1.41   | 9.4       | 1.19 | 2.7       |      |               |          |               |           |
|      |                |                | 1                         |                   | 1       |           | -      |                |         |           |       |           | 1      |      |           | 1.88 | 44         | 1.40   | 9.0       | 1.20 | 2.9       |      |               |          |               | 5         |
|      |                |                |                           | The second second |         |           |        |                |         |           |       |           |        |      |           | 1.88 | 44         | 1.59   | 8.6       | 1.17 | 2.4       |      |               |          |               | 6         |
|      |                |                |                           |                   |         |           |        |                |         |           |       |           |        |      |           | 1.87 | 43         | 1.38   | 8.3       | 1.15 | 2.0       |      |               |          |               | 7         |
|      |                |                |                           |                   |         |           | -      | A company      |         | 1         |       |           | 1.1    |      |           | 1.82 | 38         | 1.35   | 7.2       | 1.15 | 2.0       |      | a available a |          |               |           |
|      |                |                |                           |                   |         |           |        |                |         |           |       |           |        |      | -         | 1.77 | 33         | 1.31   | 5.8       | 1.13 | 1.7       | 0.75 | 0             |          |               |           |
| 10   |                |                |                           |                   |         |           |        |                |         |           |       |           | 10     |      |           | 1.72 | 29         | 1.29.  | 5.2       | 1.10 | 1.2       |      |               |          |               | 10        |
|      |                | 1              |                           |                   |         |           |        |                |         |           |       |           | 1,1    |      |           | 1.71 | 28         | 1.29   | 5.2       | 1.11 | 1.4       |      |               |          |               | 11        |
|      |                |                |                           |                   |         |           |        |                |         | -         |       |           | 12     |      |           | 1.68 | 25         | 1.27   | . 4.7     | 1.10 | 1.Z.      | 1    |               |          |               | 12        |
| 1    |                | 1              |                           |                   |         |           |        |                |         |           |       | '         | 13     | 2:30 | 94        | 1.66 | 24         | 1.27   | 1.7       | 40   | a. 1.2    |      |               |          |               | 13        |
| 1    |                |                |                           |                   |         |           |        |                |         | . 5       |       |           | 14     |      | a 94      | 1.65 | 23         | 1.21   | 3.2       | 1.08 | 1.1       |      |               |          |               | 14        |
| 1    |                | 1              | Contraction of the second |                   |         |           |        |                | -       |           |       | •         | -15    |      | a 92      |      | a 21       | 1.22   | 3.4       | 1.05 | .9        |      |               |          |               | 15        |
| 1    |                |                |                           |                   |         | •-        | 1      | -              |         | ;         |       | * * *     | 16     |      | 9 90      | •••  | a 20       | 1.27   | 4.7       | 1.02 | .7        |      |               |          |               | 16        |
| i    |                | 2.50 3         | 1.27                      |                   |         | 1         |        |                | A.C.    | 1         |       | -         | 17     | 1    | a 100     | 1.59 | 18         | 1.98   | 55        | 1.00 | 4         |      |               |          |               | 17        |
|      |                |                |                           | 1                 |         |           |        |                | 1       |           |       |           | -18    | *    | a 90      | 1.58 | 18         | 1.80   | 36        | 1.00 |           |      |               |          |               | 18        |
| 19   |                | -ura-          |                           |                   |         |           |        |                |         | 3         |       |           | 19     | 2.40 | 108       | 1.57 | 17         | 1.56   | 17 .      | 1.02 | .7        |      |               |          |               | 19        |
| 20   |                | •              |                           |                   |         |           |        |                |         |           |       | -         | 20     |      | 9 110     | 1.68 | 25         | 1.66   | 24        | 1.09 | 1.1       | 1.01 | .7            |          |               | 20        |
|      | 1              | 1              | -                         |                   |         | *         |        | •              |         | 1         |       |           | 21     | 2.38 | 105       | 1.74 | 31         | 1.68   | 18        | 1.28 | 1.1       | ,98  | .5            |          |               | 21        |
|      |                |                | 1.*                       |                   |         |           |        |                |         |           |       |           | 1 22 1 | 2.38 | 105       | 1.67 | 25         | 1.49   | 13        | 1.17 | 24        | .80  | Trad at 6 P.  | ,        | 1.5           | 27        |
| 1    |                |                |                           | 1                 |         |           |        | 1 20           | -       | -         |       |           | 11     | 2.31 | 95        | 1.62 | 21         | 1.47   | R         | 1.07 | 1.0       |      |               |          | •             | 23        |
| 24   |                |                |                           |                   |         |           |        | 1              |         |           |       |           | 24     | 2.25 | 88        | 1.60 | 19         | 1.44   | 11        | 1.09 | 1.1       | 1    |               |          |               | 24        |
| 25   |                | **             |                           |                   |         |           |        |                |         | 1         |       |           | 25     | 6    | 9.82      | 1.57 | 17.        | 1.38   | 8.3       |      | 4 8       |      |               |          |               | 25        |
|      |                | •/             |                           |                   |         |           | -      |                | •       |           | -     | -         | 26     | 2.16 | 3:76      | 1.56 | 17         | 1.37   | 8.0       | 1.00 | 0.6       |      |               |          |               | 26        |
| 17   | -              |                |                           |                   | -       |           |        | Contraction of |         | 1         |       |           | 27     | 2.10 | 69        | 1.55 | 16         | 1.34   | 6.9       |      |           |      |               |          |               | 27        |
| 20   |                | and the second |                           | •                 |         |           |        | 1              |         | 1         |       |           | 28     | 2.04 | 62        | 1.49 | B          | 1.29   | 52        |      |           |      |               |          |               | 28        |
| 29   |                |                |                           |                   |         |           |        | 1.00           | 1910    |           |       | _         | 29     | 2.01 | 58        | 1.48 | 12         | 1.28   | 5.0       |      |           |      |               |          |               | 29        |
| - 30 |                |                |                           |                   | -       |           | -      |                |         |           | -     |           | 30     | 1.98 | 55        | 1.49 | 13         | 1.27   | 4.7       |      | una pre   |      |               |          |               | 30        |
| 31   |                |                |                           |                   | -       |           | -      |                |         |           | -     |           | 31     | •••  |           | 1.50 | 13         |        |           |      |           |      |               |          |               | 31        |
|      | TOTAL          |                |                           | The second second |         |           |        |                | -       |           |       | -         |        |      | •         |      | 848        |        | 338.5     |      |           |      |               |          |               |           |
| -    |                |                |                           | -                 | 1       |           |        |                | -       |           |       |           |        |      |           |      | 27.4       |        | 11.3      |      |           |      |               |          |               |           |
| - M  | cond-feet      |                | 1                         |                   |         |           |        |                |         | _         |       |           |        |      |           |      |            |        |           |      |           |      |               |          |               | -         |
| B    | m-off in       |                | 1                         |                   |         |           |        |                |         |           |       | *         |        |      |           |      |            |        |           |      |           |      |               |          |               | -         |
|      | and the second |                |                           |                   |         |           |        |                |         |           |       |           |        |      |           |      |            |        |           |      |           | 1    |               |          |               | A comment |

| Table product Reg in Boundary, in | Della |            | (ray)  |        |              | EX<br>PA      |          | T_9<br>2 OF | 13            |           | ,     | Si                                   |          | OF        | FICE<br>Water | OF S      | TAT  | REGON<br>E ENG<br>Departm | GINEER    | N<br>2 |           |                | in Tr     | 404<br><i>F</i> | 7420       | ope            | rale         | File   | No. U.S.<br>State | 2      | 51                    |
|--|---|------------|--------|--------|--------------|---------------|----------|-------------|---------------|-----------|-------|--------------------------------------|----------|-----------|---------------|-----------|------|---------------------------|-----------|--------|-----------|----------------|-----------|-----------------|------------|----------------|--------------|--------|-------------------|--------|-----------------------|
| No.       DOT       D  | Diaty   | age H      | D      | , in J | roct, a      | nd Disch      | arge, in | a Second-f  | eet, of<br>m. | N.A       | 1. 10 | Cree<br>hnse                         | n.       | , Obae    | near<br>rver) | Gage real | 1    | rda/                      | yn.0      | 2r.    | for the   | year en        | ding Sept | . 30, 19        | 2.5        | Table          | rating table | dated  |                   | 5-11   | 0-27                  |
| No. 1       No. 1 <th< td=""><td>* *</td><td>1</td><td></td><td></td><td></td><td>OCT.</td><td></td><td>NOV.</td><td></td><td>DEC.</td><td></td><td>JAN.</td><td>1</td><td>FEB.</td><td>1</td><td>MAR</td><td>T</td><td>T</td><td>APR</td><td>T</td><td>MAY</td><td>1 7</td><td>UNE</td><td>1 3</td><td>ULY</td><td></td><td>AUG.</td><td>81</td><td>EPT.</td><td></td><td>J'ALA' I</td></th<>   | * *   | 1          |        |        |              | OCT.          |          | NOV.        |               | DEC.      |       | JAN.                                 | 1        | FEB.      | 1             | MAR       | T    | T                         | APR       | T      | MAY       | 1 7            | UNE       | 1 3             | ULY        |                | AUG.         | 81     | EPT.              |        | J'ALA' I              |
|  | ond-fe  |            |        | De     | beight       | Discharge     | Gage     | Discharge   | Gage          | Discharge | Gage  | Discharge                            | Gage     | Discharge | Gage          | Dischar   | E A  | Gage<br>height            | Discharge | Gage   | Discharge | Gage<br>height | Discharge | Gage<br>beight  | Discharge. | Gage<br>height | Discharge    | Gage   | Discharge         | Day    | Stor -                |
| 1        | -   | 1.         |        | 1      |              |               |          |             |               |           |       |                                      |          | 2         |               |           | 1    | 235                       | 64        | 1.95   | 28        | 210            | 40        | 105             | 0.4        | 1.0            | 0.1          | 1      | 4                 | 1      | 500                   |
| 1        | 51  |            |        | 2      | -            |               |          |             |               |           |       |                                      |          |           |               |           | . 2  | 245                       | 74        | 1.90   | 2 25      | 2.95           | 74        | 11              | 0.6        |                | ./           |        | 4                 | 2      |                       |
| and an and an analysis         and an analysis       and a   | 10  | 1          |        | 3      |              |               | -        |             |               |           |       |                                      |          |           |               |           | 3    | 240                       | 69        | 1.90   | 25        | 2,30           | 59        | 1.1             | 0.6        | 1.0            | ./           | 1.05   | .4                | 3 8    |                       |
| 1        | 11  |            |        | 4      | -            |               | -        |             |               |           |       |                                      |          |           |               |           | 1    | 12.40                     | 69        | 1.85   | 22        | 222            | 51        | 1.1             | 0.6        |                | )            |        | 4                 | 4      |                       |
| 1        |   |            |        | 5      | -            |               |          |             |               | -         |       |                                      |          |           |               |           | . 5  | 240                       | 69        | 1.85   | 22        | 215            | 44        | 105             | 0.4        |                |              |        | 4                 | 5 -    |                       |
| 1        | - BB  | •          |        | G      |              |               |          |             |               |           |       | -                                    |          |           |               |           | 6    | 2.50                      | 79        | 1.80   | 19        | 210            | 40        | 1.05            | .4         |                |              |        | 4                 | 6      | • • •                 |
| a       a       b       b       cos 64       cos 32       cos 4  | leche<br>leche  | .;         |        | 7      |              |               | 1        |             |               |           |       |                                      |          |           |               |           | 1    | 240                       | 69        | 1.75   | 16        | 205            | 36        | 105             | .4         |                |              | 1.05   | 4                 | 1 Inte |                       |
| 1        | AA  |            |        | 8      |              |               |          |             |               |           |       |                                      |          |           |               |           | 8    | 235                       | 64        | 1.75   | 16        | 200            | 32        | 1.05            | .4         |                |              |        | 4                 | 8 6    | Comp                  |
| Image: Solution of the second seco        | 143   |            |        | 9      | -            |               |          |             |               |           |       |                                      | 1        |           | 1 .           | -         | 9    | 230                       | 59        | 180    | 19        | 1.95           | 28        | 1.05            | .4         |                | 1.1          | 105    | .4                | 9      |                       |
| III       III       III       III       IIII       IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII  | 52  | 140        |        | 10     |              |               |          |             |               |           |       |                                      |          |           |               |           | . 10 | 225                       | 54        | 1.80   | 19        | 190            | 25        | 1.03            | .2         |                |              | 1      | 4                 | 10 \$  | QN:                   |
| 11       11       11       11       11       12 <td< td=""><td>12 4</td><td>V.</td><td></td><td>11</td><td></td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td>1</td><td>11</td><td>220</td><td>49</td><td>175</td><td>. 16</td><td>1.85</td><td>22</td><td>1.03</td><td>.2</td><td></td><td></td><td></td><td>4</td><td>11</td><td>4. 2 .</td></td<>   | 12 4  | V.         |        | 11     |              | 1             |          |             |               |           |       |                                      | 1        |           |               | 1         | 11   | 220                       | 49        | 175    | . 16      | 1.85           | 22        | 1.03            | .2         |                |              |        | 4                 | 11     | 4. 2 .                |
| 1        | in m  | 13         |        | 12     | 1            | 1             |          |             |               |           |       |                                      | -        |           |               |           | 12   | 220                       | .49       | 1.70   | 14        | 1.80           | 19        | 1.00            | .1.        | 10             |              | •      | 4.                | 12 6   | 0 80                  |
| Image: Section of the section of th        | 53  | 1          |        | 18     | 1 2 2        | 1000          | 1.       |             | -             |           |       | 12.000                               |          | 4         |               | 12        | A II | 220                       | 49        | 165    | 13        | 1.75           | 16        | 105             | 4          |                | ) 14         | 105    | 4                 | 18 .   | 9                     |
| Image: Section of the section of th        | 73  | Na l       | 1      | 14     | S.th.        | 14.15         | ·        | N           |               |           | -     | the state                            |          | quela e   |               |           | 14   | 21                        | 40        | 1.65   | 13        | 1.75           | 16        | 100             | .1         | 10.            | ./           | 160    | 11                | 14 &   |                       |
| 1        | 13  | 1          | 1.1    | 15     | 活题           | 1. 19         | 1        |             | 1.1.1         |           |       | Sec. 20                              |          | 14 J 14   |               | 1. 1.     | 10   | 21                        | 40        | 1.75   | 17        | 1.70           | 14        | 100             | /          |                | ).           | 105    | 62                | 15 #   |                       |
| на  | 5.8   | 1          |        | 16     | · Sigle      | 言語語           | - 44.    | +6 1        |               |           |       | .a                                   | 1.4      |           | 1             |           | 18   | 245                       | .74       | 120    | .14       | 1.65           | 12        | 105             | . 4.       |                | 1            | 110    | 0.6               | 16 -   |                       |
| Image: | in l  | 1          | 1      | 17     | Bart         | 122228        | 1        |             |               |           |       | - 24                                 | 4.       | N 11      |               | 1.00      | 117  | 230                       | 59:       | 1:80   | 1.19      | 160            | 11        | 105             | · 4.       | •              | 1.1          | 110    | . 0.6             | 17 1   | and in                |
| 10       200       69       10       200       69       10       25       160       1       100       1       <  |   |            |        | 18     | T            |               | n.7      | 1.1.1       |               |           |       | 1 2000                               | 1.20     |           | 245           | .74       | 18   | 220                       | 491       | 195    | -28 .     | 1.55           | 9.4       | 106             | 4.         | -              |              | 105    | 4                 | 16     |                       |
| a       265       74       265       96       256       1.3       1.0 </td <td></td> <td>1</td> <td></td> <td>19</td> <td>***</td> <td>2 **</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>111</td> <td>2:40</td> <td>69</td> <td>19</td> <td>230</td> <td>59</td> <td>190</td> <td>25</td> <td>150</td> <td>20</td> <td></td> <td></td> <td></td> <td></td> <td>100</td> <td>.1</td> <td>19 0</td> <td>Diad<br/>Diad</td>   |   | 1          |        | 19     | ***          | 2 **          |          |             |               |           |       |                                      |          | 111       | 2:40          | 69        | 19   | 230                       | 59        | 190    | 25        | 150            | 20        |                 |            |                |              | 100    | .1                | 19 0   | Diad<br>Diad          |
| a  |   | 1          |        | 20     |              | 1.1.8         | x2 .     |             |               |           | • •   |                                      |          | 2         | 2.45          | 74        | 20   | 566                       | 96        | 290    | 128       | 1.05           | 6.5       |                 | .3         |                | )            | 10     | ./                | 20     | NOJ VI                |
| 275       106       275       106       276       74       30       117       125       41         | 11 1  | 151        |        | 21     | 15817        | 19 Birth      | stor.    | 1           | * ++          |           |       | Sec. Sec. 1                          | 1.00     | 4 ····    | 275           | 106       | 1 21 | 205                       | 174       | 400    | 300       | ino            | 52        | 4 .             |            | 10             | 1-           | 10     | .1                | 21 4   | 2 2 3                 |
| 3       -  | S. 5. 2   | 明          | 200    | 22     | **#167       | بعذن فبراه مد | 100      | -           |               |           | 1.4.4 |                                      | S. 12.4. | Sec. 12   | 275           | 106       | 1 21 | 205                       | 74        | 350    | 117       | 135            | 41        |                 | · · · ·    | A. 5.          | 1            | 10     |                   | 22     | de l'                 |
| All and  | 15  | 1          |        | 23     | 1.52 .       | in her the    | 1.0      | 1.5         | 1             |           |       | Sec. al                              | 100      | 24.9      | 260           | . 90      | 23   | 200                       | 69.1-     | 200    | 115       | 130            | 3.1       |                 | .2         | 15 1 3         | 2            | (1.44) |                   | 23     | Far                   |
| Image: set of the set of        | いい  | 运行         | 探      | 贫      | 成的社          | 影行动           | 教授       | A.A.        | · print.      | 11 mar    | 公园    | 日本なる                                 | 製品       | intra an  | 255           | : 84      | 自民   | 3333                      | 159 E     | 360    | 1902      | 180            | 5.2       | 5-15-           | 出行系统       | 103            | 200          | in the | 191731            | 31.6   | al and and            |
| And  | 10  | 行業         | 127    | 12     | tratin.      |               | ""       | 1000        | 1             | A         |       | 17. 1 1 mit                          | 144      | the said  | 550           | -79       |      | 200                       | 49        | 5.00   | -79       | 130            | 19        | 100             | -1         | -1.1.1         |              |        | 1                 | 25 8   | See.                  |
| 1        | 200   | 市合語        | 13     | 2      | 1444<br>1444 | 1.2.2.3       | 北北       | ·           |               |           | 2. 22 | 15 11                                | 15 acres | 23 124    | 255           | 84        | 日次   | nstal.                    | 49%       | 200    | 64        | in             | 320.      | -A.)            | -1.A.S.S.  |                | 10           | 10     | 11                |        | 2. 1 1                |
| Image: Non-State     Image: Non-State <td></td> <td>and the</td> <td>1-12</td> <td>14.07</td> <td></td> <td>· ·er +</td> <td>10.0</td> <td>1.1</td> <td></td> <td>1</td> <td></td> <td>. T<sup>13</sup> (1<sup>-3</sup>)</td> <td>1.000</td> <td>n</td> <td>250</td> <td>179</td> <td></td> <td>215</td> <td>44</td> <td>220</td> <td>. 49</td> <td>120</td> <td>777</td> <td>14. 1</td> <td>1. 4</td> <td>1</td> <td>2</td> <td>10</td> <td></td> <td>20 10</td> <td>12 1.2</td>  |   | and the    | 1-12   | 14.07  |              | · ·er +       | 10.0     | 1.1         |               | 1         |       | . T <sup>13</sup> (1 <sup>-3</sup> ) | 1.000    | n         | 250           | 179       |      | 215                       | 44        | 220    | . 49      | 120            | 777       | 14. 1           | 1. 4       | 1              | 2            | 10     |                   | 20 10  | 12 1.2                |
| III IIII IIIIIIIIIIIIIIIIIIIIIIIIIIII  | atage atage   |            |        | 20     |              | 1 1 1         | -01      |             | 1.            |           | -     |                                      | ** .     | 1 4       | 245           | 74        | 152  | an                        | 40        | 210    | 44        | 116            | 12        | 1               |            | -              |              |        | -1 -              | 21     | 1 1 1                 |
| In mage       Image       <  | -   | Y          |        | 20     |              |               | 10       | 1 1 1       |               |           |       |                                      | 1. 10    | 1. 1      | 245           | 74        | 20   | 205                       | 36        | 20     | 54        | 16             | 12        |                 | ./         |                | - En         |        | ./                | 28 tre | cepti<br>chee<br>bits |
| X X X     X X<   | atta  | aro        |        | 20     |              |               | -        |             |               |           |       |                                      |          |           | 205           | 74        | 30   | 200                       | 32        | 220    | 49        | 110            | 06        | -               |            | 105            | 4            | 10     | 1                 | 2 6    | о.п.<br>о.п.          |
| Total     1/36     1/760     1/500     59/.6     8.7     4.8     2.5.2     5.026.3       Mean     1/4da/81/1     58.7     48.4     19.7     .28     .15     84       Tunott in scrift     2250     3,490     2980     1/70     17.5     9.50.0     9.966.       Maximum     106     96     74     .6     .4     11.  | M   | N          | 1 1    | 21     |              | 201           |          |             |               |           |       | •                                    |          |           | 210           | 69        | In   |                           |           | 511    | £ 41      |                |           |                 |            | 103.           | A            | 1.0    |                   | 30 -   | Period                |
| Mean         14dal 81.1.         58.7.         48.4.         19.7         28.8         15         84.           Mean         14dal 81.1.         58.7.         48.4.         19.7         28         15         84.           Tamoett in screett.         2250         3,490         2980         1/70         17.5         9.50.0         9.966.           Maximum         106         96         74.6         4.1         11.           Minimum         69.38         13         0.65         11         1         1   | 5 token   |            | -      | 101    |              | · · · ·       | 1.1      | 1           |               |           | -     | · • ·                                |          | 1         | 2.40          | 1136      |      |                           | 1760      | 1.     | 1.500     |                | 5916      | -               | 87         | -              | 18           |        | 050               | S1     | 50000                 |
| Run-off in acre-ft.         2250         3490         2980         1/70         17.         9.         50.0         9.956.           Maximum         106         96         —         74.         6.         4.         11.           Minimum         69.         32.         13.         0.6.         11.         11.   | Ser. Pa   | lean       | otai - | -10-   |              |               |          |             |               | 1.0.      |       |                                      |          | · 5.      | 14da          | 1811      | 2.44 |                           | 587.      |        | 484       |                | 197       |                 | 28         | the states     | 16           | -      | 81                |        | 5,0263                |
| Maximum<br>106 96 — 74 6 4 11.<br>Minimum  | 2019  | inn off to | a acre | ri.    | 12           |               | 8.3      |             |               | -         | •     |                                      | -        | 1         | . 1           | 250       | 1    | 1.4                       | \$490     |        | 2980      |                | 170       | - 1             | 17:        | 1.00           | 90           |        | 500               |        | garri                 |
| Minimum 69 32 13 0.6 11 11   |   | arimum     | 1      |        |              |               | -        |             | 1             |           |       | •                                    | 1        | 1.00      |               | 106       |      |                           | 96        |        | -         |                | 74        | The second      | .6.        |                | A            |        | 11                | -      | 2,500.                |
|  |   | linimum    |        | -      | 2            |               | 122      |             |               |           | 1.8   |                                      | 1-       | 1         | 1.            | 69        | 1    | 1-1                       | .39       |        | 1.3       |                | 0.6       |                 | ./1        |                | 1            | -      | 11                |        | *                     |

|       |          | in 1   | Feet, a    | nd Discha   | rge, in   | Second-fe   | eet, of . | Roc       | ok (   | reek                                     |        |               | -at-     | Gwe                                   | no   | 10/3   | in, c     | reg  | L. for the | l<br>year en | ding Sept. | 80, 19 | 2.6 .          | Table  | of use: Ha   | If tenths |           | _ft t   | •      |
|-------|----------|--------|------------|-------------|-----------|---|-----------|-----------|--------|--|--------|---------------|----------|---------------------------------------|------|--------|-----------|------|------------|--------------|------------|--------|----------------|--------|--------------|-----------|-----------|---------|--------|
| _     | D        | rainag | re area .  | -           |           | square mile   | s.,       | Mrs.      | N.M.   | Johns                                    | on     | Obser         | ver) (   | lage read t                           | o    | Hdi    | ts        |      | OD0        | ce a da;     | y .*       |        |                | Used   | rating table | dated     | 5-10      | -27     | - ALum |
| 1     |          | 2      | Gare       | )OT. '      | · · ·     | NOV.  | 1         | DEC.      |        | JAN.                                     |        | FEB.          | 1        | MAR.                                  | TT   | 7      | APR,      |      | MAY        | J            | UNE        |        | TULY           |        | AUG.         | 8         | EPT.      | 5 4     |        |
|       |          | 8      | height     | Discharge   | height    | Discharge   | height    | Discharge | Gage   | Discharge                                | Gage   | Discharge     | Gage     | Discharge                             | DAy  | Gage   | Discharge | Gage | Discharge  | Gage         | Discharge  | Gage   | Discharge      | height | Discharge    | height    | Discharge | a ·     | 0.0    |
|       |          | 1      |            |             |           |   |           |           |        |  |        |               |          |                                       | 1    | 2.6    | 90-       | 1.8  | 19         | 1.25         | 24         |        |                |        |              |           |           | 1       | 40     |
|       |          | 2      |            |             |           |   |           |           |        |  |        |               |          |                                       | 2    | 2.6    | 90.       | 1.7  | 14         | 1,25         | 24         |        |                | -      |              |           |           | 2 -     | a      |
|       |          | 3      |            |             |           |   |           |           |        |  |        |               | 1        |                                       | 8    | 2.45   | 74        | 1.7  | 14         | 1.25         | 2.4        |        |                |        |              |           |           | 3 0     |        |
|       |          | 4      |            |             |           |   |           |           |        |  |        |               |          |                                       | 4    | 2.5    | 79        | 1.7  | 14         | 1.2          | 17         |        |                |        |              |           |           | 4-      | -      |
|       |          | 5      |            |             |           |   |           |           |        |  |        |               |          |                                       | 5    | 2.75   | 108       | 1.8  | 19         | 1.2          | 17         |        |                |        |              |           |           | 5       |        |
|       |          | 6      |            |             |           |   | 2         |           |        |  |        |               | -        |                                       |      | 265    | 94        | 185  |            | 115          | 12         |        |                |        |              |           |           | -       |        |
|       |          | 7      |            |             |           |   |           |           |        |  |        |               | 1        |                                       | 0    | 200    | 81        | 18   | 10         | 115          | 1.6        |        | -              | -      |              |           |           | a a     | 7      |
|       |          | 8      |            |             |           |   |           | •         |        |  | 1      |               | -        |                                       |      | 2.55   | 04        | 185  | 19         | 115          | 8/12       |        |                |        |              |           |           | - Ound  | Incu   |
|       |          | 9      |            |             |           |   |           |           |        | 1  |        |               | 1        |                                       | 8    | 26     | 04        | 180  | 22         | 115          | 1.2        | -      |                |        |              |           |           | -       | 3      |
|       |          | 10     |            |             |           |   |           |           |        |  |        | -             |          |                                       |      | 25     | 90        | 175  | 12         | 115          | 14         | -      |                | +      |              |           |           | 10 5    |        |
|       |          | 11     |            |             |           | 1   |           |           |        | . *                                      | -      |               |          |                                       | 10   | 2.0    | 19        | 17   | 1.1        | 115          | 1.2        |        |                | -      |              |           |           | 10 -    | 02     |
|       |          | 10     |            | -           |           |   |           |           |        |  |        |               |          |                                       | 11   | 3.0    | 146       | 1.1  | 14         | 145          | 1.2        | -      |                |        |              |           |           | 11 2    | 18     |
|       |          | 1.     | 3.34       |             |           | +   |           |           |        |  | 2.2    | 1             |          |                                       | 12   | 2.05   | 122       | 1.05 | 12         | 1.10         | 1.2        | •      |                |        |              | -         |           | 12 -    | 0      |
| 1.    | See. 1   | 10     |            | 4- m        |           | 101.14.11   |           | -         | 1      | 3 10 10 10                               | ×      |               |          | 12                                    | 18   | 2.1    | 104       | 1.0  | 11         | 1.13         | 1.2.       |        |                | -      |              |           |           | 18 5    |        |
|       | . 1      |        | 36.4       | Strate C    | 1.1.      |   | 1         |           |        | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 | dati   | 1.1.1         | 1.0      |                                       | 11   | 2.0    | 90        | 1.6  | 11         | 1.15         | 1.2        |        |                |        |              | -         |           | 14      |        |
|       |          |        | - (.).     | Andres Car  | 1.58.51   |   |           |           |        |  |        |               |          |                                       | 15   | 2.55   | 84        | 1.6  | //         | 1.15         | 1.2        |        | *              |        |              |           |           | 15 #    |        |
|       |          | 16     | 44.64      |             | \$23      | -   |           |           |        | 44.4                                     |        | - 1.          |          |                                       | 10   | 2.45   | .74       | 1.65 | .12.       | 1.15         | . 1.2      |        |                | -      |              |           |           | 16 -    |        |
|       | 1 .      | 17     | 1.000      | Alles I. C. | Sec. 20   | 100 - | 1.00      |           | 1.0.2  | and the                                  | Sec. 1 | Constraint of |          |                                       | 17   | 2.4    | 69        | 1.65 | 12         | 1,15         | 1.2        |        |                |        | -            |           |           | 17 5    | alt.   |
| 1     |          | 18     |            |             |           |   |           |           |        | 1 45                                     |        | 1 - 1         |          | · 4                                   | 18   | 2.4    | . 69      | 1.6  | 11         | 1.1          | .6.        |        |                |        |              | -         | -         | 18      | 4      |
|       |          | 19     |            |             |           | 1   | -         |           |        |  |        |               |          |                                       | 19   | 2.4    | . 69      | 125  | 9.4        | 1.1          | .6         |        |                |        |              |           |           | 19      | ā      |
|       | 1        | 20     | 1.1        |             |           |   | :         |           | -      | n -                                      |        |               | • •      | 3                                     | 20   | 2,35   | 64        | 1.53 | 9.4        | 1.1          | .6         | 1      |                |        | *            |           |           | 30      |        |
|       |          | 21     | 1227-1     | dente di    | a's a     | 14  | -         |           | . d.   | Sec. A.L.                                | Tris   | -with the     | 12       | ···                                   | 21   | 23     | - 59      | 7.55 | 9.4        | 1.1          | .6 .       | 1.41   | -              |        | 1.000        |           |           | 21 -    |        |
|       | 1 2      | 22     | - 34-5-2 c | a har all   | SAME!     | 14  | 4         | 1. 1.     | (Care) | - All and a state                        | 1.2.2  |               | ( Shiel  | 20 State                              | 22   | 2.3    | \$ 59     | 1.45 | 6.5'       | 1:05         | 4-         | 1      |                | 1      | +            |           | -         | 22 8    | 3.6    |
| 1     |          | 23     | and the    |             | 1         | 1   |           |           |        | e = 1.14                                 | 5.     | A. C. th      |          | -                                     | 23   | 2.25   | 54.       | 1,45 | 6,5        | 1.05         | A          |        |                | *      |              | • •       |           | 23 -    | 0      |
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|       |          | 23     | 学习         |             | alpertan. | -   |           | 1         | -      | a a a a a a                              | 1      | 合合和           | Ser.     | 1.                                    | 105  | 2.2-   | -49       | 14   | - 5.2      | 1.05         | - 4-       | 2.64   | 1.             |        | · · ·        | '         | 1         | 25 -    | 1      |
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| ľ     |          | 28     | States ?   |             | 194       | 1.10  |           |           |        | 16                                       | 1.1    | 17.2 × 2.2    |          |                                       | 13.1 | 1.9    | 25        | 1.4  | · ·5.2     | -            | 0          | 1.1    | . 17           |        |              |           | 2-1       | 25 5    | I      |
| 1     |          | 29     |            |             |           | 1.00  | -         |           | +      |  |        | -             | -        |                                       | 22   | 1.85   | 22        | 1.4  | 5.2        |              | 0          |        |                |        |              |           | -         | S and   | 1      |
| ALO   |          | 30     |            |             |           |   | -         |           |        |  |        |               |          |                                       | 30   | 1.8    | 19        | 135  | 4.2        |              | 0          |        |                |        | -            |           |           | - 0     | 0.1    |
| X     | 1 1      | 81     |            |             |           |   |           |           |        |  |        |               |          | 14                                    | 81   |        |           | 1.3  | 31         |              |            | -      |                |        |              |           |           |         | Pe     |
|       | Total    | -      |            |             |           |   |           | •         |        | 3 .                                      | · .    | 10            | 1        | Sel.                                  | 0    |        | 2172      |      | 351.5      | *            | 29.4       |        |                | •      |              | 1         |           | 311     | 25     |
| en -  | 1        | 1      | er.        | 1           | 1.00      |   |           | 1.1.1     | 1.00   |  | • •    | 12 11         | 121      | 1.1.1.2                               | 1    | 14     | 72.4      | 5 A. | 11.3       | 2706         | 109        | 98 .   | and the second | 11.10  |              |           |           |         | an     |
| n-off | in acre- | r.     | · · · · ·  | 1336        |           |   |           | 14        |        | 1.2.1                                    |        | the fight     | 14%      | 18 24                                 | 1    | 1511 . | 4310      | -    | 695        | 1            | 58         |        | 4              |        | THUR         | - 1       | g         | 6.47 ** | .5     |
| rime  |          |        | 2.4        |             |           |   |           | 1         |        | • •                                      |        | 11.           | 1. 16.5. | · · · · · · · · · · · · · · · · · · · |      | 1.00   | 142       | 1R   | 22         |              | 24         | 1.3    |                |        | EXHIB        | 1=        | 1         | -       | 00     |
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## OREGON COOPERATIVE WORK

DEPARTMENT OF THE INTERIOR UNITED STATES RECLAMATION SERVICE IN COOPERATION WITH STATE OF OREGON

# JOHN DAY PROJECT Irrigation and Drainage

BY JOHN T. WHISTLER ENGINEER U. S. RECLAMATION SERVICE

JOHN H. LEWIS STATE ENGINEER FOR OREGON

FEBRUARY 1916

#### PROJECT CONSIDERED

#### JOHN DAY PROJECT

|             | Discha  | rge in Secon | Run-off |                       |         |
|-------------|---------|--------------|---------|-----------------------|---------|
| MONTH       | Maximum | Minimum      | Mean    | Total in<br>Acre-feet | A ccur- |
| 1905        |         | 1            |         | 1                     | 1       |
| March       | 87      | 28           | 50.0    | 3,070                 | B.      |
| April       | 103     | .6           | 38.1    | 2,270                 | B.      |
| May         | 145     | .3           | 12.3    | 756                   | B.      |
| June        | 488     | .3           | 45.5    | 2,710                 | B.      |
| July        | 1.3     | .3           | .67     | 41                    | B.      |
| August 1-20 | 3.8     | .3           | 1.24    | 49                    |         |
| The period  | 488     | .3           | 26.0    | 8,900                 |         |
| 1906        |         |              |         |                       |         |
| March       | 625     | 44           | 115     | 7,070                 | C.      |
| April       | 224     | 22           | 71.1    | 4,230                 | C.      |
| May         | 1,640   | 10           | 109     | 6,700                 | D.      |
| June        | 725     | 32           | 221     | 13,200                | C.      |
| July 1-21   | 32      | 19           | 22.1    | 920                   | C.      |
| The period  | 1,640   | 10           | 115.0   | 32,100                |         |

Ectimated Monthly Discharge of Willow Creek near Arlington, Oregon, for 1905-1906.

It will be noted from the tables that there is very little difference between the discharge of the river at McDonald and Clarno, during the period of low water. This would be expected, since the tributaries between the two stations are practically dry at this season of

Monthly Discharge of Rock Creek near Arlington, Oregon, for 1905 and 1911.

|              | Dischar | rge in Secon | Run-off |                       |       |  |
|--------------|---------|--------------|---------|-----------------------|-------|--|
| MONTH        | Maximum | Minimum      | Mean    | Total in<br>Acre-feet | Accur |  |
| 1905         |         |              |         |                       | 1     |  |
| March        | 256     | 32           | 93.2    | 5,730                 | B.    |  |
| April        | 167     | 10           | 57.5    | 3,420                 | B.    |  |
| May          | 50      | 10           | 22.7    | 1,400                 | B.    |  |
| June         | 45      |              | 10.2    | 607                   | C.    |  |
| July         | 10      | 0            | .97     | 60                    | C.    |  |
| The period   | 256     | 0.0          | 36.9    | 11,200                |       |  |
| 1911         |         |              |         |                       | 1     |  |
| April 6-31   | 73      | 7.3          | 36.7    | 1,880                 | B.    |  |
| May          | 10      | .9           | 4.91    | 302                   | B.    |  |
| June         | 1.2     | .6           | .87     | 51.8                  | B.    |  |
| July         | 1.2     | .2           | .57     | 35.0                  | B.    |  |
| August       | .4      | .0           | .21     | 13.0                  | B.    |  |
| September    | .9      | .0           | .37     | 22.0                  | B.    |  |
| October 1-21 | 1.6     | .6           | 1.40    | 58.3                  | В.    |  |
| The period   | 73.0    | 0.0          |         | 2,360                 |       |  |

the year. The tables show that by applying records at McDonald to the diversion site, assumptions will closely represent actual discharge at this point.

A gaging station was established on Camas Creek in April, 1914, and records have been kept since that time. The following records were furnished by the District Engineer, Water Resources Branch of the U. S. Geological Survey.

Monthly Discharge of Camas Creek below Cable Creek near Ukiah, Oregon.

| MONTH      | Discha | Run-off |        |           |
|------------|--------|---------|--------|-----------|
|            | Max.   | Min.    | Mean   | Total in  |
| 1914       | 1      | 1       |        | Acre-leet |
| May        | 265    | 10      | 1 7.15 |           |
| June       | 585    | 20      | 140    | 8,920     |
| July       | 26     | 10      | 112    | 6,660     |
| August     | 10     | 10      | 17.7   | 1,090     |
| September  | 10     | 6       | 7.5    | 460       |
|            | 13     | 5       | 10     | 600       |
| The period |        |         |        |           |
|            | 585    | 5       | 58.4   | 17,730    |
| 1914-15    |        |         |        |           |
| October    | 17     |         |        |           |
| November   | . 11   | 9       | 13.0   | 800       |
| December   | - 14   | ••      | 11.4   | 680       |
| January    |        | ••      | 7.0    | 430       |
| February   |        | ••      | 5.0    | 310       |
| March      |        |         | 10.0   | 560       |
| April      | *635   | ••      | 158    | 9 7 9 0   |
| May        | 860    | 47      | 215    | 12,800    |
| June       | 460    | 61      | 244    | 15,000    |
| ulv        | 233    | 20      | 63.3   | 2,000     |
| Ugnet      | 24     | 9       | 13.7   | 3,110     |
| leptember  | 10     | 5       | 74     | 840       |
| optember   | 10     | 5       | 7.1    | 450       |
|            |        |         | 1.1    | 420       |
| The year   | 860    | -       |        |           |
|            | 000    | 0       | 63.0   | 45,780    |

#### SOILS.

Much difference of opinion has obtained as to the value of soils along Columbia River in this region, and it has therefore appeared desirable that this phase of the problem be given the fullest con-

A soil and agricultural survey of the irrigable lands was made June 10 to June 17, inclusive, 1915, by W. L. Powers, Associate Agronomist in Irrigation and Drainage, and C. V. Ruzek, Assistant Agronomist in Soils, of Oregon Agricultural College.

\*Discharge from November 19 to March 12 estimated on account of ice. The monthly values are provisional and subject to revision when the statistic revision r

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ROCK CREEK WATERSHED PROJECT Gilliam and Morrow Counties, Oregon

FINAL ENVIRONMENTAL IMPACT STATEMENT

James W. Mitchell State Conservationist Soil Conservation Service

Sponsoring Local Organizations

Gilliam County Soil & Water Conservation Distric Arlington, Oregon 97812

Morrow Soil & Water Conservation District Heppner, Oregon 97836

Rock Creek Water Control District Arlington, Oregon 97812

April 1975

PREPARED BY

UNITED STATES DEPARTMENT OF AGRICULTURE

Soil Conservation Service

1218 S. W. Washington Street Portland, Oregon 97205





Soil Association 4 - Nearly Level to Very Steep Soils of Forested

#### Uplands, Hankins-Klicker-Boardtree Association -

This association occupies a broad, rolling plateau with many small, concave drainages in the highest part of the area. Hankins soils are very deep, dark colored, clayey soils on gentle to steep slopes with northerly aspect.

Klicker soils are moderately deep, stony, silty soils over basalt bedrock. They occupy steep to very steep slopes and are intermingled with basalt outcrops.

Boardtree soils are gravelly loam soils underlaid by clayey sediments at depths of 20 to 40 inches. These soils occupy moderately steep to steep north-facing slopes.

The Hankins, Klicker, and Boardtree soils have a high moisture-supplying capacity for plants.

Minor areas of very shallow Rockly soils occur on ridgetops.

#### Ground Water Resources

The potential for obtaining an adequate and economical supply of ground water is poor in this watershed. Potential for ground water supply is fair to good in the areas underlain by the basaltic lavas and poor in the areas of John Day sediments. The lava flows dip gently north from the Blue Mountains and receive some recharge from the mountains and from the incised drainages within the watershed. The main problem inherent to water production from this formation is the unpredictability of the well yields. Generally, wells in these basalts can be expected to produce one gallon per minute per foot of depth below the water table with a bore diameter of 10 inches or larger. Values significantly smaller or larger than this may be experienced within short horizontal distances. The water table is generally at substantial depths.

Existing wells within the basaltic lava flows of the watershed are generally for domestic supplies only. Recently, however, a few large diameter irrigation wells were drilled along the flood plain of Rock Creek and provided yields ranging from 300 to 1,250 gallons per minute. Future ground water development will depend upon evaluation of the existing units, but present indications are that this source will not sustain a significant increase in withdrawal.

#### Surface Water Resources

EXHIBIT.

PAGE 2 OF

Rock Creek is a tributary to the John Day River. The confluence of the creek and the river is 21.6 miles above the junction of the John Day with the Columbia River. (16) The principal tributaries of Rock Creek are Juniper, Lone Rock, Sixmile, and Dry Fork Creeks.

Rock Creek is 71.7 miles long with 143.4 miles of streambank. It is an unmodified perennial stream for approximately 20 miles in its upper reaches, an unmodified intermittent stream for 21 miles, and a modified intermittent stream for 30.7 miles in its lower reaches where it passes through cropland. The stream width varies from 30 to 270 feet and depth varies from 5.5 to 11 feet. The headwaters of Rock Creek are at an elevation of 5,360 feet. The creek falls to an elevation of 420 feet at the mouth. (4)

The Creek varies from a small, incised, upland channel having no flood plain to a stream having an average channel top width of 85 feet with a 100-year flood plain averaging 550 feet in width.

Rock Creek has a typical snowmelt runoff pattern of high spring flows and low to nonexistant surface flows during the summer and fall. Generally, the highest runoff volume occurs in April with about 58 percent of the annual runoff from March through May, and 71 percent from February through May in the vicinity of Cayuse Canyon. At the mouth of Rock Creek it is estimated that 64 percent of the annual runoff occurs from March through May and 79 percent occurs from February through May. (17) On occasion, however, a warm front producing precipitation combines with a warming trend and depletes the winter snow pack producing high funoff (near 9,000 cfs for a 100-year event) during the winter months. Only 7.7 percent of the annual runoff occurs during June through mid-October in the vicinity of Cayuse Canyon. (17)

EXHIBIT \_\_\_\_\_ PAGE \_3\_\_\_ OF \_3\_\_\_

Average monthly stream discharges are:

Months

Rate of discharge in cfs

| 5         | Rock Creek near Cavuse | Vicinity | Mouth of   |
|-----------|------------------------|----------|------------|
|           | Canyon (vicinity of    | of Olex  | Rock Creek |
| · · ·     | Gnost Camp) .          |          |            |
| October   | 4                      | 0 .      | 0          |
| November  | 11                     | 0        | 0          |
| December  | 34                     | 37       | 38         |
| January   | 42                     | 46       | 47         |
| February  | 61                     | 66       | 67         |
| March     | . 71                   | 77       | 79         |
| April     | 98                     | 105      | 108        |
| May       | 82                     | 77.      | 79 -       |
| June      | 2.7                    | 9        | 0          |
| July      | 4 .                    | 0        | 0          |
| August    | 0.5                    | 0        | 0          |
| September | 0.9                    | 0 .,     | 0          |

Rock Creek averages no flow for 30 days each year in the vicinity of Cayuse Canyon. In the seven years of record at this location the dry period ranged from 0 to 80 days. (17) In the lower reaches of Rock Creek the stream is essentially dry from June through November on the average.

Sixty miles of riparian vegetation occur along the creek. The ciparian vegetation is listed below.

| Trees:  | ponderosa pine<br>Douglas fir | cottonwood<br>alder        | hawthorn<br>birch              |      |
|---------|-------------------------------|----------------------------|--------------------------------|------|
| Shrubs: | willow<br>choke cherry        | elderberry<br>bittercherry | golden current<br>serviceberry | rose |

# JOHN DAY RIVER BASIN

STATE WATER RESOURCES BOARD . SALEM, OREGON March 1962



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#### BOARD MEMBERS

LOUIS H. FOOTE, Chairman - Forest Grove KARL W. ONTHANK, Vice Chairman - Eugene LaSELLE E. COLES - Prineville GEORGE H. COREY - Pendleton JOHN D. DAVIS - Stayton RUTH HAGENSTEIN - Portland ROBERT W. ROOT - Medford

DONEL J. LANE, Secretary



#### WATER SUPPLY, USE, AND CONTROL

acre per season for diversions from the main stem, North Fork, and Middle Fork of the John Day River, and four acre-feet from all other tributaries, as established by the John Day River adjudication of water rights. A duty of four acre-feet per acre per season was assumed for ground water rights.

The actual consumption of water for irrigation purposes is undoubtedly smaller, because only 49,000 acres are presently irrigated, not all rights can be exercised to their legal limit because of seasonal deficiencies in water supply, and because irrigation return flows are reused by downstream irrigators. Assuming a consumptive irrigation requirement of two acre-feet per acre, about 100,000 acre-feet would be needed each year to supply the consumptive requirements of the existing irrigated acres in the basin.

The average annual yield of the John Day River at its mouth is 1,410,000 acre-feet. Thus, the current use of irrigation water represents less than 10 percent of the gross basin water yield. However, there are many serious local and seasonal shortages relative to available water.

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The amount of yield during the main irrigation season, April through September, generally represents from 45 to 75 percent of the total annual yield. However, the monthly yield progressively diminishes through the irrigation season to the extent that the yield for September ordinarily is less than one percent of the total annual yield. Hence, all irrigated lands, including those along the main rivers, can experience late season water shortages. This situation is most serious along smaller tributaries because late summer flows are often extremely low or nonexistent. A review of 42 small watersheds, covering 80 percent of the basin area and including most of the irrigated land in the basin, indicates that 32 of these watersheds have inadequate total or late season water supplies for existing irrigated lands.

Modifications of the runoff pattern through reservoir storage would be essential in order to provide a fully adequate water supply for much of the presently irrigated land. Many lands are overirrigated during the early part of the season when a large supply of water is available. In many cases, the entire seasonal quantity of water allowed by the water right is used during the high flow months. Reservoir storage, designed to alleviate existing shortages, could function primarily to distribute the water presently used over a longer period, that is, into the later, drier months, rather than to provide additional quantities of water.

There are very few existing storage facilities for irrigation purposes in the basin. The State Engineer has only 20 water rights on file for irrigation reservoirs totaling 3,930 acre-feet. The largest reservoir right is for 2,300 acre-feet; all others are under 500 acre-feet.





# STATE ENGINEER

WATER RESOURCES DEPARTMENT

P.O. BOX 261

CANYON CITY, OREGON

Contract Contraction

June 6, 1975

97820 • Phone 575-011

FILE NO.

TOM McCALL GOVERNOR CHRIS L. WHEELER State Engineer

> Mr. Welter N. Perry State Engineer's Office 1178 Chemekets St. N.E. Salem, Oregon 97310

#### Dear Newt;

.cc: . Dave Childs

In snswer to a call from Dave Childs on May 28th, I arrived at his home at 1230 on June 2nd. We discussed the nature of Rock Creek and the water rights on Rock Creek. At 1600, we drove down to Rock Creek and looked at his weir on his ditch. His right calls for 1.6 cfs in his ditch, and he was receiving only 1.19 cfs. Since there are many upstream users pumping with later priority dates, weter could have been acquired to meet his right. At Mr. Child's request, I did not shut anybody off. Instead, I measured the flow of the creek at various points to try to document the behavior of the creek at low flows.

For most of its length, the creek is incised into the Columbia River basalts. There are long stretches of gravel and alluvium beds between outcrops of the bedrock basalt. Because of this, the surface flow of the stream varies, higher on the bedrock outcrops, and lower on the gravel stretches. My measurements and their locations are as follows:

T. R. Section Forty-scre tract Discharge. Date

| 1112 | N.<br>N.<br>S. | 19<br>20<br>21<br>21<br>22 | EEEEE. | 11<br>15<br>30<br>10 | i<br>agir | SWISEI<br>NWINEI<br>SWISEI<br>NWINEI<br>SWISEI | Mc Donald<br>R.C. 3t Atron<br>CHILDS<br>CRUMS |          | 4.2.55 | cfs<br>cfs<br>cfs<br>cfs<br>cfs | June<br>June<br>June<br>June | 2,2,3,3,3 | 1975<br>1975<br>1975<br>1975 |
|------|----------------|----------------------------|--------|----------------------|-----------|--|---|----------|--------|---------------------------------|------------------------------|-----------|------------------------------|
| 2    | S.             | 22                         | E.     | <br>9                | 1.4       | SWASEA   | TPetty John .                                 | r. +*` • | 7.1    | cfs                             | June                         | 3,        | 197                          |

I will get the flow at Cayuse Canyon on my next measuring trip.

Bob Main Watermaster, Dist.#4

FXHIBIT

## DRAFT

### STATE OF OREGON

#### CERTIFICATE OF WATER RIGHT

THIS CERTIFICATE ISSUED TO

STATE OF OREGON WATER RESOURCES DEPARTMENT SALEM, OREGON 97310

The specific limits for the use are listed below along with conditions of use.

Source: ROCK CR tributary to JOHN DAY R

County: GILLIAM

Purpose: UPSTREAM PASSAGE OF ADULT AND JUVENILE FISH INCLUDING SUMMER STEELHEAD AND RESIDENT RAINBOW TROUT

To be maintained in:

ROCK CREEK FROM USGS GAGING STATION AT WHITE PARK RM 40.0 (NESW, SECTION 36, T3S, R22E); TO THE MOUTH OF ROCK CREEK RM 0.0 (NESW, SECTION 11, T1N, R19E)

The right is established under Oregon Revised Statutes 537.341.

The date of priority is 3/21/90.

The following conditions apply to the use of water under this certificate:

 The right is limited to not more than the amounts, in cubic feet per second, during the time periods listed below:

 JAN
 FEB
 MAR
 APR
 MAY
 JUN
 JUL
 AUG
 SEP
 OCT
 NOV
 DEC

 34
 57
 57
 57
 57
 11
 1.7
 3.09
 2.47
 2.72
 6.67
 21.8

 33.10
 12.10
 3.14
 3.74
 3.24
 3.24
 9.61
 19,10

- The water right holder shall measure and report the in-stream flow along the reach of the stream or river described in the certificate as may be required by the standards for in-stream
- 3. For purposes of water distribution, this instream right shall not have priority over human or livestock consumption.

water right reporting of the Water Resources Commission.

- The instream flow allocated pursuant to this water right is not in addition to other instream flows created by a prior water right or designated minimum perennial stream flow.
- The flows are to be measured at the lower end of the stream reach to protect necessary flows throughout the reach.

Witness the signature of the Water Resources Director affixed this 1st day of \_\_\_\_\_, 19\_\_\_.

### Water Resources Director

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Recorded in State Record of Water Right Certificate number \_\_\_\_\_.

IS70863

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Oregon Water Resources Department Water Rights/Adjudication Section Water Right Application Number: IS 70251 Proposed Final Order

Summary of Recommendation: The Department recommends that the attached draft certificate be issued with conditions.

#### Application History

On 3/21/90, the Oregon Department of Fish and Wildlife submitted an application to the Department for the following instream water right certificate.

ROCK CR tributary to JOHN DAY R Source:

GILLIAM County:

UPSTREAM PASSAGE OF ADULT AND JUVENILE FISH INCLUDING Purpose: SUMMER STEELHEAD AND RESIDENT RAINBOW TROUT

The amount of water (in cubic feet per second) requested by month:

JANFEBMARAPRMAYJUNJULAUGSEPOCTNOVDEC1st½34.057.057.057.034.034.034.034.034.034.034.034.02nd½34.057.057.057.057.034.034.034.034.034.034.034.0

To be maintained in:

ROCK CREEK FROM USGS GAGING STATION AT WHITE PARK RM 40.0 (NESW, SECTION 36, T3S, R22E); TO THE MOUTH OF ROCK CREEK RM 0.0 (NESW, SECTION 11, T1N, R19E)

The Department mailed the applicant notice of its Technical Review on November 25, 1995, determining that the requested flows exceeded the estimated average natural flow during some months but that flows at a reduced amount, with exceptions for human and livestock consumption, are appropriate. The objection period closed February 1, 1995. Objections and comments were received (from A DAVID CHILDS, OREGON DEPT OF FISH AND WILDLIFE, WATER FOR LIFE, WATERWATCH OF OREGON) .

The following supporting data was submitted by the applicant:

- Engineering determined by using USGS data and passage facility (a) design.
- A letter dated April 5, 1996, stating that the flows requested (b) in this application are the minimum amount necessary to restore, protect and enhance populations and habitats of native wildlife species at self-sustaining levels

In reviewing applications, the Department may consider any relevant sources of information, including the following:

- comments by or consultation with another state agency
- any applicable basin program
- any applicable comprehensive plan or zoning ordinance
- the amount of water available
- the proposed rate of use
- pending senior applications and existing water rights of record
- the Scenic Waterway requirements of ORS 390.835
- applicable statutes, administrative rules, and case law '
- any comments received

An assessment with respect to conditions previously imposed on other instream water rights granted for the same source has been completed.

An evaluation of the information received from the local government(s) regarding the compatibility of the proposed instream water use with land use plans and regulations has been completed.

The level of instream flow requested is based on the methods of determining instream flow needs that have been approved by administrative rule of the agency submitting this application.

#### Findings of Fact

The John Day Basin Program allows the proposed use.

Senior water rights exist on this source or on downstream waters.

The source of water is not above a State Scenic Waterway.

The source of water is not withdrawn from appropriation by order of the State Engineer or legislatively withdrawn by ORS 538.

The estimated average natural flow for the lower end of the requested reach is as follows (in cubic feet per second):

| JAN  | FEB  | MAR | APR | MAY  | JUN  | JUL | AUG  | SEP  | OCT  | NOV  | DEC  |
|------|------|-----|-----|------|------|-----|------|------|------|------|------|
| 36.0 | 77.7 | 125 | 116 | 32.0 | 11.0 | 4.7 | 3.09 | 2.47 | 2.72 | 6.67 | 21.8 |

Water is NOT available for further appropriation (at a 50 percent exceedance probability) for the period May, June, July, August, September, October, Straight November and December.

Model The flows available for further appropriation are shown below:

not a JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC 35.82 77.5 123.8 110.8 24.22 1.53 -8.0 -7.41 -4.57 -0.43 6.48 2L& Complete analysis W/adjustments to fit + data points.

#### Conclusions of Law

Under the provisions of ORS 537.153, the Department must

presume that a proposed use will not impair or be detrimental to the public interest if the proposed use is allowed in the applicable basin program established pursuant to ORS 536.300 and 536.340 or given a preference under ORS 536.310(12), if water is available, if the proposed use will not injure other water rights and if the proposed use complied with rules of the Water Resources Commission.

The proposed use requested in this application is allowed in the John Day Basin Plan.

No preference for this use is granted under the provisions of ORS 536.310(12).

The proposed use will not injure other water rights.

The proposed use complies with rules of the Water Resources Commission.

The proposed use complies with the State Agency Agreement for land use.

The proposed instream flows do not fully appropriate this source of water year round. Water is available for additional storage.

While the proposed use meets the other tests, the full amount of water requested is not available during some months of the year.

Water is not available for the proposed use at the amount requested during May, June, July, August, September, October, November and December because the unappropriated water available is less than the amounts requested during these months.

For these reasons, the presumption set forth in ORS 537.153, as discussed above, has not been established. The application therefore has been processed without the statutory presumption.

"When instream water rights are set at levels which exceed current unappropriated water available the water right not only protects remaining supplies from future appropriation but establishes a management objective for achieving the amounts of instream flows necessary to support the identified public uses." OAR 690-77-015(2).

"The amount of appropriation for out-of-stream purposes shall not be a factor in determining the amount of an instream water right." "The amount allowed during any time period for the water right shall not exceed the estimated average natural flow ..." (excerpted from OAR 690-77-015 (3) and (4)).

Because the proposed use exceeds the available water, it can not be presumed to be in the public interest. However, under the direction of OAR 690-77-015 (2)(3) and(4), the proposed use is in the public interest up to the limits of the estimated average natural flow.

Oregon law allows certain uses of water to take precedence over other uses in certain circumstances. When proposed uses of water are insufficient for all who desire to use them, preference shall be given to human consumption purposes over all other uses and for livestock consumption over any other use (excerpted from ORS 536.310 (12)).

The Department therefore concludes that

- the proposed use, as limited in the draft certificate, will not result in injury to other water rights,
  the proposed use, as limited in the draft certificate, will
- the proposed use, as limited in the draft certificate, will not impair or be detrimental to the public interest as provided in ORS 537.170.
- the proposed use, as limited in the draft certificate, for purposes of water distribution, this instream right shall not have priority over human or livestock consumption.
- the flows are to be measured at the lower end of the stream reach to protect necessary flows throughout the reach.
- the stream flows listed below represent the minimum flows necessary to support the public use.

JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC AT 21 4-7 3.09 2.47 33.10 13.00 3.69 2.39 2.34 34 57 57 57 2.72 6.67 21.8 3.24 9.61 19.40 Recommendation

36.10 78 123 75.60 33.10 12.60 3.69 2.29 2.24 3.26 8.61 19.10 The Department recommends that the attached draft certificate be 0.3 issued with conditions.

DATED AUGUST 20, 1996

Steven P. Applegate Administrator Water Rights and Adjudications Division

#### Protest Rights

Under the provisions of ORS 537.153(6) or 537.621(7), you have the right to submit a protest against this proposed final order. Your protest must be in writing, and must include the following:

- Your name, address, and telephone number;
- A description of your interest in the proposed final order, and, if you claim to represent the public interest, a precise statement of the public interest represented;
- A detailed description of how the action proposed in this proposed final order would impair or be detrimental to your interest;
- A detailed description of how the proposed final order is in error or deficient, and how to correct the alleged error or deficiency;



70251



# FEB 1 4 1995

SALEM, OREGON

A David Childs 1806 Thompson St The Dalles, OR 97058 February 10 1995 503/ 298/1499

Mr Mike Mattick Instream Water Rights Water Resources Department Commerce Building 158 12th Street NE Salem, Oregon, 97310-0210

Dear Mike.

Rather than as you suggest, I believe you expressed a strong knowledge of reality. I interpret your remarks of February 1st and your letter, of the 6th as truly remarkable. I have volunteered information many times. But this is a first for WRD (not the first apology, I have another, which I did accept.) You have nothing to apologize for. This was the first time I felt my input was asked for.

I participated in the Advisory committee for The John Day basin plan and also in the State Wide Basin Advisory committee and for the formative years of the Strategic Water Management Group I 've written reams of critique for stream benefit and worked hard for wetted-stream legislation, including being a member of the rule writing committee for instream water rights.)

The answer to your first question is easy, <u>none</u>. The answer to the second question, for the moment, is thanks for asking.

---- "What is truly possible?" What a kind and generous question. The closest I ever got to influencing anyone in modern WRD. happened when I was told, "You had input, we chose not to use it."

I'll send you my answer to your second question, probably by Washington's birthday. Thanks for asking.

I am enclosing a corrected front sheet to my comment-letter of January first. in which I accidentally left out the word 'along'.

Sincerely,

David Childs

aldution correction

DEC

FEB 1 4 1995

WATER MEDICALS DEPT. SALEM, OREGON

A David Childs 1806 Thompson St The Dalles, OR 97058 January 31 1995 503/ 298/1499

Mr Mike Mattick Instream Water Rights Water Resources Department Commerce Building 158 128th Street NE Salem, Oregon, 97310-0210

Dear Mike.

The proposed instream water right, (application No. 70251) for Rock Creek Gilliam County is seriously flawed.

1 / The forty mile stream-reach described for the Instream Water Right is dry for much of its distance during August, September, and October.

2 / The stream reach above The Gage Station is also dry for much of its distance up to the divide during this period.

3./ The period of summer dry-up with no water was about 30 days at our former ranch below French Charlie In the era of 1900.

Interview (1976) and visit with Ethel Sprinkel. She was born on the ranch in 1888, and lived there until 1906. I asked, "When you were here, the creek never went dry did it?" She responded, " It went dry every August for about a month.

My father came to Rock Creek in 1903, lived with his mentor-family, Tip and Mrs Mobley, until 1910. Tip settled on Rock Creek near Olex in 1867. Father ranched In the community until his death in 1946. I was born in 1923 and started fishing with my Dad in 1927. I rode horseback for 3 miles and forded the creek twice each day riding to school at Olex. DAVID CHILDS 1806 Thompson St. The Dalles OR 97058





MR Mike MATTICK Instream Water Rights WATER RESources Department COMMERCE BUILDING 158 12Th STREET NE. SALEM, OR 97310-0210

P.1/4

#### SENT BY FAX AND REGULAR MAIL

January 31, 1995

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Water Resources Department 158 12th Street, NE Salem, OR 97310

RE: Comments; 5 John Day River basin Instream Water Right Technical Reviews; Applications 69960, 70250, 70251, 70263 and 70648.

ODFW has reviewed the subject Technical Reviews and offer the following comments:

#### General Comments

1. ODFW has previously indicated it does not oppose reducing instream water right flow levels from amounts requested to the estimated average natural flow when this is less than requested flows. This is consistent with OAR 690-77-045 (3e).

2. According to OAR 690-77-026 (1), WRD "shall undertake a technical review ... and prepare a report." This subsection further lists 8 [(a) through (h)] mandatory criteria which, at a minimum, must be assessed during the

criteria which, at a minimum, must be assessed during the technical review. ODFW has concerns with the apparent level of assessment relative to subsection (c):

OAR 690-77-026 (1) (c)--Assessing the proposed instream water right with respect to conditions previously imposed on other instream water rights granted for use of water from the same source.

In the subject John Day River basin reports of technical review, WRD is proposing to condition each application to exempt human and livestock consumption from regulation in favor of these instream rights as follows:

This instream right shall not apply to permits for appropriation for domestic or livestock use....



2501 SW First Avenue PO Box 59 Portland, OR 97207 (503) 229-5400 TDD (503) 229-5459 WRD; IWR Comments; John Day River January 30, 1995 Page 2

This instream right shall not have priority over human or livestock consumption.

Instream water rights certificates in the John Day River basin based on conversion of minimum perennial streamflows generally contain similar conditioning language giving preference to the listed uses.

By rule, WRD's technical review process includes <u>assessing</u> conditions previously imposed on other instream water rights from the same source. If found to be appropriate, WRD may propose that new instream water rights contain the same exemption. There is no requirement that this exemption be automatically included as a proposed condition.

When ODFW reviewed WRD files on some of these applications for documentation of assessments of prior conditions, we found nothing to document that any such assessments had been done. ODFW, therefore, assumes the required assessments were not done, contrary to rule. ODFW also objects to the routine placement of exemptions on any of the subject applications on the grounds that to do so does not give adequate consideration to the public's interest in maintaining fishery resources in John Day River basin streams. OAR 690-11-195 (4dA).

#### Specific Comments

Application 70251; Rock Creek; RM 40 to 0--In its water availability analysis, WRD staff find that water is not naturally available to meet even ODFW's recommended <u>minimum</u> flows for fish in May through December. For the months of July through November, the water availability analysis indicates that only about 1/3 of the minimum recommended flow is available. When these calculated flows are compared with other <u>measured</u> flow records, it appears that the estimated average natural flow levels for July through December are potentially erroneous.

The estimated average natural flow and instream water right should be calculated and measured at the mouth of Rock Creek, the downstream limit of this application. Records for USGS gage 14047390 (50% exceedance; 1975-87; RM 40) indicate actual flows (after cumulative withdrawals above) are similar to what WRD staff
WRD; IWR Comments; John Day River January 30, 1995 Page 3

|                                    | JUL | AUG | SEP | OCT | NOV  | DEC  |
|------------------------------------|-----|-----|-----|-----|------|------|
| WRD Water Avail-<br>ability (RM 0) | 4.7 | 3.1 | 2.5 | 2.7 | 6.7  | 21.8 |
| USGS Gage Records<br>(RM 40)       | 2.9 | 1.7 | 2.1 | 3.7 | 11.0 | 30.0 |
| Robison, 1991 (RM<br>40)           | 1.8 | 0.7 | 2.3 | 2.6 | 10.6 | 31.9 |

predict would be naturally available at the mouth of Rock Creek, 40 miles downstream.

The numbers above listed as "Robison, 1991" were extracted from WRD's 1991 Hydrology Report #1, "Water Availability for Oregon's River and Streams: Appendix B". Again, these are natural flow predictions (50% exceedance) for a gage 40 miles upstream from the mouth of Rock Creek, the point of natural flow measurement for the proposed instream water right.

Based on the observation that natural stream flows generally increase as a stream progresses downstream, it is doubtful that the flows cited above accurately represent the instream flow picture.

During physical stream surveys conducted by ODFW personnel in 1971, stream flows in Rock Creek were measured at 1 mile intervals for the lower 9 miles. During this survey, numerous active water diversions were noted. Despite the loss of flow at 22 diversions, measured instream flows (e.g., 4.8 cfs at RM 2) often exceeded the estimated average natural flow.

Although this comparison can not be considered conclusive, ODFW believes significant evidence exists to cast doubt on the results of the water availability analysis performed for this application and is the basis for our objection to same.

Application 70250; Bridge Creek; RM 19 to 13--WRD's water availability analysis indicates water is not naturally available to meet ODFW's recommended minimum flows 10 months out of 12, May through February. There are no gage records available to us for comparison here. We do, however, have limited instream flow measurements taken in July, 1971, that indicated the estimated average natural flow presented in this technical review underestimate natural flow. WRD; IWR Comments; John Day River January 30, 1995 Page 4

The water availability analysis predicts less than one cfs would be available naturally in Bridge Creek during July. ODFW's measurements during July, 1971, recorded a flow at RM 13 of 7.2 cfs after an observed 7 active diversions. Although not conclusive evidence, these measurements, coupled with anecdotal information obtained from field personnel, leads ODFW to believe sufficient doubt exists as to the accuracy of the water availability analysis completed for Bridge Creek.

#### Application 70263; Bear Creek; RM 11 to 0

The situation on the lower 11 miles of Bear Creek is similar to that of Bridge Creek to which it is tributary. Although no gage data exists for comparison, flow measurements taken by ODFW in July, 1971, recorded flows between 2.2 and 6.2 cfs in this stream section. ODFW district personnel indicate that these observed levels of flow are not extraordinary.

Thank you for this opportunity to review the subject technical reports. We appreciate WRD's efforts to move forward with these applications and encourage you to proceed to certification as guickly as possible.

Sincerely,

assunato

Stephanie Burchfield - Water Resources Program Manager Habitat Conservation Division

c. Unterwegner, John Day Lauman/Eddy, La Grande WaterWatch of Oregon (public information request)

File: WRD/Instream Water Right/Communts



## RECEIVED

FEB 0 1 1995

WATER RESOURCES DEP

WATER FOR LIFE'S OBJECTION TO TECHNICAL REVIEW: APPLICATIONS # EN 25 REGON

Submitted to the Oregon Water Resources Department, January 31, 1995

Water for Life hereby submits the following objection to Application # 70251, an instream water right application filed by the Oregon Department of Fish & Wildlife ("ODFW"). Water for Life asserts that the technical review by the Water Resources Department ("WRD' or "Department") is defective and there are elements of the water right as approved that may impair or be detrimental to the public interest, based on the facts and issues set forth below. The applicant has requested flows that exceed the level of flow necessary to support the uses applied for (ORS 537.336 and OAR 690-77-015 (9)). For the reasons set out herein, the application should be rejected or returned to the applicant for the curing of defects.

#### A. WRD FAILED TO ANALYZE FLOW NEEDS

The flow levels approved by the technical review are not based on any analysis of the need for the flows requested. ORS 537.336 sets out the statutory standard which the Department is supposed to follow when determining instream water rights; the "quantity of water necessary to support those public uses." Water for Life asserts this standard means the minimum quantity necessary to support the public use. The technical review does not address the quantity of water or flow levels necessary to support the uses applied for. A review of the WRD file shows that no such analysis has occurred. The only review undertaken by the WRD was a check to see if the requested flows are less than the average estimate natural flow ("EANF"; OAR 690-77-015 (4)). At the very least, the flows approved should not exceed the lesser of EANF or the minimum flow recommended in the Basin Investigations.

#### B. NO SUPPORTING DATA SUBMITTED FOR REQUESTED FLOW LEVELS

An integral part of the technical review by the WRD is the analysis of the application and supporting data (see OAR 690-77-026 (1)(a)). OAR 690-77-015 also requires an application to include at a minimum "a description of the technical data and methods used to determine the requested amount;" (emphasis added).

No analysis of supporting data, or the lack thereof, appears in the WRD file for the application. The technical review is defective in that the WRD did not evaluate "whether the level of instream flow requested is based on the methods for determination of instream flow needs as directed by statute and approved by the administrative rules of the applicant agency." (OAR 690-77-026 (1)(h)).

ODFW does not have specific files for their instream water right applications. The original data supporting the Basin Investigation has apparently been lost or destroyed. Such information is essential to understand and evaluate the requested flows and assess their accuracy. No supporting data or "technical data" was submitted by the applicant as required by OAR 690-77-020 (4). Since no technical data was included with ODFW's application. the application should be returned to the applicant for curing of defects or resubmittal (OAR 690-77-021 and 022).

#### C. OREGON METHOD IS INHERENTLY FLAWED - WRD SHOULD REJECT APPLICATION

The methodology used for this application, the "Oregon Method", is inherently flawed in that it is based on a methodology that has been superseded and is not reliable, and is based on outdated or insufficient information (note testimony of Albert H. Mirati, Jr. on the Oregon Method at the Water Resources Commission, December 6. 1990 meeting).

The Oregon Method was further critiqued in <u>Instream Flow Methodologies</u>, EA Engineering, Science and Technology, Inc. (1986), a publication referenced ODFW's own publication also entitled <u>Instream Flow</u> <u>Methodologies</u>, Louis C. Fredd, Oregon Department of Fish and Wildlife (1989). In that critique at page 10-71, the authors stated:

"The principal limitation is the arbitrariness of the flow criteria. There is no way of knowing if they are necessary or sufficient. The binary velocity and depth criteria are also arbitrary and can result in misleading conclusions. It [Oregon Method] is one of the earliest developments of the concept of depth, velocity, and especially substrate size and dissolved oxygen, but has now been superseded."

The determinations made for the Oregon Method are not reliable and should therefore be rejected by the WRD or the Commission as the final authority in determining the level of instream flows necessary to protect the public use (ORS 537.343).

#### D. OREGON METHOD WAS NOT FOLLOWED TO OBTAIN FLOW LEVELS REQUESTED

One of the requirements of the Department's technical review is contained in OAR 690-77-026 (1)(h): "Evaluating whether the level of instream flow requested is based on the methods for determination of instream flow needs as directed by statute and approved by the administrative rules of the applicant agency." This requirement does not mean the Department can simply accept ODFW's assertion that the "Oregon Method" is the basis for the requested flows. The Department must actively review the application to see if the Oregon Method and ODFW's instream rules are being followed. Where applicable, ODFW must also submit supporting data to show that the standards and criteria contained in their rules have been followed.

The actual measurements used by ODFW to set requested flow levels are totally inadequate to validate those amounts; these measurements were made by ODFW's predecessor, the Oregon State Game Commission, as shown in the Appendices to the Basin Investigations. Actual measurements of streamflow were not made at times when key life stages occurred and, in fact, the severe limitations of the data available show that they are inadequate to validate the requested flows: "Actual measurement of streamflow made at or near recommended instream flow requirements and made at times when key life stages occur are important to validate the methodology use, and to validate that the recommended instream flow requirements provide desirable habitat conditions." Instream Flow Methodologies, Louis C. Fredd, Oregon Department of Fish and Wildlife (1989), p. 12.

#### E. "EANF" CALCULATIONS ARE DEFECTIVE OR INCOMPLETE

There are no calculations or information in the WRD file to show what ratios or models were used or how adjustments were made to determine the 50% exceedance flows, and there is also no information in the technical review to show the type of statistics used (see "Methods for Determining Streamflows and Water Availability in Oregon", <u>Robison</u>, p. 22 and 23.) The EANF calculations are defective, resulting in high EANF levels and thus allowing excessive recommended flows by the WRD. The model used to calculate EANF should be reviewed and revised to properly set EANF figures.

#### F. FISH SPECIES MAY NOT BE PRESENT IN STREAM

The application is defective in that the purpose listed in the application (to provide required stream flows for several different types of fish species) listed fish species that may not be present in the stream. Insufficient information was submitted with the application to determine if the fish species listed in the application are actually present in the stream reach applied for. No supporting data was submitted to show the presence of the listed species as required by ODFW's rules (OAR 635-400-015 (8)(a)).

#### G. "REPORT CONCLUSIONS" CONTAIN BOILERPLATE LANGUAGE

The "Report Conclusions" of the technical review contain boilerplate language apparently agreed upon by the Department and ODFW, some of which is not applicable to this application. There is no information in the application file to indicate the "conclusions" were actually reached as part of the technical review.

#### H. "OPTIMUM FLOW" REQUEST IS CONTRARY TO STATUTORY STANDARD

ODFW applied for the "optimum" flow rates listed Basin Investigation. The statutory standard for instream water rights, however, is the quantity "necessary to support" the public uses allowed (ORS 537.336 (1)), not optimum flows.

The January 1963 South Coast Basin report listed minimum flow amounts in Table D as recommendations to "provide what is considered the basic flows necessary to meet present requirements for anadromous fish passage, spawning, and rearing. These are not considered optimum flows although they may approach optimum in some instances." (South Coast Basin, State Water Resources Board, January 1963, page 73).

When new information was developed from a 1969 survey, the Oregon State Game Commission prepared the April 1972 report (Basin Investigation, also known as "Environmental Investigation"). The new report did modify some minimum flow amounts, and added "recommended optimum flows ... designed to provide instream conditions capable of maintaining an optimum desirable level of natural production." (1972 Environmental Investigation, South Coast Basin, Appendix 2, page 58). It is obvious from the data involved that both EANF and the flows allowed by the technical review are excessive.

The flow rates allowed should be reduced to the minimum flow recommendations of the Basin Investigation or EANF, whichever is less.

#### I. "REACH" REQUESTED IS TOO EXTENSIVE

A significant defect in the application and supporting data that the Department failed to consider concerns the reach of the stream allowed under this instream water right. The flow rates allowed would be applicable to the entire reach requested. This reach is far too long for the flow rates allowed, especially in light of the incoming tributaries between the mouth and the upstream end of the reach (see basin maps). The instream right "shall be approved only if the amount, timing and location serve a public use or uses." OAR 690-77-015 (9).

OAR 690-77-015 (6) states that instream rights "shall, insofar as practical, be defined by reaches of the river rather than points on the river."; OAR 690-77-202 (4)(d) requires that the application shall include the stream "reach delineated by river mile." It is neither practical nor reasonable to approve the same flow rates for the entire reach given the length of the reach applied for, the water available in the stream and the additional tributaries that flow into the stream within the reach.

The stream reach is also excessive according to ODFW's own instream rules. OAR 635-400-015 (11) details the requirements for a specific stream reach. A stream reach is limited to a point where "Streamflow diminishes by at least 30%" (OAR 635-400-015 (11)(B)). OAR 635-400-015 (11)(C) also appears to have been violated since the "stream order" (OAR 635-400-010 (19)) changes within the reach requested due to the incoming tributaries.

The flow requests by ODFW are based on the old Basin Investigations. The Basin Investigations lists the location of the recommended flows in the appendix listing the recommended flows. It is clear that the flow recommendations in the Basin Investigation did not extend upstream and the facts cited above further prove that the reach approved should be limited significantly.

#### J. EXISTING INSTREAM WATER RIGHTS NOT TAKEN INTO ACCOUNT

An instream water right already exists within the reach of the stream at issue in this application. The amount of the existing instream right should be subtracted from any instream right allowed under this application.

OAR 690-77-015 (10) requires that the "combination of instream rights, for the same reach or lake, shall not exceed the amount needed to provide increased public benefits and shall be consistent with (4) and (5) above. Subsection (4) of that section deals with the "EANF" determination; the existing rights were also not accounted for in that calculation. See also OAR 690-77-015 (9).

If the existing instream water right is not subtracted from the approved flow levels, the Department should add a condition to the water right as follows: "The instream flow allocated pursuant to this water right is not in addition to any other instream water rights with a senior priority date and is not in addition to a designated minimum perennial stream flow."

#### K. ODFW'S GAGE RULE NOT FOLLOWED

The application fails to abide by another rule applicable to ODFW's instream applications, OAR 635-400-015 (10)(a). This rule requires ODFW to compare hydrological estimates or gaging data to the amount of water they request for instream flows ("instream flow requirements"). A specific evaluation is set out in subsection (10)(b) regarding appropriate levels for any given time period in relation to the naturally occurring stream flows. ODFW never performed this evaluation for the application.

#### CONCLUSION

This objection is filed in accordance with OAR 690-77-028. The issues raised should be considered as part of a contested case hearing. The WRD technical review is inadequate and defective and has failed to follow applicable rules. A thorough review of the application is necessary to determine the flow levels necessary to support the public uses applied for.

For the reasons set forth above, the objector asserts the application is defective and should be returned to the applicants. The flow levels requested are excessive and not necessary to support the public uses proposed. Flow levels set at the rates proposed interfere with future maximum economic development. Excessive flow rates for instream water rights represent a wasteful and unreasonable use of the water involved (ORS 537.170). The flow rates approved should be set the minimum quantity necessary to support the public use applied for.

Todd Heidgerken Executive Director of Water for Life

Hand Delivered

Rue. 2/1/95

January 31, 1995

Oregon Water Resources Department Water Rights Section 158 12th Street NE Salem, Oregon 97310

Re: Technical Reports for: 69960, 70250, 70251, 70263, 70648 ODFW, Instream Applications, John Day River Basin

WaterWatch of Oregon strongly supports the flows <u>requested</u> in the above referenced Oregon Department of Fish and Wildlife applications. These flows are essential for survival of resident salmonids, small-mouth bass, summer steelhead, rainbow trout, and channel catfish. Streamflows are critical to the survival of these fish. By this letter WaterWatch requests copies of any objections filed on these applications.

**WaterWatch** 

In addition, we file the following objections to the water availability analyses in the technical reports pursuant to OAR 690-77-028:

#### The Water Availability Analysis is Defective

Instream water rights are a means for the state to achieve equitable allocation of water and Oregon Statutes place a duty on the state to act in a way that will protect instream flows needed for fish populations. OAR 690-77-015(2), ORS 496.430, OAR 690-410-070(2)(h). The agencies administrative rules require the technical reports to contain an evaluation of the estimated average natural flow (ENAF) available from the proposed source. OAR 690-77-026(1)(g). The rules also state that the amount of appropriation for out of stream uses is not a factor in determining the amount protected under the instream water right. OAR 690-77-015(3).

However, the technical reports state that they contain an:

"evaluation of the estimated average natural flow available from the proposed source during the time(s) and in the amounts requested in the application . . . The recommended flows take into consideration planned uses and reasonable anticipated future demands for water from the source for agricultural and other uses as required by the standards for public interest review . . ."

Technical reports page 2 (emphasis added). Clearly, this analysis is contrary to the agencies rules because it takes into account out-of-stream uses. These instream water right application requests must be evaluated according to the higher ENAF figures.

#### Water Resources Department Page 2

The technical reports propose to issue instream water rights for the Department's lower "average flows" rather than those requested for several months of each year. The flows requested by ODFW are necessary for the requested beneficial use of water - fish life. These flows are needed for migration, spawning, egg incubation, fry emergence and juvenile rearing and for fish passage and habitat maintenance. There should be no reduction in the requested flows. ODFW's flow requests are either within the ENAF or are needed to account for high flow events that are needed for fish passage and habitat maintenance pursuant to OAR 690-77-015(4).

#### The proposed conditions are contrary to the public interest.

The technical reports propose to subordinate these instream flow requests to human consumption or livestock. The technical reports do not provide any support or reasoning behind its proposal. These uses, while they use small amounts of water individually, have cumulative adverse effects on streamflows needed for fish.

Streamflows are not only critical for fish survival, they help abate water quality problems. The Department of Environmental Quality (DEQ) has designated a segment of the John Day as water quality limited. The river is not able to support the designated beneficial use of aquatic life. Rivers can not assimilate pollution loadings unless there is sufficient water instream. Thus, streamflow protection is critical to pollution abatement.

These proposed conditions are contrary to the public interest in protecting the resource. The Commission's statewide policies recognize the importance of maintaining streamflows and place high priority on protecting streamflows. OAR 690-410-030(1). This policy directs the state to take action to restore flows in critical areas such as this system. Id. The public uses of the this river system have been impaired. Adoption of these instream water rights without conditions is just one small step towards restoring this system.

Adoption of these and other instream flows is critical to the health of Oregon's watersheds and must be a high priority for Oregon if the state is to develop solutions to the resource crises that threatens to destroy the livability of Oregon. Instream water rights not only help to achieve a more equitable allocation of water between instream and out of stream uses, they also establish management objectives for Oregon's rivers. WaterWatch supports the Department's efforts to finally begin to implement an Act that has been "on the books" for the past six years. We look forward to the adoption of these instream water rights.

Sincerely Kimberley Priestley Legal/Policy Analyst

#### COPY CHECK-OFF SHEET FOR INSTREAM TECHNICAL REVIEWS

CC: FILE # WATERWATCH ODF&W (DEPENDING ON - IF NOT APPLICANT) COUNTY (IES): Gilliam WATERMASTER # 4 REGIONAL MANAGER - NC KEN STAHR 1 David childe, 1806 Thompson St. The Dollar, OR 27058 OTHER ADDRESSES: (OVER FOR MORE ADDRESSES) AGRICULTURE, DEPARTMENT OF, VES GARNER BOYER, JOHN, JR. COALITION FOR REPONSIBLE WATER PLANNING COOS COUNTY BOARD OF COMMISSIONERS, GORDON ROSS (COOS RIVER BASIN ONLY) CROOK COUNTY STOCKGROWERS ASSOC., JEFF & RUNINDA MCCORMACK DEPARTMENT OF ENVIRONMENTAL QUALITY DOUGLAS COUNTY LIVESTOCK ASSOCIATION 10/24 mm ORIGINAL TO APPLICANT 10/14/94 CASEWORKER

### COPY CHECK-OFF SHEET FOR **INSTREAM TECHNICAL REVIEWS** OTHER ADDRESSES:

F. A. I. R.

FRUIT GROWERS LEAGUE

HURRICANE CREEK IRRIGATION DITCH CORPORATION, RICHARD A. BOUCHER, SEC./TREAS. ILLINOIS VALLEY WATER RIGHT OWNERS ASSOC. LAKE COUNTY STOCKGROWERS, ANN TRACY, PRESIDENT MORROW COUNTY COMMISSIONER, RAY FRENCH MOON, DAVID, ATTORNEY OREGON ASSOCIATION OF NURSERYMEN, INC., CLAYTON W. HANNON, EXECUTIVE DIRECTOR OREGON ASSOCIATION OF REALTORS, JERRY SCHMIDT, WATER CONSULTANT OREGON CATTLEMEN'S ASSOC. OREGON HOP GROWERS ASSOC. OREGON SHEEP GROWERS ASSOCIATION, INC. OREGON WHEAT GROWERS LEAGUE, MACK KERNS WALLOWA COUNTY COURT, OFFICE OF THE JUDGE WALLOWA COUNTY STOCKGROWERS ASSOC., C/O JEAN STUBBLEFIELD, SECRETARY WATER FOR LIFE WATER RESOURCES CONGRESS

2 .

Revised: 10/14/94 Poul Bates Gillion County SWCD, POBox 106, Condon, OR 97823 Joe Rietmann, Morrow SWCD, POBox 127, Heppener, OR 27836

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Oregon

NOV 1 6 1994 NATER RESOURCES DEPT. SALEM, OREGON



DEPARTMENT OF

FISH AND

WILDLIFE

HABITAT CONSERVATION DIVISION

November 15, 1994

Mike Mattick Water Resources Department 158 12th Street, NE Salem, OR 97310

RE: Instream Water Right 70251; supporting information

Dear Mike:

Attached is the subject material you requested. Hopefully it will serve to support our application for sufficient water to operate the fishway at Harper Dam on Rock Creek (John Day River).

Sincerely,

Aunt

Albert H. Mirati, Jr. Fish Passage Coordinator

c: Burchfield



2501 SW First Avenue PO Box 59 Portland, OR 97207 (503) 229-6967





Koor VL, pur ony

WR 20251

UNITED STATES DEPARTMENT OF COMMERCE

National Oceanic and Atmospheric Administration NATIONAL MARINE FISHERIES SERVICE ENVIRONMENTAL & TECHNICAL SERVICES DIVISION 1002 NE HOLLADAY STREET - ROOM 620 PORTLAND, OREGON 97232 503/230-5400

January 24, 1990

NOV 1 6 1994

RECEIVED

NATER RESOURCES DEPT. F/NWRALEM, OREGON

Sharon Convers Oregon Department of Fish and Wildlife 506 S.W. Mill Street P.O. Box 59 Portland Or. 97207

Dear Ms. Convers,

Attached is the functional design for the Harper Dam Fishway on Rock Creek (Enclosed). This is the second fishway of a series of upwards of 6 that is needed to insure safe and efficient adult anadromous fish passage into the upper basin of Rock Creek in the John Day River Basin. It is our understanding that the Oregon Department of Fish and Wildlife (ODFW) plans to construct the Harper Fishway during the summer of 1990 with funds carried over from FY89.

As you recall the National Marine Fisheries Service (NMFS) volunteered to help design the first couple of fishways to expedited the project. The first fishway at Ramsey Dam was designed by NMFS last September and ODFW personnel constructed it in October.

Please have your engineering staff review the enclosed functional design for the Harper Fishway. Detailed structural design is required before construction can begin on this fishway. The NMFS is not prepared to do the structural design for the Harper Dam site so the ODFW will need to either do the structural design or contract it out to a private engineering firm. As nearly \$18,000 in engineering related funding was provided to ODFW by NMFS for this project, the design costs should be covered.

Technical comments or questions on the design should be directed to Mr. Randy Lee at 230-5411. Any other comments or questions can be directed to Mr. Mike Delarm of my staff at 230-5412. We look forward to moving ahead with this project.

Sincerel

Robert Z./Smith Director, Columbia River Fisheries Development Program



## RECEIVED

Harper Dam Fishway Rock Creek John Day River Basin NOV 1 6 1994 NATER RESOURCES DEPT. SALEM, OREGON

#### Background

Rock Creek enters the John Day River at river mile 21.6. The Oregon Department of Fish and Wildlife (ODFW) personnel indicated that 75 miles of habitat would be opened by correcting passage problems on Rock Creek. According to ODFW, steelhead is the only species of anadromous fish which utilize the Rock Creek drainage. Steelhead currently utilize the lower 25 miles of the creek.

There are six irrigation dams within a 20 mile creek reach. The dams are located at creek miles 7 (Ramsey Dam), 19.75 (#2), 23.5 (Irby Dam), 25.5 (Harper Dam), 27 (McCoin Dam), and 28 (#6). Steelhead passage is entirely blocked at the Harper damsite, but all the other dams probably delay or block*g* passage during low to moderate flows (possibly during higher flows).

In October of 1989, ODFW constructed a fishway designed by the National Marine Fisheries Service (NMFS) at the Ramsey damsite. In general, the fishway consists of two pools with a vertical slot insert placed between the pools.

The following presents a functional design for providing safe and efficient passage of adult steelhead at Harper Dam.

Harper Dam Fishway Rock Creek John Day River Basin

Summary

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Location: Approximate creek mile 25.5 T2S, R22E, Sec. 5 Gilliam County, Oregon

Fishway type: Vertical Slot Floor slope 1 vertical to 8 horizontal 7 vertical slots with one 15-inch entrance Pool dimensions 6 foot wide by 8 foot long Vertical slot either can be formed concrete or inserts.

| Design | Flows: | 57 | cfs | maximum |
|--------|--------|----|-----|---------|
|        |        | 47 | cfs | normal  |
|        |        | 34 | CÍS | minimum |

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NOV 1 6 1994

NATER RESOURCES DEPT. SALEM, OREGON

#### Hydraulic Design

The proposed fishway at the Harper Dam is a vertical slot type with each slot having a width of one foot. Field surveys by ODFW taken May 4, 1988 indicated a head of approximately 8 feet will need to be managed by the fishway. This results in a fishway with 7 vertical slots and one 15-inch wide entrance to satisfactorily manage the 8 foot drop. Due to cost and space limitations, the fishway proposed is to have a slope of 1 vertical to 8 horizontal and have pool dimensions of 6 foot wide by 8 foot long. This is considered to be minimum dimensions for this type of fishway. Vertical slots can be either formed concrete or fabricated metal inserts which may be constructed offsite and installed in the flume when completed.

It is expected that adult steelhead will be present during the months of February through May, therefore, the fishway is designed to accomodate passage during this period. Design flows for the fishway are as follows: 57 cubic feet per second (cfs) maximum, 47 cfs normal and 34 cfs minimum. From high water marks, there appears to be 4 feet of head over the dam crest. Using the standard weir formula, this converts to a streamflow of approximately 1259 cfs. At this streamflow the effectiveness of the fishway entrance flow to attract fish is negligible without auxiliary water, however, at this high streamflow it appears fish may choose to pass over the dam or wait and use the fishway when streamflows subside.

Stoplogs at the entrance are utilized to control the discharge from the fishway. To increase operational flexibility and ease of adjustments, a gate may be considered. Adjustments to the logs or gate will be necessary to insure a hydraulic drop of 1.25 feet across the entrance. This will result in and entrance jet velocity of approximately 9 feet per second. A short flow deflecting wall is constructed between the entrance pool and the first slot upstream from the fishway entrance. The purpose of this wall is to dissipate the energy from the oncoming jet. Additionally, for dewatering purposes, stoplog slots are located at the exit. A coarse trashrack is also located at the exit. TO allow passage of fish past the trashrack, the spacing between vertical rack bars are 9 inches and the spacing between horizontal members are 2 feet. To facilitate cleaning of debris from the rack, the rack face is set at a slope or 4 vertical to 1 horizontal. To insure safety, it is recommended the fishway be covered by the use of metal walkway grating.

57 MAX TEUS 7 > NORM 37 MIN

| SHEET NO. | TITLE  |
|-----------|--|
| 1         | INDEX TO DRAWINGS  |
| 2         | PLAN   |
| 3         | SECTION  |
| 4         | HYDRAULIC PROFILE  |
| 5         | DETAILS  |
|           | PRELIMINARY<br>FOR REVIEW  |
|           | NATIONAL MARINE FISHERIES SERVICE<br>1002 NE HOLLADAY STREET - RM 620<br>PORTLAND. OREGON 97232<br>HARPER DAM FISHWAY<br>INDEX TO DRAWINGS |
|           |  |











W A T E R R E S O U R C E S D E P A R T M E N T

August 13, 1991

A. David Childs 1806 Thompson St. The Dalles, Oregon 97058

Re: Instream Water Right Application 70251

Dear Dave;

I have received your letter asking for a review of the Rock Creek instream water right application and have forwarded it, along with a copy of this response, to Lorna Stickel.

At this point we are in agreement that the flows requested by ODFW may be too high during a portion of the year. The certificate for this application will not be issued pending resolution of this flow issue. The stream flow analysis has not yet been shared with ODFW. You will be notified of any modification of the proposal based on this information.

The Department's current course of action on instream water right applications is to attempt to resolve all issues on a basin by basin basis. We are currently focusing on the North Coast Basin. We have not prioritized the rest of the state for subsequent activity. However, there may be good reason to address either the Sandy or Umpgua Basins next.

You will be notified of any proposed resolution of the Rock Creek flow issue prior to final action on the application.

Sincerely, milar J. Mattick

MICHAEL J. MATTICK Water Rights Specialist

MJM:

cc: Lorna Stickel Laura Pryor, Gilliam County Judge Al Mirati, ODFW



3850 Portland Rd NE Salem, OR 97310 (503) 378-3739 FAX (503) 378-8130

# RECEIVED

AUG 1 2 1991 WATER RESOURCES DEPT. SALEM, OREGON A David Childs 1806 Thompson St July 31, 1991 The Dalles, OR 97058 (503) 298- 1499

Lorna Stickel Chairman Water Resources Commission Attn, Mr Mike Mattick Instream Water Rights Water Resources Department 3850 Portland Road NE. Salem, Oregon, 97310

Dear Mike.

I am writing to ask that the instream water right , application No. 70251 on Rock Creek Gilliam county, be reviewed.

George Robison's, hydrologist's model predicts "natural' flows of only three to 10 percent of those asked for, during several months in the application flow and time frame.

1/ The stream-reach described in the Instream Water Right is dry for most of its distance during July, August, September, and October,.

2/ The stream-reach above The Gage Station is also dry for most of its distance during this period. There is no water coming down stream to the gage. There is no water in the watershed, above the gage, during the critical period, other than from convection storms and a few areas of springs and drying trickles in the headwaters.

3./ There is no water during the critical time-frame. Fish are not in the described stream reach other than in areas of spring fed water surfacing from basalt aquifers. Springs have for centuries been the lifesupport system for downstream fish. The upstream dry-up is a last-40year happening. 4 / The period of summer dry-up with no water for fish and no water for irrigation was only about 30 days annually a century ago. The dry period has lengthened over the years to become five to seven months.

However the ODFW asked for IWR, flows during July through October are not now nor have they ever been available from Rock Creek's watershed, this is not a function of down stream irrigation but a function of upstream watershed condition.

This has also been the historic pattern, however, it has been amplified in the upper watershed by practices that have speeded winter water from the watershed via excessive surface runoff. It has been amplified in the lower watershed by the change from flood irrigation and alluvial recharge to a system with a preponderance of sprinkler irrigation and little alluvial recharge.

The seed-stock for anadromous and resident fish have developed in tune with the nonpassage system of the natural summer dry-up for many centuries it can not be changed by numbers. The numbers were never there.

. Simply building a fish-way designed for 34 cfs for a time-period that has not, by any measure, ran over 2 cfs, will not restore the fishery or the aquatic resource. Rather it will create false hopes and wasteful priority of funding. The enhancement of the stream and restoration of the fishery is possible but this means, setting 34 cfs IWR, will only extend the delay and weaken the chances for recovery. Needed is a responsible diagnosis of the aquatic ills of the stream.

Since Rock Creek Gilliam county has been thoroughly researched by the Water Resources Department, it would seem prudent to use that evaluation in setting the flows for instream water rights. The stream flow data has been published. The recording gages were result of coordination between local people and the Water Resource Department.

I object to the proposed flows. They are not attainable, never were there, and send us down the wrong track to recover this stream.

I'm available should you find it desirable to discuss this further.

I have enclosed a copy of a portion of comments to the Umatilla National Forest dealing with Rock Creek Gilliam and Morrow County. Thank you for your consideration.

Sincerely,

Jan Phild

David Childs

Copy to Laura Pryor, Gilliam County Judge

Enclosures:

1/Description of Rock Creek -Letter to Forest Supervisor

2/ Flow data 1966 - 1989 The gage site was changed in 1976.

3/ TRIBUTORY Flaw data to GAGE for IWR

#### INTEROFFICE MEMORANDUM Water Rights Section



FROM: Dwight French, x268

DATE: March 26, 1997

RE: Water Availability for ISWR applications/files

You asked about the file copies of Estimated Average Natural Flow (EANF) for ISWR applications.

There is not a printout in each file similar to what you would generally see in an out of stream application file. The EANF information is in either the Technical Review (TR) or Initial Review (IR) as well as the Proposed Final Order (PFO).

During the processing of the ISWR applications, Rick Cooper and/or Ken Stahr would provide us with a electronic copy of the water availability information for a particular group of ISWR applications. We would then cut and paste that information directly into the TR or IR. When preparing the PFO, we would cut and paste from the TR or IR directly into the PFO.

In summary, our EANF numbers are in the TR or IR and the PFO for each particular ISWR application file.

cc: Mike Mattick

All Protested ISWR Files

# Altern Applications with Protests

| Basin          | App Num              |   |  |
|----------------|----------------------|---|--|
| 2              |                      |   |  |
|                | o <sup>K</sup> 71556 | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
| tal for Basin  | 2: 1                 |   |  |
| 4              |                      |   |  |
|                | <b>6</b> 71793       | w | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | ok 71798             | w | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 72076                | W | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 72077                | W | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 72078                | W | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 72079                | W | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 72080                | W | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 72081                | W | OREGON DEPARTMENT OF FISH & WILDLIFE         |
| otal for Basin | 4: 8                 |   |  |
| 5              |                      |   |  |
|                | JL 70353             | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 1 70354              | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | DK 70357             | A | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 70358                | S | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 70358                | S | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 1 70358              | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 0K 70605             | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 70606                | S | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 1 70606              | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 70612                | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 70695                | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | 70695                | А | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                | j 73199              | A | OREGON DEPARTMENT OF FISH & WILDLIFE         |
| tal for Basin  | 5: 13                |   |  |
| 6              |                      |   |  |
|                | 69949                | А | OREGON DEPARTMENT OF FISH & WILDLIFE & PARKS |
| 16             | t v 69949            | S | OREGON DEPARTMENT OF FISH & WILDLIFE & PARK  |
| yere o         | 69951                | S | OREGON DEPARTMENT OF FISH & WILDLIFE & PARK  |
| ULU P          | 69951                | А | OREGON DEPARTMENT OF FISH & WILDLIFE & PARK  |
|                | 69958                | S | OREGON DEPARTMENT OF FISH & WILDLIFE & PARK  |
|                | 69958                | А | OREGON DEPARTMENT OF FISH & WILDLIFE & PARK  |
|                | 69958                | S | OREGON DEPARTMENT OF FISH & WILDLIFE & PARK  |

4

89

18

74

2-3992

12

12

69959

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OREGON DEPARTMENT OF FISH & WILDLIFE & PARKS

| astrea | m | App | ollcations | with | Protests |
|--------|---|-----|------------|------|----------|
| 4/2/97 | • |     | •          |      |          |

| Basin           | App Num   |            |
|-----------------|-----------|------------|
| 6               |           | A STATE OF |
|                 | 69959     | S          |
|                 | 69959     | А          |
|                 | 69961     | А          |
|                 | 69961     | S          |
|                 | 69961     | S          |
|                 | 69963     | А          |
|                 | 69963     | S          |
|                 | 69963     | А          |
|                 | OK 70251  | A          |
|                 | OK 70589  | А          |
|                 | 70640     | S          |
|                 | 70640     | А          |
|                 | 70641     | А          |
|                 | .) 70641  | S          |
|                 | 70642     | А          |
|                 | 1 70642   | S          |
|                 | 0 K 70645 | А          |
|                 | 70645     | S          |
|                 | 70646     | S          |
|                 | 70646     | A          |
|                 | 70651     | S          |
|                 | 70651     | A          |
|                 | 70652     | A          |
|                 | 70652     | S          |
|                 | 70653     | S          |
|                 | 70653     | A          |
|                 | 70654     | S          |
|                 | 70654     | A          |
|                 | 70655     | S          |
|                 | 70655 ــز | A          |
| Total for Basin | 6: 38     |            |
| 9               |           |            |
|                 | 70863     | А          |
|                 | 70864     | А          |
|                 | 70870     | A          |

72163

72168

A

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#### Instream Applications with Protests 4/2/97

| Basin           | App Num              |     |  |
|-----------------|----------------------|-----|--|
| 9               |                      |     |  |
|                 | 72168                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72169                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72169                | S   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72170                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72173                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72181                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72186                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72187                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72188                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72191                | А   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 72194                | А   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
| Total for Basin | 9: 16                |     |  |
| 10              |                      |     |  |
|                 | 71450                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 71455                | S   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 71455                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
| Total for Basin | 10: 3                |     |  |
| 11              | - Hwell              |     |  |
| Dwight          | D <sup>61</sup> 7002 | A   | OREGON DEPARTMENT OF FISH & WILDLIFE & PARKS |
| Total for Basin | 11: 1                |     |  |
| 12              |                      |     | 1  |
|                 | 71467                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 71468                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 71472                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
| Total for Basin | 12: 3                |     |  |
| 13              |                      |     |  |
|                 | 70486                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70487                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70656                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70657                | А   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70658                | А   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70659                | А   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70662                | Α · | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70663                | A   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
|                 | 70664                | А   | OREGON DEPARTMENT OF FISH & WILDLIFE         |
| Total for Basin | 13: 9                |     |  |

Page 3 of 6

#### Instream Applications with Protests 4/2/97 .

| Basin | App Num    |   |        |
|-------|------------|---|--------|
| 14    |            |   |        |
|       | 70094      | А | OREGON |
|       | Duff 70094 | А | OREGON |
|       | y70094     | А | OREGON |
|       | 70798      | S | OREGON |
|       | 70798      | А | OREGON |
|       | 70799      | А | OREGON |
|       | 70799      | S | OREGON |
|       | 70800      | А | OREGON |
|       | 70800      | S | OREGON |
|       | 70801      | А | OREGON |
|       | 70801      | S | OREGON |
|       | 70802      | А | OREGON |
|       | 70802      | S | OREGON |
|       | 70804      | А | OREGON |
|       | 70804      | S | OREGON |
|       | 70807      | А | OREGON |
|       | 70807      | S | OREGON |
|       | 70807      | S | OREGON |
|       | 70808      | А | OREGON |
|       | 70808      | S | OREGON |
|       | 70809      | А | OREGON |
|       | 70809      | А | OREGON |
|       | 70809      | S | OREGON |
|       | 70812      | А | OREGON |
|       | 70812      | S | OREGON |
|       | 70812      | А | OREGON |
|       | 70812      | А | OREGON |
|       | 70813      | А | OREGON |
|       | 70813      | S | OREGON |
|       | 70813      | А | OREGON |
|       | 70813      | А | OREGON |
|       | 70813      | А | OREGON |
|       | 70815      | A | OREGON |
|       | 70815      | S | OREGON |
|       | 70816      | А | OREGON |
|       | 70816      | S | OREGON |
|       | 70821      | A | OPEGON |

DEPARTMENT OF FISH & WILDLIFE & PARKS DEPARTMENT OF FISH & WILDLIFE & PARKS DEPARTMENT OF FISH & WILDLIFE & PARKS DEPARTMENT OF FISH & WILDLIFE **DEPARTMENT OF FISH & WILDLIFE DEPARTMENT OF FISH & WILDLIFE** DEPARTMENT OF FISH & WILDLIFE DEPARTMENT OF FISH & WILDLIFE **DEPARTMENT OF FISH & WILDLIFE** DEPARTMENT OF FISH & WILDLIFE **DEPARTMENT OF FISH & WILDLIFE DEPARTMENT OF FISH & WILDLIFE** DEPARTMENT OF FISH & WILDLIFE **DEPARTMENT OF FISH & WILDLIFE** DEPARTMENT OF FISH & WILDLIFE **DEPARTMENT OF FISH & WILDLIFE** DEPARTMENT OF FISH & WILDLIFE **DEPARTMENT OF FISH & WILDLIFE** DEPARTMENT OF FISH & WILDLIFE DEPARTMENT OF FISH & WILDLIFE

**OREGON DEPARTMENT OF FISH & WILDLIFE** 

| 2/97<br>Basin |              |   |                                      |
|---------------|--------------|---|--------------------------------------|
| Dasin         | App Num      |   |                                      |
| 14            |              |   |                                      |
|               | 70824        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70826        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70829        | S | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70829        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70829        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70829        | S | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70830        | S | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70830        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70830        | S | OREGON DEPARTMENT OF FISH & WILDLIFE |
| Total for B   | asin 14: 46  | 6 |                                      |
| 15            |              |   |                                      |
|               | 70982        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70993        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 70998        | w | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71008        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71201        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71614        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71622        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 72843        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
| Total for B   | asin 15: 8   |   |                                      |
| 16            |              |   | 1                                    |
|               | 71172        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71173        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71174        | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71181        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71182        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71183        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71184        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71185        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71190        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|               | 71192        | A | OREGON DEPARTMENT OF FISH & WILDLIFF |
|               | 71193        | A | OREGON DEPARTMENT OF FISH & WILDLIFF |
|               | 73350        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
| Total for B   | asin 16 : 11 | 2 |                                      |
| 17            |              |   |                                      |
| 17            | 70000        |   |                                      |
|               | /0228        | A | OREGON DEPARTMENT OF FISH & WILDLIFE |

Instream Applications with Protests

| 4/2/97          | The self |   |                                      |
|-----------------|----------|---|--------------------------------------|
| Basin           | App Num  |   |                                      |
| 17              |          | • |                                      |
|                 | 70229    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70230    | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70348    | S | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70348    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70448    | S | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70448    | A | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70574    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70877    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70891    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
| -               | 70895    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70895    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 70915    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 71697    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
|                 | 80446    | А | OREGON DEPARTMENT OF FISH & WILDLIFE |
| Total for Basin | 17: 15   |   |                                      |
| 172             |          |   |                                      |

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Instream Applications with Protests

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UNITED STATES DEPARTMENT OF THE INTERIOR - GEOLOGICAL SURVEY - OREGON OFFICE 12/04/89

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

DISCHARGE, CUBIC FEET PER SECOND, WATER YEAR OCTOBER 1974 TO SEPTEMBER 1975 MEAN VALUES

| •     |     |     |     |     | ME  | AN VALUES | 5    |     |     |     |     | 5 4M | 1 |
|-------|-----|-----|-----|-----|-----|-----------|------|-----|-----|-----|-----|------|---|
| DAY   | 0CT | NOV |     |     |     |           | APR  | MAY |     |     |     | LITI |   |
| DAT   | 001 | NOV | DEC | JAN | FEB | MAR       | Arts | TAT | JUN | JUL | AUG | SEP  |   |
| 1     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 2     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 3     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 4     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 5     |     |     |     |     |     |           |      |     |     |     |     |      |   |
|       |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 6     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 7     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 8     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 9     |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 10    |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 11    |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 11    |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 13    |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 14    |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 15    |     |     |     |     |     |           |      |     |     |     |     |      |   |
|       |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 16    |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 17    |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 18    |     |     |     |     |     |           |      |     |     |     |     | . 44 |   |
| 19    |     |     |     |     |     |           |      |     |     |     |     | . 40 |   |
| 20    |     |     |     |     |     |           |      |     |     |     |     | . 40 |   |
|       |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 21    |     |     |     |     |     |           |      |     |     |     |     | .40  |   |
| 22    |     |     |     |     |     |           |      |     |     |     |     | . 40 |   |
| 25    |     |     |     |     |     |           |      |     |     |     |     | • 40 |   |
| 25    |     |     |     |     |     |           |      |     |     |     |     | • 30 |   |
|       |     |     |     |     |     |           |      |     |     |     |     |      |   |
| 26    |     |     |     |     |     |           |      |     |     |     |     | .33  |   |
| 27    |     |     |     |     |     |           |      |     |     |     |     | .37  |   |
| 28    |     |     |     |     |     |           |      |     |     |     |     | .40  |   |
| 29    |     |     |     |     |     |           |      |     |     |     |     | .40  |   |
| 30    |     |     |     |     |     |           |      |     |     |     |     | .40  |   |
| 31    |     |     |     |     |     |           |      |     |     |     |     | (/   |   |
|       |     |     |     |     |     |           |      |     |     |     |     |      |   |
| TOTAL |     |     |     |     |     |           |      |     |     |     |     |      |   |
| MEAN  |     |     |     |     |     |           |      |     |     |     |     |      |   |
| MAX   |     |     |     |     |     |           |      |     |     |     |     |      |   |
| MIN   |     |     |     |     |     |           |      |     |     |     |     |      |   |
|       |     |     |     |     |     |           |      |     |     |     |     |      |   |

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON, OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

|                                      |   | DISCHA                                 | RGE, CUBI                              | C FEET PE                              | R SECOND                                  | , WATER Y<br>MEAN VALU            | EAR OCTOBE<br>ES                   | ER 1976 TO                         | ) SEPTEMBE                             | R 1977<br>U.7                    | 309                                    | 2.4                              |
|--------------------------------------|---|--|--|--|---|-----------------------------------|------------------------------------|------------------------------------|--|----------------------------------|--|----------------------------------|
| DAY                                  | ОСТ   | NOV                                    | DEC                                    | JAN                                    | FEB                                       | MAR                               | APR                                | МАҮ                                | JUN                                    | JUL                              | AUG                                    | SEP                              |
| 1<br>2<br>3<br>4<br>5                | 2.4<br>2.4<br>2.1<br>2.1<br>2.3               | 2.8<br>2.8<br>2.8<br>2.8<br>2.8<br>2.8 | 3.8<br>3.9<br>3.9<br>3.8<br>3.8        | 3.9<br>3.9<br>3.8<br>4.1<br>3.3        | 3.9<br>4.1<br>3.9<br>3.9<br>4.1           | 8.3<br>9.0<br>9.0<br>9.0<br>8.3   | 14<br>18<br>20<br>37<br>59         | 4.1<br>4.3<br>4.6<br>5.0<br>5.0    | 7.6<br>7.3<br>7.3<br>6.9<br>6.1        | .51<br>.45<br>.45<br>.57<br>.57  | 20<br>21<br>20<br>20<br>20<br>21       | •11<br>•11<br>•11<br>•11<br>•11  |
| 6<br>7<br>8<br>9<br>10               | 2.3<br>2.1<br>2.1<br>2.1<br>2.1<br>2.1        | 2.8<br>2.9<br>3.0<br>3.0<br>3.0        | 3.6<br>3.8<br>3.8<br>4.1<br>3.9        | 4.0<br>4.1<br>4.0<br>4.0<br>4.7        | 4 • 4<br>4 • 4<br>4 • 4<br>4 • 1<br>4 • 4 | 7.9<br>8.6<br>12<br>16<br>17      | 81<br>71<br>58<br>40<br>31         | 5.3<br>6.9<br>7.3<br>7.3<br>16     | 5.3<br>4.3<br>3.8<br>3.8<br>3.8<br>3.5 | .57<br>.51<br>.40<br>.33<br>.33  | 5.5<br>.36<br>.18<br>.15<br>.14        | .11<br>.10<br>.10<br>.10<br>.10  |
| 11<br>12<br>13<br>14<br>15           | 2.1<br>2.0<br>2.0<br>2.0<br>1.8               | 3.0<br>3.0<br>3.0<br>3.5<br>3.6        | 4.1<br>4.3<br>4.6<br>4.3<br>4.3        | 4.5<br>5.0<br>5.4<br>5.6<br>5.3        | 4.8<br>5.3<br>5.8<br>6.9<br>7.6           | 16<br>14<br>14<br>13<br>11        | 25<br>22<br>19<br>18<br>17         | 45<br>45<br>38<br>28<br>24         | 3.3<br>3.5<br>3.2<br>3.0<br>2.7        | .30<br>.27<br>.27<br>.25<br>.23  | .14<br>.14<br>.12<br>.14<br>.12        | .10<br>.10<br>.10<br>.10<br>.10  |
| 16<br>17<br>18<br>19<br>20           | 2.0<br>2.0<br>2.0<br>2.0<br>2.1               | 3.9<br>3.9<br>4.1<br>4.3<br>4.1        | 4.3<br>4.3<br>4.1<br>3.5<br>3.3        | 5.0<br>5.0<br>5.5<br>5.0<br>5.5        | 7.6<br>7.6<br>7.2<br>6.9<br>6.6           | 9.8<br>10<br>9.4<br>9.8<br>9.0    | 15<br>13<br>12<br>11<br>9.8        | 22<br>21<br>19<br>17<br>15         | 2.3<br>2.4<br>2.0<br>2.0<br>1.8        | .21<br>.21<br>.23<br>.23<br>.20  | .12<br>.11<br>.11<br>.11<br>.11        | .11<br>.11<br>.12<br>.12<br>.14  |
| 21<br>22<br>23<br>24<br>25           | 2.1<br>2.1<br>2.1<br>2.3<br>2.4               | 4 • 1<br>4 • 1<br>4 • 6<br>4 • 6       | 3.4<br>3.4<br>3.3<br>3.5<br>3.8        | 5.3<br>5.0<br>5.0<br>5.0<br>5.0        | 6.6<br>6.6<br>6.3<br>6.3                  | 9.0<br>9.0<br>9.4<br>12<br>13     | 9.4<br>8.3<br>7.3<br>6.3<br>5.8    | 13<br>11<br>11<br>12<br>12         | 1.7<br>1.3<br>.89<br>.99<br>.79        | 20<br>20<br>20<br>20<br>20<br>20 | .11<br>.10<br>.12<br>.15<br>.16        | .14<br>.14<br>.14<br>.15<br>.15  |
| 26<br>27<br>28<br>29<br>30<br>31     | 2.4<br>2.4<br>2.5<br>2.5<br>2.5<br>2.5<br>2.7 | 4.3<br>4.1<br>3.6<br>3.6<br>3.8        | 3.9<br>3.9<br>4.1<br>3.9<br>3.9<br>3.9 | 4.6<br>4.6<br>3.6<br>3.9<br>3.8<br>4.1 | 6.1<br>6.1<br>6.6<br>                     | 13<br>14<br>16<br>16<br>15<br>14  | 5.0<br>4.8<br>4.3<br>4.1<br>3.8    | 12<br>11<br>12<br>11<br>9.4<br>8.3 | .79<br>.63<br>.63<br>.57<br>.57        | 20<br>20<br>18<br>20<br>20<br>20 | .16<br>.15<br>.12<br>.11<br>.12<br>.11 | .15<br>.15<br>.16<br>.18<br>.16  |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>AC-FT | 68.0<br>2.19<br>2.7<br>1.8<br>135             | 106.0<br>3.53<br>4.6<br>2.8<br>210     | 120.5<br>3.89<br>4.6<br>3.3<br>239     | 141.5<br>4.56<br>5.6<br>3.3<br>281     | 159.1<br>5.68<br>7.6<br>3.9<br>316        | 361.5<br>11.7<br>17<br>7.9<br>717 | 649.9<br>21.7<br>81<br>3.8<br>1290 | 462.5<br>14.9<br>45<br>4.1<br>917  | 90.96<br>3.03<br>7.6<br>.57<br>180     | 9.27<br>.30<br>.57<br>.18<br>18  | 9.97 /<br>.32<br>5.5<br>.10<br>20      | 3.68<br>.12<br>.18<br>.10<br>7.3 |

• CAL YR 1976 TOTAL 11019.12 MEAN 30.1 MAX 305 MIN .23 AC-FT 21860 WTR YR 1977 TOTAL 2182.88 MEAN 5.98 MAX 81 MIN .10 AC-FT 4330

UNITED STATES DEPARTMENT OF THE INTERIOR - GEOLOGICAL SURVEY - OREGON OFFICE 12/04/89

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021 3.09

DISCHARGE, CUBIC FEET PER SECOND, WATER YEAR OCTOBER 1975 TO SEPTEMBER 1976 MEAN VALUES 4.7 APR MAY

| DAY                              | ОСТ                                    | NOV                                    | DEC                              | JAN                              | FEB                        | MAR                               | APR                             | MAY                                    | JUN                             | JUL   | AUG                                    | SEP                             |
|----------------------------------|--|--|----------------------------------|----------------------------------|----------------------------|-----------------------------------|---------------------------------|--|---------------------------------|---|--|---------------------------------|
| 1                                | .40                                    | 2.2                                    | 5.6                              | 21                               | 35                         | 50                                | 87                              | 81                                     | 10                              | 1.3   | .27                                    | 3.0                             |
| 2                                | .40                                    | 2.2                                    | 6.0                              | 23                               | 33                         | 34                                | 83                              | 69                                     | 9.8                             | 1.3   | .51                                    | 2.8                             |
| 3                                | .40                                    | 2.3                                    | 7.6                              | 27                               | 30                         | 30                                | 96                              | 56                                     | 9.0                             | 1.1   | .51                                    | 2.7                             |
| 4                                | .45                                    | 2.4                                    | 8.8                              | 32                               | 21                         | 27                                | 106                             | 50                                     | 8.3                             | .99   | .36                                    | 2.5                             |
| 5                                | .45                                    | 2.6                                    | 9.2                              | 36                               | 16                         | 24                                | 149                             | 45                                     | 7.3                             | .99   | .33                                    | 2.3                             |
| 6<br>7<br>8<br>9<br>10           | .57<br>.63<br>.59<br>.57<br>.57        | 2.9<br>3.3<br>3.3<br>3.3<br>3.3<br>3.6 | 8.8<br>10<br>11<br>12<br>11      | 32<br>31<br>129<br>118<br>81     | 14<br>15<br>17<br>21<br>18 | 29<br>30<br>27<br>30<br>36        | 231<br>194<br>194<br>305<br>223 | 41<br>37<br>31<br>28<br>24             | 6.3<br>6.1<br>5.3<br>5.3<br>5.0 | .79<br>.71<br>.89<br>.89<br>.71               | .71<br>20<br>22<br>13<br>8.3           | 2.1<br>1.8<br>1.8<br>1.8<br>1.7 |
| 11<br>12<br>13<br>14<br>15       | .58<br>.56<br>.51<br>.50<br>.50        | 3.9<br>3.9<br>3.9<br>3.9<br>3.9<br>3.9 | 10<br>9.0<br>8.6<br>7.6<br>7.9   | 68<br>58<br>44<br>48<br>113      | 16<br>20<br>22<br>27<br>29 | 40<br>33<br>39<br>40<br>41        | 183<br>159<br>180<br>153<br>143 | 24<br>22<br>17<br>14<br>13             | 4.6<br>4.3<br>3.8<br>3.8<br>3.5 | .63<br>.63<br>.57<br>.51<br>.45               | 6.3<br>4.8<br>4.1<br>5.0<br>6.3        | 1.7<br>1.5<br>1.5<br>1.4<br>2.4 |
| 16                               | .50                                    | 4 • 0                                  | 8.3                              | 236                              | 29                         | 50                                | 129                             | 12                                     | 3.5                             | .45   | 8.3                                    | 3.2                             |
| 17                               | .50                                    | 4 • 0                                  | 8.3                              | 245                              | 48                         | 96                                | 113                             | 11                                     | 3.6                             | .40   | 15                                     | 2.5                             |
| 18                               | .50                                    | 4 • 0                                  | 7.6                              | 183                              | 53                         | 191                               | 113                             | 9.8                                    | 3.5                             | .40   | 9.4                                    | 2.3                             |
| 19                               | .50                                    | 4 • 0                                  | 7.6                              | 121                              | 52                         | 214                               | 101                             | 9.4                                    | 3.0                             | .36   | 8.3                                    | 2.0                             |
| 20                               | .50                                    | 4 • 0                                  | 6.9                              | 92                               | 39                         | 124                               | 116                             | 10                                     | 2.9                             | .36   | 7.3                                    | 2.1                             |
| 21                               | .54                                    | 4 • 0                                  | 6.6                              | 69                               | 32                         | 108                               | 146                             | 11                                     | 2.7                             | .40   | 6.3                                    | 2.1                             |
| 22                               | .58                                    | 4 • 0                                  | 6.6                              | 59                               | 32                         | 106                               | 124                             | 9.0                                    | 2.4                             | .40   | 5.5                                    | 2.5                             |
| 23                               | .68                                    | 4 • 0                                  | 7.3                              | 59                               | 29                         | 101                               | 129                             | 8.3                                    | 2.3                             | .36   | 5.3                                    | 3.0                             |
| 24                               | .79                                    | 4 • 0                                  | 11                               | 48                               | 29                         | 113                               | 124                             | 7.6                                    | 2.3                             | .36   | 5.3                                    | 3.2                             |
| 25                               | 1.0                                    | 4 • 0                                  | 12                               | 38                               | 32                         | 143                               | 108                             | 7.3                                    | 1.8                             | .33   | 5.8                                    | 3.2                             |
| 26<br>27<br>28<br>29<br>30<br>31 | 1.5<br>2.4<br>2.6<br>2.3<br>2.1<br>2.0 | 4.5<br>5.2<br>6.0<br>5.8<br>5.6        | 14<br>53<br>43<br>39<br>61<br>46 | 37<br>36<br>36<br>43<br>41<br>37 | 41<br>56<br>68<br>53<br>   | 103<br>94<br>89<br>77<br>79<br>96 | 101<br>94<br>89<br>94<br>92     | 6.9<br>6.3<br>6.6<br>6.6<br>6.9<br>9.0 | 1.8<br>1.7<br>1.5<br>1.3<br>1.2 | .30<br>.23<br>.23<br>.23<br>.23<br>.23<br>.23 | 6.1<br>5.5<br>5.0<br>4.3<br>3.9<br>3.5 | 3.0<br>2.9<br>2.8<br>2.7<br>2.5 |
| TOTAL                            | 26.67                                  | 114.7                                  | 471.3                            | 2241                             | 927                        | 2294                              | 4159                            | 689.7                                  | 127.9                           | 17.73   | 197.29 25                              | 71.0                            |
| MEAN                             | .86                                    | 3.82                                   | 15.2                             | 72.3                             | 32.0                       | 74.0                              | 139                             | 22.2                                   | 4.26                            | 57  | 6.36                                   | 2.37                            |
| MAX                              | 2.6                                    | 6.0                                    | 61                               | 245                              | 68                         | 214                               | 305                             | 81                                     | 10                              | 1.3   | 22                                     | 3.2                             |
| MIN                              | .40                                    | 2.2                                    | 5.6                              | 21                               | 14                         | 24                                | 83                              | 6.3                                    | 1.2                             | 23  | .27                                    | 1.4                             |
| AC-FT                            | 53                                     | 228                                    | 935                              | 4450                             | 1840                       | 4550                              | 8250                            | 1370                                   | 254                             | 35  | 391                                    | 141                             |

WTR YR 1976 TOTAL 11337.29 MEAN 31.0 MAX 305 MIN .23 AC-FT 22490

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UNITED STATES DEPARTMENT OF THE INTERIOR - GEOLOGICAL SURVEY - OREGON OFFICE 12/04/89

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

DISCHARGE, CUBIC FEET PER SECOND, WATER YEAR OCTOBER 1977 TO SEPTEMBER 1978

| DAY<br>1<br>2<br>3                 | OCT<br>.18<br>.18<br>.18<br>.18<br>.18<br>.20 | NOV<br>• 57<br>• 63<br>• 63        | DEC<br>36<br>29                   | JAN<br>15                        | FEB                              | MAR                              | APR                               | MAY                              | JUN                               | JUL                                       | AUG                                    | SEP                               |
|------------------------------------|---|------------------------------------|-----------------------------------|----------------------------------|----------------------------------|----------------------------------|-----------------------------------|----------------------------------|-----------------------------------|---|--|-----------------------------------|
| 1 2 3                              | .18<br>.18<br>.18<br>.18<br>.18<br>.20        | .57<br>.63<br>.63                  | 36<br>29                          | 15                               | 10                               |                                  |                                   |                                  |                                   |   |  |                                   |
| 45                                 |   | .63<br>.63                         | 41<br>34<br>27                    | 17<br>29<br>86<br>171            | 69<br>69<br>70<br>78<br>93       | 128<br>109<br>93<br>93<br>90     | 81<br>88<br>72<br>65<br>63        | 61<br>53<br>46<br>42<br>42       | 12<br>9.8<br>8.6<br>7.6<br>6.9    | 3.6<br>5.5<br>9.8<br>15<br>12             | .71<br>.71<br>.63<br>.57<br>.45        | 1.5<br>1.4<br>1.3<br>1.3<br>1.3   |
| 6<br>7<br>8<br>9<br>10             | .20<br>.21<br>.21<br>.21<br>.21               | .71<br>.71<br>.63<br>.63<br>.71    | 23<br>19<br>18<br>15<br>14        | 86<br>69<br>70<br>126<br>185     | 161<br>268<br>370<br>251<br>188  | 103<br>109<br>154<br>295<br>230  | 62<br>70<br>63<br>54<br>48        | 39<br>34<br>28<br>26<br>28       | 6.0<br>5.3<br>4.6<br>4.1<br>4.3   | 8.6<br>6.9<br>15<br>17<br>12              | .45<br>.40<br>.36<br>.36<br>.33        | 1.5<br>1.5<br>1.8<br>1.8<br>1.7   |
| 11<br>12<br>13<br>14<br>15         | .27<br>.33<br>.36<br>.36<br>.40               | .71<br>.71<br>.89<br>.89<br>.89    | 14<br>13<br>34<br>166<br>310      | 149<br>147<br>149<br>179<br>349  | 144<br>111<br>107<br>93<br>92    | 188<br>166<br>149<br>128<br>113  | 43<br>39<br>37<br>35<br>33        | 28<br>26<br>24<br>24<br>40       | 4.8<br>5.0<br>5.5<br>6.6<br>6.0   | 9.0<br>7.6<br>6.3<br>5.0<br>4.1           | .33<br>.40<br>.71<br>.79<br>.99        | 1.8<br>1.8<br>1.8<br>2.1<br>2.3   |
| 16<br>17<br>18<br>19<br>20         | • 4 C<br>• 4 C<br>• 4 5<br>• 5 1<br>• 4 5     | .99<br>.99<br>.80<br>.72<br>.66    | 164<br>99<br>75<br>57<br>42       | 362<br>310<br>230<br>205<br>191  | 73<br>77<br>72<br>92<br>128      | 107<br>101<br>101<br>95<br>92    | 36<br>41<br>38<br>33<br>30        | 42<br>32<br>27<br>22<br>19       | 5.5<br>5.0<br>4.1<br>3.8<br>3.3   | 3 • 8<br>3 • 8<br>3 • 5<br>3 • 2<br>2 • 8 | 1.3<br>.99<br>.79<br>.71<br>.99        | 2.3<br>2.4<br>2.5<br>2.7<br>2.7   |
| 21<br>22<br>23<br>24<br>25         | .51<br>.51<br>.57<br>.51<br>.51               | .80<br>1.2<br>2.9<br>3.3<br>19     | 35<br>37<br>36<br>35<br>34        | 164<br>142<br>115<br>92<br>97    | 126<br>119<br>126<br>126<br>151  | 85<br>81<br>81<br>99<br>83       | 28<br>28<br>31<br>30<br>27        | 17<br>18<br>19<br>18<br>19       | 3.0<br>2.8<br>2.9<br>3.8<br>4.1   | 2.5<br>2.1<br>1.8<br>1.7<br>1.4           | 1.2<br>1.4<br>1.5<br>1.3<br>1.4        | 2.7<br>2.8<br>2.8<br>2.8<br>2.8   |
| 26<br>27<br>28<br>29<br>30<br>31   | •57<br>•57<br>•57<br>•57<br>•57<br>•57        | 73<br>54<br>45<br>39<br>41         | 32<br>29<br>29<br>30<br>31<br>32  | 90<br>77<br>83<br>83<br>80<br>72 | 164<br>179<br>147<br>            | 73<br>66<br>61<br>55<br>53<br>53 | 95<br>171<br>115<br>83<br>67      | 18<br>18<br>17<br>15<br>14<br>13 | 4.1<br>3.6<br>3.2<br>13<br>4.8    | 1.3<br>1.4<br>1.2<br>1.1<br>.99<br>.79    | 1.3<br>1.2<br>1.1<br>1.1<br>1.3<br>1.5 | 2.7<br>2.5<br>2.4<br>2.4<br>2.4   |
| TOTA<br>MEAN<br>MAX<br>MIN<br>AC-F | L 11.92<br>.38<br>.57<br>.18<br>T 24          | 293.93<br>9.80<br>73<br>.57<br>583 | 1590<br>51.3<br>310<br>13<br>3150 | 4220<br>136<br>362<br>15<br>8370 | 3744<br>134<br>370<br>69<br>7430 | 3434<br>111<br>295<br>53<br>6810 | 1706<br>56.9<br>171<br>27<br>3380 | 869<br>28.0<br>61<br>13<br>1720  | 164.1<br>5.47<br>13<br>2.8<br>325 | 170.78 14<br>5.51 17<br>.79<br>339        | 27.27<br>.88<br>1.5<br>.33<br>54       | 63.8<br>2.13<br>2.8<br>1.3<br>127 |

CAL YR 1977 TOTAL 3784.23 MEAN 10.4 MAX 310 MIN .10 AC-FT 7510 WTR YR 1978 TOTAL 16294.80 MEAN 44.6 MAX 370 MIN .18 AC-FT 32320
STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS LATITUCE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

|       |      | DISCHA | DCE, CURT | C EEET OF | D SECOND  | WATED YE   | AR OCTOBE | R 1978 TO | SEPTEMBE   | P 1070 | 200     |        |            |
|-------|------|--------|-----------|-----------|-----------|------------|-----------|-----------|------------|--------|---------|--------|------------|
|       |      | DISCHA | COST COBT | C FEET PE | K SECOND, | IEAN VALUE | S         |           | OCT I CHOE | 117    | Sitt    | 2.47   |            |
| DAY   | OCT  | NOV    | DEC       | JAN       | FEB       | MAR        | APR       | MAY       | JUN        | JUL    | AUG     | SEP    |            |
| 1     | 2.4  | 2.7    | 27        | 7.6       | 7.1       | 107        | 175       | 192       | 18         | 3.94   | .94     | 1.7    |            |
| 2     | 2.3  | 2.8    | 25        | 9.0       | 6.8       | 83         | 202       | 159       | 16         | 3.9    | .94     | 1.7    |            |
| 5     | 2.4  | 2.8    | 21        | 10        | 9.0       | 82         | 202       | 137       | 14         | 3.9    | .94     | 1.7    |            |
| 5     | 2.3  | 2.8    | 75        | 8.6       | 494       | 346        | 208       | 182       | 12         | 3.5    | .94     | 1.4    | huld       |
| 6     | 2.3  | 2.8    | 5.8       | 8.6       | 573       | 556        | 224       | 247       | 11         | 3.5    | .94     | 1.4    | A obre and |
| 7     | 2.3  | 3.0    | 37        | 8.6       | 716       | 539        | 244       | 208       | 10         | 3.5    | .94     | 1.1    | 1 2 2 2 1  |
| 8     | 2.3  | 3.0    | 35        | 7.8       | 264       | 401        | 218       | 187       | 9.6        | 3.9    | .94     | 1.1    | proposed   |
| 9     | 2.1  | 3.0    | 33        | 7.0       | 394       | 306        | 218       | 173       | 9.0        | 3.9    | .94     | 1.1    | > We ka    |
| 10    | 2.1  | 3.0    | 32        | 9.0       | 284       | 295        | 200       | 150       | 9.0        | 3.9    | .94     | 1.4    | wowwww. Th |
| 11    | 2.0  | 2.8    | 53        | 11        | 303       | 282        | 190       | 126       | 9.0        | 4.4    | .94     | 1.4    | 1 1000 10  |
| 12    | 2.0  | 2.7    | 83        | 13        | 367       | 300        | 187       | 113       | 8.4        | 4.4    | .80     | 1.1    | 22         |
| 13    | 2.0  | 2.7    | 63        | 15        | 522       | 282        | 185       | 107       | 7.4        | 4.4    | .80     | 1.1    | 10.        |
| 14    | 2.1  | 2.7    | 42        | 14        | 300       | 274        | 166       | 97        | 7.4        | 3.9    | .94     | 1.1    |            |
| 15    | 2.1  | 2.5    | 37        | 12        | 197       | 282        | 159       | 90        | 6.9        | 3.9    | 121     | 1.1    |            |
| 16    | 2.1  | 2.8    | 33        | 11        | 155       | 311        | 159       | 85        | 6.9        | 3.5    | 6.0     | 1.1    |            |
| 17    | 2.3  | 2.7    | 29        | 9.5       | 115       | 282        | 166       | 77        | 8.4        | 3.5    | 2.87    | .94    |            |
| 18    | 2.3  | 2.4    | 26        | 8.6       | 96        | 259        | 142       | 69        | 9.6        | 2.8    | 1.7     | • 94   |            |
| 19    | 2.1  | 2.1    | 23        | 8.1       | 81        | 244        | 126       | 64        | 9.0        | 2.2    | 2.2     | .94    |            |
| 20    | 2.1  | 3.2    | 20        | 0.0       | 07        | 224        | 115       | 54        | 0.4        | 1.1    | 2.2     | .74    |            |
| 21    | 2.1  | 3.3    | 19        | 13        | 64        | 205        | 107       | 48        | 7.4        | 1.7    | 36      | .94    |            |
| 22    | 2.1  | 3.0    | 19        | 12        | 52        | 182        | 133       | 45        | 6.9        | 1.4    | 4.4     | .94    |            |
| 23    | 2.1  | 3.0    | 21        | 11        | 54        | 166        | 195       | 39        | 6.0        | 1.4    | 2.2     | .80    |            |
| 24    | 2.1  | 3.0    | 25        | 11        | 50        | 108        | 401       | 48        | 0.0        | 1.4    | 1 7     | - 80   |            |
| 20    | 2.1  | 5.0    | 54        | 10        | 10        | 110        | 390       | 48        | 7.4        | 1.4    | 1.1     | .00    |            |
| 26    | 2.3  | 3.0    | 43        | 10        | 171       | 162        | 274       | 37        | 4.8        | 1.4    | 1.7     | .80    |            |
| 27    | 2.4  | 2.8    | 35        | 9.2       | 162       | 185        | 256       | 34        | 4.8        | 1.4    | 1.(     | .80    |            |
| 28    | 2.4  | 3.0    | 30        | 0.0       | 150       | 210        | 256       | 30        | 4.0        | 1 1    | 1 7     | • 0 0  |            |
| 29    | 2.4  | 0.0    | 20        | 0.0       |           | 227        | 241       | 21        | 3.9        | 1.1    | 1.7     | .68    |            |
| 31    | 2.5  | 19     | 10        | 7.2       |           | 195        | 216       | 22        |            | 1.1    | 1.7     |        |            |
|       |      |        |           |           |           |            |           |           | 257 (      | 07 0   | 201 103 | 77 700 |            |
| TOTAL | 69.0 | 108.2  | 1072      | 305.8     | 5/45.9    | 7702       | 6128      | 3094      | 251.4      | 2 81   | 204.08  | 1 11   |            |
| MEAN  | 2.23 | 3.61   | 54.6      | 7.80      | 205       | 248        | 204       | 99.8      | 0.00       | 4.4    | 121     | 2.2    |            |
| MAX   | 2.5  | 21     | 00        | 7 0       | 6.8       | 22         | 401       | 24/       | 3.9        | 1.1    | .80     | .68    |            |
| AC-FT | 137  | 215    | 2130      | 607       | 11400     | 15280      | 12150     | 6140      | 511        | 173    | 406     | 66     |            |
|       |      |        |           |           |           |            |           |           |            |        |         |        |            |

 CAL YR 1978
 TOTAL 15648.15
 MEAN 42.9
 MAX 370
 MIN .33
 AC-FT 31040

 .WTR YR 1979
 TOTAL 24807.36
 MEAN 68.0
 MAX 716
 MIN .68
 AC-FT 49210

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS LATITUCE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

| •                                      |  | DISCHAR                             | RGE, CUBIC                        | FEET PER                          | SECOND,                          | WATER YEAR<br>EAN VALUES               | OCTOBE                           | R 1979 TO                        | SEPTEMBE                          | R 1980                                  | 25.9                                   | - 42  |
|--|--|-------------------------------------|-----------------------------------|-----------------------------------|----------------------------------|--|----------------------------------|----------------------------------|-----------------------------------|---|--|---|
| DAY                                    | ОСТ                                    | NOV                                 | DEC                               | JAN                               | FEB                              | MAR                                    | APR                              | MAY                              | JUN                               | JUL                                     | AUG                                    | SEP   |
| 1<br>2<br>3<br>4<br>5                  | .68<br>.68<br>.58<br>.58               | 6.0<br>6.4<br>6.4<br>4.4            | 31<br>47<br>92<br>135<br>150      | 14<br>13<br>14<br>16<br>34        | 35<br>52<br>70<br>92<br>74       | 155<br>158<br>178<br>172<br>166        | 88<br>78<br>74<br>69<br>70       | 28<br>26<br>21<br>20<br>30       | 11<br>16<br>15<br>13<br>11        | 10<br>9.4<br>9.9<br>9.4<br>9.4          | 1.5<br>1.5<br>1.5<br>1.5<br>1.5<br>1.5 | 2.1<br>2.1<br>2.1<br>2.1<br>2.1<br>2.1        |
| 6<br>7<br>8<br>9<br>10                 | .58<br>.58<br>.48<br>.48<br>.58        | 2.2<br>2.2<br>2.2<br>4.4<br>9.6     | 97<br>80<br>67<br>58<br>54        | 64<br>52<br>43<br>42<br>38        | 76<br>78<br>72<br>62<br>59       | 155<br>175<br>169<br>160<br>149        | 80<br>70<br>62<br>67<br>72       | 34<br>30<br>27<br>24<br>29       | 9.9<br>7.6<br>11<br>14<br>14      | 8.2<br>6.5<br>5.9<br>6.5<br>5.5         | 1.5<br>1.5<br>1.5<br>1.3<br>1.3        | 1.8<br>1.5<br>1.5<br>1.5<br>1.5               |
| 11<br>12<br>13<br>14<br>15             | .68<br>.68<br>.58<br>.68<br>.80        | 10<br>9.6<br>10<br>9.0<br>9.0       | 37<br>39<br>36<br>31<br>27        | 48<br>175<br>422<br>410<br>283    | 56<br>53<br>47<br>40<br>42       | 172<br>149<br>138<br>146<br>146        | 64<br>59<br>56<br>53<br>51       | 35<br>29<br>22<br>25<br>30       | 14<br>14<br>14<br>14<br>14        | 5.0<br>4.6<br>4.2<br>3.4<br>3.4         | 1.3<br>1.3<br>1.3<br>1.1<br>1.1        | 1.5<br>2.1<br>2.4<br>2.4<br>2.4<br>2.1        |
| 16<br>17<br>18<br>19<br>20             | .8C<br>.68<br>.68<br>2.8<br>7.9        | 9.6<br>12<br>22<br>42<br>43         | 26<br>24<br>24<br>26<br>24        | 225<br>207<br>149<br>117<br>105   | 43<br>48<br>240<br>201<br>188    | 119<br>119<br>117<br>117<br>117<br>110 | 48<br>46<br>41<br>39<br>41       | 33<br>31<br>26<br>23<br>19       | 281<br>29<br>17<br>13<br>11       | 3.0<br>2.7<br>2.4<br>2.4<br>2.4<br>2.4  | 1.1<br>1.1<br>1.1<br>1.3<br>1.3        | 1.8<br>1.8<br>1.8<br>1.8<br>1.8<br>1.8        |
| 21<br>22<br>23<br>24<br>25             | 13<br>9.0<br>7.4<br>7.4<br>9.0         | 37<br>36<br>39<br>43<br>56          | 23<br>21<br>15<br>15<br>21        | 107<br>88<br>78<br>76<br>72       | 175<br>160<br>155<br>158<br>163  | 122<br>143<br>181<br>152<br>132        | 44<br>44<br>43<br>39<br>35       | 17<br>14<br>20<br>18<br>14       | 10<br>10<br>13<br>13<br>12        | 2.4<br>2.4<br>2.1<br>2.1<br>2.1<br>2.1  | 1.1<br>1.1<br>1.1<br>1.1<br>1.1        | 1.8<br>2.1<br>2.1<br>2.1<br>2.1               |
| 26<br>27<br>28<br>29<br>30<br>31       | 9.6<br>7.4<br>6.4<br>6.2<br>0.2<br>6.2 | 109<br>60<br>30<br>28<br>29         | 15<br>11<br>12<br>13<br>13<br>13  | 56<br>27<br>28<br>28<br>28<br>32  | 236<br>279<br>221<br>178         | 124<br>119<br>100<br>96<br>90<br>92    | 33<br>31<br>29<br>31<br>31       | 15<br>33<br>44<br>33<br>17<br>17 | 15<br>20<br>17<br>13<br>11        | 2.1<br>1.8<br>1.8<br>1.5<br>1.5         | 1.1<br>1.1<br>1.1<br>1.3<br>1.5<br>2.1 | 1.8<br>1.8<br>1.8<br>1.8<br>1.8<br>1.8<br>1.8 |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>* AC-FT | 109.98<br>3.55<br>13<br>.48<br>218     | 693.0<br>23.1<br>109<br>2.2<br>1370 | 1277<br>41.2<br>150<br>11<br>2530 | 3091<br>99.7<br>422<br>13<br>6130 | 3353<br>116<br>279<br>35<br>6650 | 4321<br>139<br>181<br>90<br>8570       | 1588<br>52.9<br>88<br>29<br>3150 | 784<br>25.3<br>44<br>14<br>1560  | 424.5<br>14.1<br>29<br>7.6<br>842 | 135.8 11<br>4.38 11<br>10<br>1.5<br>269 | 40.3<br>1.30<br>2.1<br>1.1<br>80       | 57.0<br>1.90<br>2.4<br>1.5<br>113             |

 CAL YR
 1979
 TOTAL
 25638.14
 MEAN
 70.2
 MAX
 716
 MIN
 .48
 AC-FT
 50850

 WTR
 YR
 1980
 TOTAL
 15874.58
 MEAN
 43.4
 MAX
 422
 MIN
 .48
 AC-FT
 31490

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STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

DISCHARGE, CUBIC FEET PER SECOND, WATER YEAR OCTOBER 1980 TO SEPTEMBER 1981

|                                      |  |  |  |                                  | M                                 | EAN VALUE                              | S                                 |                                    |                                  | 47                                     | 3.09                             | 2.47   |
|--------------------------------------|--|--|--|----------------------------------|-----------------------------------|--|-----------------------------------|------------------------------------|----------------------------------|--|----------------------------------|--|
| DAY                                  | OCT                                    | NOV                                    | DEC                                    | JAN                              | FEB                               | MAR                                    | APR                               | МАҮ                                | JUN                              | JUL                                    | AUG                              | SEP  |
| 1<br>2<br>3<br>4<br>5                | 1.5<br>1.8<br>2.1<br>2.1<br>2.1<br>2.1 | 6.5<br>7.0<br>7.0<br>6.5<br>0.5        | 8.2<br>8.2<br>9.4<br>13<br>14          | 22<br>21<br>20<br>19<br>18       | 17<br>15<br>21<br>20<br>19        | 54<br>48<br>46<br>44<br>46             | 143<br>119<br>105<br>96<br>85     | 30<br>27<br>25<br>25<br>24         | 56<br>47<br>41<br>35<br>34       | 9.4<br>8.2<br>7.6<br>6.5<br>5.5        | 1.1<br>.93<br>.93<br>.93<br>.93  | .69<br>.69<br>.69<br>.59<br>.59              |
| 6<br>7<br>8<br>9<br>10               | 2.1<br>2.1<br>2.1<br>1.8<br>2.1        | 6.5<br>11<br>9.4<br>8.9<br>3.9         | 13<br>11<br>8.2<br>8.6<br>8.9          | 17<br>17<br>15<br>15<br>15       | 17<br>13<br>16<br>16<br>12        | 40<br>43<br>40<br>39<br>36             | 76<br>69<br>65<br>64<br>64        | 23<br>23<br>24<br>23<br>20         | 44<br>46<br>69<br>92<br>82       | 5.9<br>7.6<br>7.0<br>6.5<br>5.9        | .93<br>.69<br>.69<br>.69<br>.69  | .59<br>.51<br>.51<br>.43<br>.37              |
| 11<br>12<br>13<br>14<br>15           | 2.1<br>2.1<br>2.4<br>2.4<br>3.C        | 8.2<br>8.2<br>7.0<br>7.0<br>7.0        | 9.4<br>9.4<br>9.4<br>8.9<br>8.9        | 14<br>13<br>12<br>11<br>11       | 16<br>22<br>28<br>169<br>204      | 34<br>32<br>30<br>29<br>28             | 56<br>62<br>69<br>57<br>51        | 19<br>17<br>16<br>16<br>17         | 78<br>64<br>64<br>54<br>47       | 5.5<br>5.0<br>4.6<br>4.2<br>3.8        | .59<br>.59<br>.69<br>.59<br>.51  | • 37<br>• 37<br>• 37<br>• 37<br>• 37<br>• 37 |
| 16<br>17<br>18<br>19<br>20           | 3.8<br>3.8<br>3.8<br>3.8<br>3.8<br>3.8 | 7.0<br>7.0<br>7.0<br>7.0<br>7.0<br>7.0 | 8.9<br>9.4<br>9.9<br>10<br>9.9         | 11<br>11<br>11<br>11<br>11       | 243<br>263<br>225<br>279<br>211   | 35<br>46<br>39<br>35<br>34             | 46<br>40<br>38<br>36<br>56        | 23<br>24<br>25<br>65<br>82         | 40<br>38<br>34<br>32<br>30       | 3.4<br>3.4<br>3.0<br>2.7<br>2.4        | .51<br>.43<br>.43<br>.43<br>.59  | . 37<br>. 37<br>. 37<br>. 37<br>. 37<br>. 43 |
| 21<br>22<br>23<br>24<br>25           | 3.8<br>3.8<br>3.8<br>3.8<br>5.0        | 7.0<br>7.0<br>7.0<br>7.0<br>7.0        | 9.9<br>36<br>30<br>24<br>41            | 11<br>11<br>13<br>14<br>15       | 155<br>127<br>112<br>98<br>84     | 40<br>94<br>119<br>92<br>94            | 51<br>44<br>39<br>39<br>40        | 64<br>51<br>41<br>38<br>214        | 27<br>23<br>21<br>19<br>17       | 2.1<br>1.8<br>1.8<br>1.8<br>1.8        | .59<br>.59<br>.59<br>.59<br>.59  | • 43<br>• 51<br>• 59<br>• 59<br>• 69         |
| 26<br>27<br>28<br>29<br>30<br>31     | 5.0<br>5.C<br>5.C<br>5.C<br>5.5<br>5.5 | 8.2<br>8.2<br>8.2<br>8.2<br>8.2<br>8.2 | 5 0<br>4 6<br>3 5<br>3 0<br>2 6<br>2 4 | 15<br>14<br>14<br>18<br>23<br>22 | 72<br>64<br>59<br>                | 204<br>243<br>197<br>152<br>140<br>122 | 38<br>46<br>46<br>38<br>33        | 211<br>127<br>92<br>74<br>69<br>67 | 15<br>13<br>13<br>12<br>11       | 1.8<br>1.5<br>1.3<br>1.1<br>1.1<br>1.1 | .59<br>.59<br>.59<br>.59<br>.59  | .80<br>2.1<br>2.1<br>1.8<br>1.5<br>0         |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>AC-FT | 102.4<br>3.30<br>5.9<br>1.5<br>203     | 227.2<br>7.57<br>11<br>6.5<br>451      | 557.5<br>18.0<br>59<br>8.2<br>1110     | 465<br>15.0<br>23<br>11<br>922   | 2597<br>92.7<br>279<br>12<br>5150 | 2275<br>73.4<br>243<br>28<br>4510      | 1811<br>60.4<br>143<br>33<br>3590 | 1596<br>51.5<br>214<br>16<br>3170  | 1198<br>39.9<br>92<br>11<br>2380 | 125.3 1<br>4.04<br>9.4<br>1.1<br>249   | 20.46<br>.66<br>1.1<br>.43<br>41 | 20.53<br>.68<br>2.1<br>.37<br>41             |

 CAL YR 1980
 TOTAL 14681.7
 MEAN 40.1
 MAX 422
 MIN 1.1
 AC-FT 29120

 WTR YR 1981
 TOTAL 10995.39
 MEAN 30.1
 MAX 279
 MIN .37
 AC-FT 21810

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021 

|                                      |   | DISCHA                                 | RGE, CUBIC                          | FEET PE                                | R SECOND,                          | WATER YE<br>IEAN VALUE                 | AR OCTOBER                       | 1901 10                          | SEPTEMBE                          | R 1982                                       | 3.09                                   | 2.47                               | 1 |
|--------------------------------------|---|--|-------------------------------------|--|------------------------------------|--|----------------------------------|----------------------------------|-----------------------------------|--|--|------------------------------------|---|
| DAY                                  | ОСТ                                       | NOV                                    | DEC                                 | JAN                                    | FEB                                | MAR                                    | APR                              | MAY                              | JUN                               | JUL  | AUG                                    | SEP                                |   |
| 1<br>2                               | 1.1                                       | 6.5                                    | 25<br>44                            | 55<br>60                               | 155<br>149                         | 388<br>420                             | 133<br>124                       | 70<br>65                         | 16<br>16                          | 9.3  | .86                                    | .69                                |   |
| 3<br>4<br>5                          | •93<br>•93<br>•93                         | 6.5<br>7.0<br>7.0                      | 88<br>69<br>67                      | 64<br>65<br>51                         | 158<br>85<br>70                    | 340<br>312<br>302                      | 124<br>121<br>115                | 61<br>64<br>56                   | 16<br>18<br>26                    | 9.7<br>10<br>8.6                             | 1.1<br>1.1<br>.95                      | • 5 5<br>• 5 5                     |   |
| 6<br>7<br>8<br>9<br>10               | .93<br>1.1<br>1.3<br>1.3<br>1.5           | 7.0<br>7.0<br>7.0<br>7.0<br>7.0        | 468<br>300<br>175<br>132<br>122     | 28<br>31<br>34<br>36<br>36             | 75<br>75<br>70<br>73<br>80         | 284<br>263<br>253<br>249<br>239        | 110<br>110<br>100<br>98<br>98    | 50<br>48<br>47<br>47<br>58       | 25<br>21<br>18<br>15<br>14        | 7.6<br>7.2<br>7.6<br>7.9<br>6.9              | - 86<br>- 86<br>- 78<br>- 69<br>- 69   | .60<br>.60<br>.55<br>.55<br>.78    |   |
| 11<br>12<br>13<br>14<br>15           | 2 • 1<br>2 • 4<br>2 • 4<br>2 • 7<br>2 • 7 | 7.0<br>7.0<br>7.0<br>7.0<br>7.0<br>7.6 | 98<br>82<br>74<br>88<br>279         | 36<br>39<br>43<br>45<br>50             | 80<br>82<br>88<br>225<br>540       | 242<br>223<br>214<br>211<br>226        | 223<br>263<br>232<br>246<br>223  | 61<br>52<br>44<br>39<br>36       | 12<br>13<br>26<br>24<br>19        | 6.0<br>5.0<br>4.3<br>4.3<br>4.0              | .78<br>.86<br>.78<br>.78<br>.86        | .95<br>1.1<br>1.2<br>1.1<br>1.1    |   |
| 16<br>17<br>18<br>19<br>20           | 2.7<br>3.0<br>3.0<br>3.4<br>3.8           | 8.9<br>15<br>20<br>16<br>14            | 263<br>207<br>204<br>809<br>525     | 140<br>130<br>117<br>98                | 1280<br>982<br>690<br>720<br>822   | 205<br>187<br>178<br>151<br>151        | 199<br>184<br>166<br>148<br>139  | 31<br>33<br>49<br>40<br>35       | 16<br>14<br>13<br>11<br>9.7       | 4.0<br>3.6<br>3.5<br>2.9<br>2.4              | .86<br>.69<br>.60<br>.55<br>.55        | .95<br>1.1<br>1.1<br>1.4<br>2.2    |   |
| 21<br>22<br>23<br>24<br>25           | 4 • 2<br>4 • 6<br>4 • 6<br>5 • 0<br>5 • 0 | 13<br>16<br>21<br>33<br>33             | 344<br>243<br>188<br>163<br>149     | 100<br>82<br>130<br>344<br>316         | 786<br>456<br>396<br>319<br>288    | 139<br>145<br>142<br>142<br>142        | 130<br>124<br>124<br>121<br>108  | 30<br>27<br>23<br>21<br>19       | 9.3<br>10<br>9.0<br>8.3<br>7.9    | 2.2<br>2.1<br>1.9<br>1.8<br>1.5              | • 50<br>• 50<br>• 50<br>• 45<br>• 45   | 2.7<br>2.9<br>2.6<br>2.9<br>3.3    |   |
| 26<br>27<br>28<br>29<br>30<br>31     | 5.0<br>5.0<br>5.5<br>5.9<br>6.5<br>6.5    | 28<br>28<br>26<br>25<br>25             | 135<br>117<br>107<br>74<br>62<br>55 | 352<br>279<br>232<br>194<br>172<br>166 | 277<br>284<br>277<br>              | 154<br>157<br>148<br>151<br>145<br>136 | 103<br>93<br>90<br>83<br>77      | 18<br>18<br>20<br>21<br>19<br>18 | 8.3<br>8.3<br>8.6<br>9.0<br>9.3   | 1.4<br>1.3<br>1.2<br>.95<br>.95<br>.86       | .40<br>.40<br>.40<br>.45<br>.60<br>.69 | 5.3<br>5.0<br>4.5<br>4.3<br>4.5    |   |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>AC-FT | 96.95<br>3.13<br>6.5<br>.93<br>192        | 426.0<br>14.2<br>33<br>6.5<br>845      | 5756<br>186<br>809<br>25<br>11420   | 3589<br>116<br>352<br>28<br>7120       | 9582<br>342<br>1280<br>70<br>19010 | 6639<br>214<br>420<br>136<br>13170     | 4209<br>140<br>263<br>77<br>8350 | 1220<br>39.4<br>70<br>18<br>2420 | 430.7<br>14.4<br>26<br>7.9<br>854 | 139.56 <b>12</b><br>4.50<br>10<br>.86<br>277 | 21.40<br>.69<br>1.1<br>.40<br>42       | 56.17<br>1.87<br>5.3<br>.55<br>111 |   |

CAL YR 1981 TOTAL 16387.24 MEAN 44.9 MAX 809 MIN .37 AC-FT 32500 WTR YR 1982 TOTAL 32165.78 MEAN 88.1 MAX 1280 MIN .40 AC-FT 63800

|                                      |  | UNITE                           | D STATES D                        | EPARTMEN                               | IT OF THE                                 | INTERIOR -                             | GEOLOGI                          | CAL SURVE                          | Y - OREGO                       | N OFFICE                                   | 1 2                                    | 2/04/89  |                        |
|--------------------------------------|--|---------------------------------|-----------------------------------|--|---|--|----------------------------------|------------------------------------|---------------------------------|--|--|--|------------------------|
|                                      | STATION<br>LATITUDE                    | NUMBER 14<br>451553 1           | 4047390<br>LONGITUDE              | ROCK CRE<br>1200115                    | EK AB WHY<br>DRAINAG                      | TE PARK NR<br>E AREA                   | CONDON.<br>297.                  | OREG. ST<br>ATUM 171               | REAM SOU<br>4.50 STA            | RCE AGENCI<br>TE 41 COU                    | Y USGS<br>JNTY 021                     |  |                        |
| •                                    |  | DISCHAR                         | RGE, CUBIC                        | FEET PE                                | R SECOND,                                 | WATER YEA<br>EAN VALUES                | R OCTOBE                         | R 1982 TO                          | SEPTEMBE                        | R 1983                                     | 3.09                                   | 2.47   |                        |
| DAY                                  | OCT                                    | NOV                             | DEC                               | JAN                                    | FEB                                       | MAR                                    | APR                              | ΜΑΥ                                | JUN                             | JUL  | AUG                                    | SEP  |                        |
| 1<br>2<br>3<br>4<br>5                | 4.0<br>4.0<br>4.3<br>4.3               | 25<br>22<br>20<br>19<br>18      | 37<br>33<br>32<br>52<br>77        | 43<br>47<br>47<br>50<br>59             | 110<br>105<br>83<br>67<br>62              | 376<br>404<br>352<br>816<br>816        | 270<br>444<br>348<br>288<br>256  | 157<br>166<br>130<br>124<br>1860   | 39<br>38<br>35<br>32<br>30      | 18<br>21<br>21<br>18<br>16                 | 4.9<br>6.0<br>7.1<br>6.0<br>4.9        | 5 • 2<br>4 • 6<br>4 • 3<br>4 • 3<br>4 • 0          |                        |
| 6<br>7<br>8<br>9<br>10               | 4.5<br>4.3<br>4.3<br>4.8<br>5.0        | 18<br>18<br>17<br>17<br>16      | 103<br>105<br>61<br>61<br>52      | 260<br>372<br>340<br>256<br>199        | 62<br>65<br>65<br>81<br>95                | 786<br>738<br>625<br>655<br>585        | 226<br>205<br>184<br>169<br>154  | 1320<br>834<br>708<br>635<br>495   | 29<br>27<br>26<br>32<br>31      | 13<br>12<br>12<br>12<br>12<br>12           | 4.0<br>3.8<br>3.5<br>3.5<br>3.5<br>3.3 | 4 • 0<br>3 • 8<br>3 • 5<br>3 • 5<br>3 • 5<br>3 • 5 |                        |
| 11<br>12<br>13<br>14<br>15           | 5.3<br>5.3<br>5.3<br>5.3<br>5.3<br>5.3 | 15<br>15<br>15<br>14<br>13      | 44<br>44<br>48<br>45<br>43        | 166<br>145<br>127<br>105<br>88         | 130<br>260<br>298<br>239<br>235           | 495<br>515<br>1070<br>858<br>666       | 145<br>130<br>118<br>108<br>90   | 348<br>309<br>267<br>211<br>184    | 38<br>35<br>30<br>26<br>26      | 11<br>10<br>9.1<br>8.7<br>8.3              | 3.0<br>4.0<br>4.0<br>3.8<br>3.0        | 3.8<br>3.8<br>3.8<br>3.5<br>3.5<br>3.5             | Witest yours on Record |
| 16<br>17<br>18<br>19<br>20           | 5.5<br>5.3<br>5.5<br>5.8<br>6.3        | 15<br>15<br>16<br>18<br>19      | 139<br>281<br>196<br>151<br>121   | 93<br>93<br>93<br>105<br>118           | 356<br>372<br>684<br>625<br>505           | 530<br>444<br>380<br>323<br>281        | 81<br>77<br>72<br>68<br>72       | 199<br>164<br>140<br>128<br>117    | 24<br>23<br>20<br>19<br>20      | 7.9<br>8.7<br>9.1<br>7.1<br>6.7            | 2.6<br>2.6<br>2.1<br>1.9<br>2.1        | 3.5<br>3.3<br>3.5<br>6.0<br>6.0                    |                        |
| 21<br>22<br>23<br>24<br>25           | 6.5<br>6.9<br>8.3<br>8.3<br>9.0        | 18<br>16<br>15<br>15<br>14      | 115<br>173<br>148<br>103<br>81    | 103<br>93<br>90<br>90<br>100           | 4 6 5<br>5 2 5<br>5 2 5<br>4 8 5<br>4 4 4 | 260<br>246<br>226<br>208<br>193        | 166<br>142<br>110<br>115<br>98   | 104<br>95<br>85<br>78<br>69        | 18<br>18<br>17<br>17<br>15      | 6.0<br>5.6<br>5.2<br>6.0<br>6.3            | 2.1<br>2.1<br>3.0<br>4.0,<br>4.6       | 6.3<br>6.0<br>6.0<br>6.0<br>5.6                    | cloud bust 4.30        |
| 26<br>27<br>28<br>29<br>30<br>31     | 9.0<br>9.7<br>10<br>35<br>62<br>33     | 15<br>15<br>16<br>23<br>41      | 83<br>65<br>55<br>45<br>43<br>43  | 118<br>175<br>169<br>151<br>130<br>118 | 424<br>352<br>356<br>                     | 184<br>196<br>205<br>193<br>515<br>348 | 81<br>75<br>68<br>199<br>172     | 63<br>59<br>51<br>47<br>43<br>38   | 12<br>11<br>13<br>14<br>15      | 7.1<br>6.7<br>6.3<br>5.6<br>5.2<br>4.9     | 4.6<br>4.3<br>4.0<br>4.3<br>4.6<br>4.3 | 5.6<br>5.2<br>5.2<br>5.2<br>6.0 30                 |                        |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>AC-FT | 296.1<br>9.55<br>62<br>4.C<br>587      | 533<br>17.8<br>41<br>13<br>1060 | 2689<br>86.7<br>281<br>32<br>5330 | 4143<br>134<br>372<br>43<br>8220       | 8075<br>288<br>684<br>62<br>16020         | 14489<br>467<br>1070<br>184<br>28740   | 4731<br>158<br>444<br>68<br>9380 | 9228<br>298<br>1860<br>38<br>18300 | 730<br>24.3<br>39<br>11<br>1450 | 306.5 <b>3</b><br>9.89<br>21<br>4.9<br>608 | 118.0<br>3.81<br>7.1<br>1.9<br>234     | 138.5<br>4.62<br>6.3<br>3.3<br>275                 |                        |
| CAL YR<br>WTR YR                     | R 1982 T<br>R 1983 T                   | OTAL 2940<br>OTAL 454           | 4.93 MEAN<br>77.1 MEAN            | 80.6                                   | MAX 1280<br>MAX 1860                      | MIN .40<br>MIN 1.9                     | AC-FT AC-FT                      | 58320                              |                                 |  |  |  |                        |

|                                      | STATION<br>LATITUDE                   | NUMBER 1<br>451553              | 4047390<br>LONGITUDE               | ROCK CREE<br>1200115                   | K AB WHY                         | TE PARK N                              | 297. DA                             | TUM 171                          | REAM SOUR                         | RCE AGENCY<br>TE 41 COU                    | USGS<br>NTY 021                                    |  |             |         |
|--------------------------------------|---------------------------------------|---------------------------------|------------------------------------|--|----------------------------------|--|-------------------------------------|----------------------------------|-----------------------------------|--|--|--|-------------|---------|
|                                      |                                       | DISCHA                          | RGE, CUBIC                         | FEET PER                               | SECOND,                          | WATER YE<br>EAN VALUE                  | AR OCTOBER<br>S                     | R 1983 TO                        | SEPTEMBER                         | R 1984<br>4-7                              | 309  | 2.47                                   |             |         |
| YAC                                  | ОСТ                                   | NOV                             | DEC                                | JAN                                    | FEB                              | MAR                                    | APR                                 | МАҮ                              | JUN                               | JUL  | AUG  | SEP                                    |             |         |
| 1<br>2<br>3<br>4<br>5                | 6.0<br>6.0<br>6.0<br>6.0<br>6.0       | 13<br>14<br>15<br>15<br>13      | 26<br>25<br>25<br>24<br>22         | 120<br>155<br>450<br>480<br>390        | 95<br>90<br>86<br>77<br>77       | 184<br>344<br>273<br>228<br>207        | 485<br>425<br>375<br>348<br>449     | 221<br>321<br>269<br>249<br>224  | 48<br>46<br>43<br>52<br>79        | 34<br>30<br>29<br>27<br>24                 | 15<br>10<br>7.0<br>5.5<br>5.0                      | 9.7<br>9.7<br>9.3<br>9.0<br>8.6        |             |         |
| 6<br>7<br>8<br>9<br>10               | 6.0<br>5.6<br>6.0<br>8.7<br>11        | 14<br>16<br>16<br>16<br>16      | 24<br>24<br>36<br>91<br>256        | 300<br>240<br>200<br>155<br>130        | 82<br>82<br>82<br>88<br>77       | 194<br>207<br>231<br>294<br>420        | 550<br>437<br>628<br>531<br>511     | 217<br>194<br>171<br>163<br>160  | 130<br>169<br>147<br>116<br>112   | 24<br>21<br>20<br>19<br>17                 | 4 • 7<br>4 • 7<br>4 • 7<br>4 • 7<br>4 • 7<br>4 • 7 | 8.2<br>9.0<br>9.3<br>9.7<br>9.3        |             |         |
| 11<br>12<br>13<br>14<br>15           | 11<br>9.6<br>9.1<br>8.7<br>8.3        | 18<br>20<br>19<br>19<br>19      | 164<br>115<br>102<br>143<br>280    | 120<br>100<br>80<br>65<br>55           | 70<br>74<br>339<br>425<br>273    | 449<br>362<br>357<br>583<br>576        | 518<br>473<br>415<br>380<br>395     | 157<br>147<br>135<br>123<br>121  | 107<br>99<br>101<br>152<br>107    | 17<br>16<br>15<br>14<br>13                 | 4 • 7<br>4 • 7<br>4 • 7<br>4 • 5<br>4 • 2          | 9.0<br>8.6<br>8.2<br>8.2<br>8.2<br>8.2 |             |         |
| 16<br>17<br>18<br>19<br>20           | 8.3<br>7.9<br>8.3<br>8.7<br>8.7       | 21<br>50<br>50<br>32<br>26      | 140<br>106<br>82<br>69<br>50       | 46<br>46<br>47<br>47<br>48             | 242<br>210<br>169<br>163<br>174  | 563<br>622<br>443<br>390<br>420        | 390<br>375<br>362<br>628<br>511     | 114<br>101<br>95<br>88<br>84     | 86<br>72<br>63<br>56<br>54        | 11<br>10<br>9.7<br>8.5<br>7.5              | 3.9<br>3.9<br>3.9<br>3.9<br>3.9<br>3.7             | 8.2<br>8.2<br>8.2<br>8.2<br>7.9        |             | and and |
| 21<br>22<br>23<br>24<br>25           | 8.7<br>8.7<br>9.6<br>9.6<br>10        | 24<br>22<br>20<br>25<br>35      | 32<br>27<br>25<br>25<br>26         | 55<br>60<br>80<br>130<br>155           | 197<br>184<br>169<br>166<br>163  | 654<br>589<br>615<br>524<br>437        | 415<br>362<br>312<br>285<br>273     | 77<br>72<br>92<br>92<br>77       | 88<br>114<br>101<br>79<br>64      | 7.0<br>6.7<br>6.6<br>6.5<br>6.4            | 3.5<br>3.5<br>3.5<br>3.5<br>3.5<br>3.5             | 7.9<br>8.2<br>10<br>12<br>13           | 29 part fre | Sa      |
| 26<br>27<br>28<br>29<br>30<br>31     | 9.6<br>9.1<br>9.1<br>9.6<br>9.6<br>11 | 31<br>28<br>26<br>30<br>29      | 30<br>55<br>60<br>65<br>100<br>120 | 155<br>140<br>130<br>120<br>110<br>100 | 135<br>147<br>147<br>163         | 524<br>615<br>635<br>596<br>550<br>511 | 249<br>224<br>203<br>197<br>184     | 84<br>76<br>63<br>57<br>53<br>53 | 56<br>51<br>45<br>40<br>36        | 5.6<br>5.6<br>5.7<br>5.7<br>8.0 <b>3</b> 1 | 3.5<br>3.8<br>4.5<br>5.3<br>6.2<br>8.6 <u>3</u> ]  | 13<br>12<br>12<br>12<br>12<br>11 30    |             |         |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>AC-FT | 260.5<br>8.40<br>11<br>5.6<br>517     | 692<br>23.1<br>50<br>13<br>1370 | 2369<br>76.4<br>280<br>22<br>4700  | 4509<br>145<br>480<br>46<br>8940       | 4446<br>153<br>425<br>70<br>8820 | 13597<br>439<br>654<br>184<br>26970    | 11890<br>396<br>628<br>184<br>23580 | 4150<br>134<br>321<br>53         | 2513<br>83.8<br>169<br>36<br>4980 | 436.1<br>14.1<br>34<br>5.6<br>865          | 157.5<br>5.08<br>15<br>3.5<br>312                  | 285.8<br>9.53<br>13<br>7.9<br>567      |             |         |

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON.OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

DISCHARGE, CUBIC FEET PER SECOND, WATER YEAR OCTOBER 1984 TO SEPTEMBER 1985

| ,      |      |             |         |         | 1       | MEAN VALL | JES         |      |       |      | 3.07 | 2,41   |
|--------|------|-------------|---------|---------|---------|-----------|-------------|------|-------|------|------|--------|
| DAY    | ОСТ  | NOV         | DEC     | JAN     | FEB     | MAR       | APR         | MAY  | JUN   | JUL  | AUG  | SEP    |
| 1      | 11   | 16          | 55      | 32      | 32      | 177       | 607         | 66   | 23    | 4 0  | 2 3  | 2.2    |
| 2      | 11   | 26          | 42      | 30      | 31      | 165       | 663         | 61   | 23    | 3.8  | 2.3  | 2.6    |
| 3      | 11   | 49          | 40      | 29      | 28      | 134       | 611         | 56   | 21    | 3.1  | 2.2  | 2.9    |
| 4      | 11   | 35          | 38      | 28      | 28      | 139       | 519         | 55   | 20    | 2.9  | 2.2  | 2.8    |
| 5      | 11   | 27          | 35      | 2.7     | 28      | 118       | 489         | 52   | 19    | 2.6  | 2.2  | 2.8    |
| 6      | 11   | 24          | 28      | 27      | 35      | 110       | 493         | 48   | 21    | 2.6  | 2.2  | 2.9    |
| 7      | 11   | 22          | 38      | 26      | 49      | 93        | 463         | 43   | 23    | 2.6  | 2.0  | 3.4    |
| 8      | 11   | 20          | 40      | 27      | 52      | 98        | 411         | 40   | 23    | 2.3  | 2.0  | 3.8    |
| 9      | 11   | 22          | 36      | 27      | 38      | 98        | 3/1         | 38   | 22    | 2.3  | 2.2  | 4.2    |
| 10     | 11   | 24          | 56      | 27      | 34      | 100       | 548         | 37   | 18    | 2.2  | 2.2  | 6.1    |
| 11     | 12   | 30          | 58      | 27      | 77      | 114       | 384         | 37   | 17    | 2.0  | 2.3  | 6.1    |
| 12     | 13   | 122         | (4      | 26      | 168     | 127       | 262         | 22   | 15    | 2.0  | 2.3  | 5.5    |
| 13     | 13   | 130         | 08      | 21      | 107     | 150       | 202         | 71   | 14    | 2.0  | 2.2  | 5.1    |
| 14     | 13   | 67          | 62      | 20      | 107     | 101       | 200         | 20   | 14    | 2.0  | 2.2  | 2.2    |
|        | 14   | 01          | 02      | 29      | 107     | 171       | 207         | 29   | 14    | 1.9  | 2.2  | 0.1    |
| 16     | 15   | 55          | 55      | 29      | 157     | 249       | 195         | 26   | 13    | 1.9  | 2.0  | 8.6    |
| 17     | 15   | 48          | 51      | 29      | 122     | 312       | 171         | 23   | 10    | 1.7  | 2.0  | 7.6    |
| 18     | 14   | 50          | 48      | 32      | 110     | 411       | 156         | 23   | 9.0   | 1.7  | 2.0  | 7.2    |
| 19     | 14   | 55          | 46      | 33      | 106     | 443       | 155         | 23   | 8.2   | 1.6  | 2.3  | 7.1    |
| 20     | 14   | 51          | 44      | 61      | 104     | 440       | 145         | 22   | 6.7   | 1.4  | 2.3  | 6.9    |
| 21     | 15   | 65          | 43      | 67      | 97      | 466       | 134         | 21   | 5.8   | 1.3  | 2.3  | 6.6    |
| 22     | 15   | 61          | 80      | 63      | 151     | 342       | 133         | 19   | 5.8   | 1.3  | 2.5  | 6.5    |
| 23     | 15   | 51          | 62      | 20      | 179     | 212       | 134         | 18   | 5.8   | 1.4  | 2.51 | 6.4    |
| 24     | 15   | 74          | >>      | 22      | 226     | 452       | 129         | 18   | 5.5   | 1.4  | 2.3  | 6.5    |
| 25     | 15   | (1          | 49      | 51      | 223     | 330       | 123         | 18   | 2.2   | 1.4  | 2.2  | 0.8    |
| 26     | 17   | 63          | 48      | 47      | 176     | 255       | 114         | 17   | 5.5   | 1.4  | 2.2  | 7.0    |
| 27     | 19   | 57          | 46      | 42      | 143     | 220       | 104         | 17   | 4.9   | 1.3  | 2.0  | 7.0    |
| 28     | 19   | 58          | 43      | 44      | 142     | 205       | 90          | 18   | 4.7   | 1.3  | 1.9  | 7.1    |
| 29     | 18   | 65          | 44      | 40      |         | 194       | 79          | 23   | 4.5   | 1.3  | 2.0  | 7.3 30 |
| 30     | 18   | 62          | 42      | 35      |         | 191       | 72          | 30   | 4.0   | 1.4  | 2.0  | 7.3 00 |
| 31     | 17   |             | 41      | 53      |         | 327       |             | 26   |       | 2.5  | 2.0  |        |
| TOTAL  | 43C  | 1618        | 1535    | 1135    | 2927    | 7053      | 8320        | 1001 | 385.9 | 62.6 | 67.5 | 168.5  |
| MEAN   | 13.9 | 53.9        | 49.5    | 30.0    | 105     | 228       | 277         | 32.3 | 12.9  | 2.02 | 2.18 | 5.62   |
| MAX    | 19   | 130         | 86      | 67      | 225     | 466       | 663         | 66   | 23    | 4.0  | 2.5  | 8.6    |
| MIN    | 11   | 16          | 28      | 26      | 28      | 93        | 72          | 17   | 4.0   | 1.3  | 1.9  | 2.2    |
| AC-FT  | 853  | 3210        | 3040    | 2250    | 5810    | 13990     | 16500       | 1990 | 765   | 124  | 134  | 334    |
| CAL YR | 1984 | TOTAL 45567 | .4 MEAN | 125 MA  | X 654 M | MIN 3.5   | AC-FT 90700 |      |       |      |      |        |
| WTR YR | 1985 | TOTAL 24703 | .> MEAN | 01.1 MA | × 003 1 | 111 1.3   | AC-FT 49000 |      |       |      |      |        |

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WATEH RESOURCES DEPT SALEM, OREGON

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON.OREG. STREAM SOURCE AGENCY USGS LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA 297. DATUM 1714.50 STATE 41 COUNTY 021

DISCHARGE, CUBIC FEET REP SECOND, WATER YEAR OCTOBER 1985 TO SEPTEMBER 1986

| )                                     |                                   | DISCHAR                           | GET CUBIC                        | FEEL PER                            | ME                                  | AN VALUES                              |                                  |                                  |                                   |   | 200                                    | 2.47                                   |
|---------------------------------------|-----------------------------------|-----------------------------------|----------------------------------|-------------------------------------|-------------------------------------|--|----------------------------------|----------------------------------|-----------------------------------|---|--|--|
| DAY                                   | OCT                               | NCV                               | DEC                              | JAN                                 | FEB                                 | MAR                                    | APR                              | МАҮ                              | JUN                               | JUL   | AUG                                    | SEP                                    |
| 1<br>2<br>3<br>4<br>5                 | 7.3<br>7.3<br>7.3<br>7.5<br>7.5   | 13<br>13<br>13<br>13<br>13<br>13  | 10<br>14<br>21<br>21<br>25       | 19<br>23<br>24<br>22<br>20          | 369<br>339<br>334<br>228<br>185     | 551<br>430<br>338<br>279<br>275        | 95<br>88<br>80<br>74<br>67       | 36<br>35<br>36<br>37<br>37       | 16<br>17<br>18<br>19<br>20        | 5.1<br>4.7<br>4.6<br>6.0<br>6.8               | 2.2<br>2.2<br>2.1<br>2.0<br>2.1        | 2.9<br>2.5<br>2.5<br>2.5<br>2.5<br>2.4 |
| 6<br>7<br>8<br>9<br>10                | 7.7<br>12<br>16<br>13<br>12       | 13<br>13<br>14<br>15<br>14        | 40<br>69<br>56<br>40<br>35       | 38<br>28<br>27<br>73<br>134         | 149<br>124<br>94<br>87<br>91        | 251<br>366<br>410<br>390<br>352        | 63<br>58<br>54<br>52<br>50       | 37<br>37<br>36<br>35<br>35       | 19<br>18<br>17<br>15<br>14        | 6.01<br>5.1<br>4.9<br>4.6<br>4.3              | 2.1<br>2.1<br>2.0<br>2.0<br>1.8        | 2.5<br>2.7<br>2.6<br>3.0<br>3.1        |
| 11<br>12<br>13<br>14<br>15            | 12<br>12<br>12<br>11<br>11        | 12<br>9.0<br>10<br>11<br>11       | 30<br>35<br>30<br>27<br>25       | 105<br>86<br>73<br>69<br>65         | 82<br>70<br>70<br>68<br>70          | 338<br>299<br>290<br>270<br>250        | 52<br>52<br>50<br>47<br>47       | 35<br>34<br>32<br>30<br>28       | 13<br>12<br>10<br>9.4<br>8.5      | 4.7<br>4.6<br>4.4<br>3.9<br>3.8               | 1.7<br>1.8<br>1.9<br>1.8<br>1.7        | 3.3<br>3.3<br>3.3<br>3.4<br>4.0        |
| 16<br>17<br>18<br>19<br>20            | 11<br>11<br>11<br>11<br>11<br>11  | 11<br>13<br>15<br>17<br>13        | 23<br>22<br>19<br>17<br>16       | 79<br>186<br>151<br>244<br>188      | 369<br>673<br>618<br>420<br>295     | 230<br>220<br>210<br>190<br>180        | 49<br>51<br>52<br>45<br>40       | 25<br>22<br>20<br>19<br>25       | 8.7<br>9.0<br>9.4<br>9.7<br>10    | 3.7<br>3.9<br>3.7<br>3.5<br>3.2               | 1.7<br>1.8<br>1.7<br>1.7<br>1.7        | 4.9<br>6.3<br>6.1<br>5.5<br>6.5        |
| 21<br>22<br>23<br>24<br>25            | 11<br>12<br>15<br>18<br>17        | 11<br>10<br>8.5<br>8.0<br>8.0     | 16<br>16<br>16<br>16<br>16       | 134<br>121<br>141<br>123<br>97      | 259<br>785<br>1760<br>1410<br>981   | 160<br>150<br>200<br>210<br>175        | 40<br>40<br>40<br>40<br>40       | 35<br>35<br>29<br>24<br>21       | 8.0<br>6.0<br>5.0<br>4.3<br>3.8   | 3.0<br>2.8<br>2.6<br>2.5<br>2.4               | 1.8<br>1.7<br>1.7<br>1.8<br>2.0        | 7.6<br>6.8<br>7.1<br>8.5<br>8.7        |
| 26<br>27<br>28<br>29<br>30<br>31      | 15<br>14<br>14<br>13<br>13<br>13  | 11<br>13<br>10<br>9.0<br>9.0      | 16<br>15<br>14<br>13<br>14<br>15 | 90<br>85<br>90<br>100<br>437<br>434 | 894<br>644<br>690<br>               | 155<br>145<br>135<br>125<br>115<br>100 | 41<br>43<br>43<br>41<br>38       | 22<br>19<br>17<br>16<br>15<br>15 | 3.9<br>4.8<br>7.4<br>6.3<br>6.0   | 2.4<br>2.4<br>2.5<br>2.3<br>2.3<br>2.3<br>2.3 | 1.9<br>2.0<br>6.0<br>7.2<br>4.1<br>3.4 | 8.5<br>8.5<br>9.2<br>9.7 2             |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>-AC-FT | 365.6<br>11.8<br>18<br>7.3<br>725 | 353.5<br>11.8<br>17<br>8.0<br>701 | 742<br>23.9<br>69<br>10<br>1470  | 3506<br>113<br>437<br>19<br>6950    | 12158<br>434<br>1760<br>68<br>24120 | 7789<br>251<br>551<br>100<br>15450     | 1572<br>52.4<br>95<br>38<br>3120 | 879<br>28.4<br>37<br>15<br>1740  | 328.2<br>10.9<br>20<br>3.8<br>651 | 119.05<br>3.84<br>6.8<br>2.3<br>236           | 71.74<br>2.31<br>7.2<br>1.7<br>142     | 156.5<br>5.22<br>9.7<br>2.4<br>310     |

CAL YR 1985 TOTAL 22581.6 MEAN 61.9 MAX 663 MIN 1.3 AC-FT 44790 WTR YR 1986 TOTAL 28040.5 MEAN 76.8 MAX 1760 MIN 1.7 AC-FT 55620

| <b>D</b> ,                          |   | UNIT                            | ED STATES                        | DEPARTMENT                       | OF THE                           | INTERIOR                               | - GEOLOG                          | ICAL SURVE                         | Y - OREGON                        | OFFICE  | 1   | 2/04/89                                |             |
|-------------------------------------|---|---------------------------------|----------------------------------|----------------------------------|----------------------------------|--|-----------------------------------|------------------------------------|-----------------------------------|---|---|--|-------------|
|                                     | STATION<br>LATITUDE                     | NUMBER 1<br>451553              | 14047390<br>LONGITUDE            | ROCK CREE<br>1200115             | K AB WHY<br>DRAINAG              | TE PARK N<br>E AREA                    | R CONDON.<br>297. I               | OREG. ST<br>DATUM 171              | REAM SOUR                         | CE AGENCY<br>E 41 COUN                        | USGS<br>NTY 021                           |  |             |
| •                                   |   | DISCH                           | ARGE, CUBI                       | C FEET PER                       | SECOND                           | WATER YE<br>EAN VALUE                  | AR OCTOB<br>S                     | ER 1986 TC                         | ) SEPTEMBER                       | 1987  | 2.09                                      |  |             |
| DAY                                 | OCT                                     | NOV                             | DEC                              | JAN                              | FEB                              | MAR                                    | APR                               | ΜΑΥ                                | JUN                               | JUL   | AUG                                       | SEP24                                  | 7           |
| 1<br>2<br>3<br>4<br>5               | 9.5<br>9.4<br>9.2<br>9.1<br>9.0         | 14<br>12<br>11<br>11<br>11      | 37<br>35<br>33<br>31<br>32       | 16<br>19<br>19<br>18<br>15       | 101<br>125<br>113<br>95<br>82    | 61<br>63<br>238<br>543<br>740          | 117<br>125<br>127<br>118<br>112   | 36<br>47<br>40<br>32<br>27         | 14<br>13<br>11<br>9.8<br>9.4      | 2.7<br>2.7<br>2.9<br>2.5<br>2.7               | 2.6<br>2.6<br>2.4<br>2.2                  | 1.5<br>1.6<br>1.7<br>1.7<br>1.7        |             |
| 6<br>7<br>8<br>9<br>10              | 9.0<br>8.5<br>8.6<br>8.7<br>8.3         | 11<br>12<br>13<br>14<br>14      | 37<br>37<br>30<br>20<br>18       | 14<br>13<br>13<br>13<br>13       | 77<br>88<br>88<br>85<br>86       | 781<br>525<br>424<br>428<br>352        | 105<br>97<br>90<br>83<br>77       | 23<br>21<br>19<br>16<br>14         | 9.0<br>7.9<br>7.6<br>7.2<br>7.2   | 2.5<br>2.5<br>2.4<br>2.2<br>2.3               | 2 . 2<br>2 . 2<br>2 . 2<br>1 . 9<br>1 . 8 | 1.7<br>1.6<br>1.6<br>1.8<br>1.8        |             |
| 11<br>12<br>13<br>14<br>15          | 8.7<br>9.0<br>9.2<br>9.5<br>9.4         | 12<br>12<br>14<br>16<br>17      | 17<br>17<br>18<br>19<br>17       | 13<br>16<br>15<br>16<br>14       | 116<br>147<br>548<br>527<br>321  | 302<br>478<br>875<br>549<br>578        | 98<br>87<br>76<br>69<br>65        | 12<br>11<br>12<br>12<br>12         | 6.6<br>5.7<br>5.2<br>4.9<br>5.4   | 2.1<br>1.8<br>1.7<br>1.6<br>1.5               | 1.8<br>1.9<br>2.3<br>2.6<br>2.4           | 1.8<br>1.9<br>2.0<br>2.1<br>2.2        |             |
| 16<br>17<br>18<br>19<br>20          | 9.5<br>9.7<br>9.8<br>9.6<br>10          | 17<br>21<br>22<br>23<br>23      | 17<br>17<br>16<br>16<br>16       | 12<br>11<br>12<br>12<br>17       | 226<br>186<br>160<br>134<br>111  | 560<br>534<br>556<br>420<br>340        | 58<br>54<br>53<br>48<br>43        | 12<br>11<br>10<br>9.0<br>9.4       | 6.9<br>7.3<br>6.6<br>6.1<br>5.6   | 1.5<br>1.9<br>2.6<br>4.1<br>3.5               | 2.3<br>2.2<br>2.2<br>2.1<br>1.9           | 2.4<br>2.5<br>2.5<br>2.5<br>2.5<br>2.4 |             |
| 21<br>22<br>23<br>24<br>25          | 10<br>10<br>9.9<br>9.4<br>9.4           | 23<br>24<br>23<br>28<br>26      | 16<br>16<br>17<br>17<br>17       | 13<br>13<br>12<br>14<br>41       | 103<br>92<br>88<br>69<br>59      | 289<br>243<br>220<br>224<br>199        | 42<br>38<br>36<br>34<br>30        | 9.4<br>9.4<br>9.4<br>9.8<br>11     | 6.4<br>6.2<br>5.6<br>5.5<br>4.8   | 3.5<br>3.3<br>3.4<br>3.5<br>3.3               | 1.9<br>1.9<br>1.9<br>1.9<br>1.9<br>1.9    | 2.4<br>2.5<br>2.4<br>2.5=<br>2.6       |             |
| 26<br>27<br>28<br>29<br>30<br>31    | 9.6<br>12<br>11<br>11<br>11<br>14<br>14 | 26<br>27<br>53<br>49<br>43      | 17<br>15<br>14<br>14<br>14<br>14 | 51<br>65<br>85<br>65<br>56<br>55 | 54<br>65<br>65<br>               | 178<br>158<br>142<br>125<br>116<br>113 | 29<br>26<br>27<br>29<br>26        | 12<br>13<br>14<br>14<br>12<br>14   | 4.1<br>3.5<br>3.2<br>3.0<br>2.8   | 3.0<br>2.9<br>2.9<br>2.6<br>2.6<br>2.6<br>2.6 | 1.8<br>1.8<br>1.8<br>1.7<br>1.6<br>1.6    | 2.9<br>3.1<br>3.2<br>3.2<br>3.3        |             |
| TOTAN<br>MEAN<br>MAX<br>MIN<br>AC-F | 304.C<br>9.81<br>14<br>8.3<br>603       | 622<br>20.7<br>53<br>11<br>1230 | 651<br>21.0<br>37<br>14<br>1290  | 761<br>24.5<br>35<br>11<br>1510  | 4011<br>143<br>548<br>54<br>796C | 11354<br>366<br>875<br>61<br>22520     | 2019<br>67.3<br>127<br>26<br>4000 | 513.4<br>16.6<br>47<br>9.0<br>1020 | 201.5<br>6.72<br>14<br>2.8<br>400 | 81.3<br>2.62<br>4.1<br>1.5<br>161             | 64.2<br>2.07<br>2.6<br>1.6<br>127         | 67.1<br>2.24<br>3.3<br>1.5<br>133      |             |
| CAL WTR                             | (R 1986 T<br>(R 1987 T                  | OTAL 2815<br>OTAL 2064          | 6.4 MEAN<br>9.5 MEAN             | 77.1 MAX<br>56.6 MAX             | 1760 M<br>875 M                  | IIN 1.7 A<br>IIN 1.5 A                 | C-FT 5585                         | 0                                  |                                   |   |   |  | RECEIVED    |
|                                     |   |                                 |                                  |                                  |                                  |  | 4096                              | 0                                  |                                   |   |   |  | FFR -1 1995 |

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WATER RESOURCES DEPT. SALEM, OREGON

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WATER RESOURCES DEPT. SALEM, OREGON

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UNITED STATES DEPARTMENT OF THE INTERIOR - GEOLOGICAL SURVEY - OREGON OFFICE 12/04/89

STATION NUMBER 14047390 ROCK CREEK AB WHYTE PARK NR CONDON/OREG. STREAM SOURCE AGENCY USGS 297. DATUM 1714.50 STATE 41 COUNTY 021 LATITUDE 451553 LONGITUDE 1200115 DRAINAGE AREA

DISCHARGE, CUBIC FEET PER SECOND, WATER YEAR OCTOBER 1987 TO SEPTEMBER 1988 MEAN VALUES

| DAY                                  | OCT                                       | NOV                                    | DEC                               | JAN                                 | FEB                              | MAR                              | APR                               | MAY  | ИПГ                                | JUL                               | AUG                                  | SEP                              |
|--------------------------------------|---|--|-----------------------------------|-------------------------------------|----------------------------------|----------------------------------|-----------------------------------|--|------------------------------------|-----------------------------------|--------------------------------------|----------------------------------|
| 1<br>2<br>3<br>4<br>5                | 3.C<br>3.C<br>3.C<br>3.2<br>3.3           | 6.0<br>6.0<br>6.1<br>6.1<br>6.4        | 8.1<br>11<br>13<br>12<br>12       | 8.0<br>7.9<br>e7.5<br>e7.5<br>e9.3  | 16<br>13<br>21<br>20<br>18       | 41<br>39<br>38<br>36<br>47       | 28<br>27<br>28<br>30<br>29        | e 57<br>e 57<br>e 57<br>e 57<br>e 55         | e 20<br>20<br>21<br>21<br>21<br>21 | 3.3<br>3.1<br>2.9<br>3.0<br>3.0   | .60<br>.64<br>.71<br>.71<br>.64      | .60<br>.60<br>.63<br>.66         |
| 6<br>7<br>8<br>9<br>10               | 3.5<br>3.6<br>3.7<br>3.7<br>3.7           | 6.6<br>6.7<br>6.7<br>7.0<br>7.0        | 11<br>11<br>10<br>12<br>25        | 9.0<br>9.0<br>9.0<br>9.7<br>63      | 16<br>17<br>18<br>39<br>75       | 51<br>43<br>37<br>41<br>44       | 26<br>24<br>22<br>20<br>18        | e 53<br>e 49<br>e 44<br>e 39<br>e 34         | 25<br>27<br>28<br>27<br>24         | 2.7<br>2.5<br>2.2<br>2.0<br>1.8   | .65<br>.68<br>.71<br>.67<br>.67      | .63<br>.63<br>.64<br>.64<br>.66  |
| 11<br>12<br>13<br>14<br>15           | 3.9<br>4.1<br>4.2<br>4.4<br>4.3           | 6.9<br>7.8<br>8.9<br>8.0<br>7.9        | 30<br>21<br>16<br>13<br>e11       | 46<br>26<br>26<br>164<br>156        | 89<br>80<br>71<br>56<br>53       | 35<br>31<br>28<br>26<br>25       | 17<br>16<br>15<br>14<br>14        | e 30<br>e 28<br>e 26<br>e 25<br>e 25<br>e 25 | 21<br>18<br>16<br>14<br>12         | 1.7<br>1.8<br>1.9<br>1.8<br>1.5   | • 58<br>• 57<br>• 59<br>• 64<br>• 64 | .73<br>.74<br>.81<br>.81<br>.78  |
| 16<br>17<br>18<br>19<br>20           | 4 • 3<br>4 • 4<br>4 • 4<br>4 • 4<br>4 • 7 | 7.7<br>7.3<br>7.2<br>7.2<br>7.2<br>7.2 | e11<br>e11<br>e10<br>e10<br>e10   | 71<br>43<br>31<br>28<br>25          | 53<br>40<br>39<br>33<br>31       | 23<br>21<br>20<br>20<br>20       | 12<br>21<br>82<br>55<br>54        | e23<br>e22<br>e20<br>e18<br>e15              | 11<br>9.5<br>8.8<br>7.9<br>7.0     | 1.4<br>1.3<br>1.2<br>1.1<br>.94   | .69<br>.64<br>.73<br>.77<br>.72      | .79<br>.82<br>.90<br>1.2<br>1.3  |
| 21<br>22<br>23<br>24<br>25           | 4.9<br>4.9<br>4.9<br>4.8<br>4.7           | 7.2<br>7.2<br>7.4<br>7.6<br>7.5        | 11<br>12<br>11<br>e9.5<br>e8.0    | 22<br>20<br>19<br>16<br>16          | 33<br>36<br>32<br>29<br>28       | 19<br>20<br>22<br>24<br>24<br>24 | 230<br>615<br>408<br>220<br>161   | e14<br>e13<br>e11<br>e10<br>e10              | 6.3<br>5.5<br>5.0<br>4.7<br>4.4    | .88<br>.80<br>.78<br>.81<br>.76   | .71<br>.70<br>.70<br>.68<br>.67      | 1.3<br>1.3<br>1.2<br>1.2<br>1.2  |
| 26<br>27<br>28<br>29<br>30<br>31     | 4.8<br>5.0<br>5.3<br>5.6<br>5.7<br>5.8    | 6.9<br>6.9<br>6.9<br>6.9<br>6.6        | e8.0<br>e8.0<br>8.1<br>8.2<br>8.3 | 16<br>16<br>16<br>20<br>28<br>28    | 28<br>32<br>36<br>39             | 24<br>28<br>28<br>28<br>29<br>29 | 136<br>105<br>96<br>e70<br>e57    | e15<br>e17<br>e20<br>e26<br>e25<br>e21       | 4.4<br>4.0<br>3.8<br>3.7<br>3.4    | .74<br>.72<br>.67<br>.67<br>.67   | .64<br>.63<br>.63<br>.62<br>.60      | 1.2<br>1.3<br>1.4<br>1.4<br>1.4  |
| TOTAL<br>MEAN<br>MAX<br>MIN<br>AC-FT | 133.2<br>4.30<br>5.8<br>3.0<br>264        | 211.8<br>7.06<br>8.9<br>6.0<br>420     | 368.2<br>11.9<br>30<br>8.0<br>730 | 972.9<br>31.4<br>164<br>7.5<br>1930 | 1091<br>37.6<br>89<br>13<br>2160 | 941<br>30.4<br>51<br>19<br>1870  | 2650<br>88.3<br>615<br>12<br>5260 | 916<br>29.5<br>57<br>10<br>1820              | 404.4<br>13.5<br>28<br>3.4<br>802  | 49.28<br>1.59<br>3.3<br>.64<br>98 | 20.43<br>.66<br>.77<br>.57<br>41     | 28.10<br>.94<br>1.4<br>.60<br>56 |
| .CAL YR<br>WTR YR                    | 1987 Т<br>1988 Т                          | OTAL 1978<br>OTAL 7786                 | 5.7 MEAN<br>.31 MEAN              | 54.2 MAX<br>21.3 MAX                | K 875 MIN<br>K 615 MIN           | N 1.5 A<br>N .57 A               | C-FT 39240<br>C-FT 15440          |  |                                    |                                   |                                      |                                  |

e Estimated

H David Childs 1806 Thompson The Dalles, DR 97058

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FEB -1 1995

WATER RESOURCES DEPT. SALEM, OREGON

70251 716

Mr. Mike Mattick Instream Water Rights Water Resources Department Commerce Building 158 120th Street NE Salem, Oregon 97310-0210

While You Were Out To 12/10/90 Date Time\_ called of Phone . Telephoned In person **Please call** Wants to see you Will call again **Returned your call** Messa Son S 1058 plication on Taken by **FORM CS 97883** 

## DAVID C. MOON Attorney at Law



OCT 4 1996

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P.O. Box 82 · Eugene, OR 97440 · Phone or FAX: (541) 485-5350

WATER RESOURCES DEPT. SALEM, OREGON

October 4, 1996

Personally Delivered

Oregon Water Resources Department Water Rights and Adjudications Division Commerce Building 158 12th Street N.E. Salem, Oregon 97310-0210

Re: Protest to Proposed Final Order (Application IS 70251)

To Whom It May Concern:

Enclosed please find a Protest to Proposed Final Order for Application IS 70251 on behalf of A. David Childs. Also enclosed is a check for the filing fee of \$200 (Check # 1359).

If anything further is required for this Protest, please contact me. Thanks.

Sincerely,

Daid C. Moon

David C. Moon

cc: Client ODFW

 Bailey; IWR PFO Comments; Miscellaneous Basins Page 2 October 3, 1996

DRAIST

F.4/13

### ODFW COMMENTS AND RECOMMENDATIONS INSTREAM WATER RIGHT PROPOSED FINAL ORDERS

### WRD BASIN: Miscellaneous Basins ODFW FISH DISTRICT: Micellaneous Districts

Note: unless otherwise specified, all comments/changes apply to both the Proposed Final Order (PFO) and the draft Certificate.

1) 70251 (John Day Basin)

The proposed flow for May should be: 32 cfs.

2) 70569 (Umatilla Basin)

The proposed flow for August should be: 8.05 cfs.

3) 70573 (Umpqua Basin)

Flows to satisfy this instream use in Cow Creek released from store water in Galesville Reservoir and therefore not subject to the exemption of human and livestock as they would be if natural flows were used. The proposed condition number 3. exempting human and livestock consumption from being regulated to satisfy use from stored water should be deleted from this draft Certificate.

4) 71480 (Sandy Basin)

The stream reach applied for begins in one County and ends in another. The two counties are, from upper to lower: Clackamas/Multnomah. If only one county can be listed, ODFW requests that is be the county in which the reach terminates, in this case Multnomah.

# RECEIVED

NATER RESOURCES DEPT. SALEM, OREGON Oregon

January 30, 1995



DEPARTMENT OF FISH AND WILDLIFE

Water Resources Department 158 12th Street, NE Salem, OR 97310

RE: Comments; 5 John Day River basin Instream Water Right Technical Reviews; Applications 69960, 70250, 70251, 70263 and 70648.

ODFW has reviewed the subject Technical Reviews and offer the following comments:

#### General Comments

1. ODFW has previously indicated it does not oppose reducing instream water right flow levels from amounts requested to the estimated average natural flow when this is less than requested flows. This is consistent with OAR 690-77-045 (3e).

2. According to OAR 690-77-026 (1), WRD "shall undertake a technical review ... and prepare a report." This subsection further lists 8 [(a) through (h)] mandatory criteria which, at a minimum, must be assessed during the technical review. ODFW has concerns with the apparent level of assessment relative to subsection (c):

OAR 690-77-026 (1) (c)--Assessing the proposed instream water right with respect to conditions previously imposed on other instream water rights granted for use of water from the same source.

In the subject John Day River basin reports of technical review, WRD is proposing to condition each application to exempt human and livestock consumption from regulation in favor of these instream rights as follows:

This instream right shall not apply to permits for appropriation for domestic or livestock use....



2501 SW First Avenue PO Box 59 Portland, OR 97207 (503) 229-5400 TDD (503) 229-5459 WRD; IWR Comments; John Day River January 30, 1995 Page 2

OR

This instream right shall not have priority over human or livestock consumption.

Instream water rights certificates in the John Day River basin based on conversion of minimum perennial streamflows generally contain similar conditioning language giving preference to the listed uses.

By rule, WRD's technical review process includes assessing conditions previously imposed on other instream water rights from the same source. If found to be appropriate, WRD may propose that new instream water rights contain the same exemption. There is no requirement that this exemption be automatically included as a proposed condition.

When ODFW reviewed WRD files on some of these applications for documentation of assessments of prior conditions, we found nothing to document that any such assessments had been done. ODFW, therefore, assumes the required assessments were not done, contrary to rule. ODFW also objects to the routine placement of exemptions on any of the subject applications on the grounds that to do so does not give adequate consideration to the public's interest in maintaining fishery resources in John Day River basin streams. OAR 690-11-195 (4dA).

Specific Comments

Application 70251; Rock Creek; RM 40 to 0--In its water availability analysis, WRD staff find that water is not naturally available to meet even ODFW's recommended minimum flows for fish in May through December. For the months of July through November, the water availability analysis indicates that only about 1/3 of the minimum recommended flow is available. When these calculated flows are compared with other measured flow records, it appears that the estimated average natural flow levels for July through December are potentially erroneous.

The estimated average natural flow and instream water right should be calculated and measured at the mouth of Rock Creek, the downstream limit of this application. Records for USGS gage 14047390 (50% exceedance; 1975-87; RM 40) indicate actual flows (after cumulative withdrawals above) are similar to what WRD staff WRD; IWR Comments; John Day River January 30, 1995 Page 3

• • • • • • • •

|                                    | JUL | AUG | SEP | OCT | NOV  | DEC  |
|------------------------------------|-----|-----|-----|-----|------|------|
| WRD Water Avail-<br>ability (RM 0) | 4.7 | 3.1 | 2.5 | 2.7 | 6.7  | 21.8 |
| USGS Gage Records<br>(RM 40)       | 2.9 | 1.7 | 2.1 | 3.7 | 11.0 | 30.0 |
| Robison, 1991 (RM<br>40)           | 1.8 | 0.7 | 2.3 | 2.6 | 10.6 | 31.9 |

predict would be naturally available at the mouth of Rock Creek, 40 miles downstream.

The numbers above listed as "Robison, 1991" were extracted from WRD's 1991 Hydrology Report #1, "Water Availability for Oregon's River and Streams: Appendix B". Again, these are natural flow predictions (50% exceedance) for a gage 40 miles upstream from the mouth of Rock Creek, the point of natural flow measurement for the proposed instream water right.

Based on the observation that natural stream flows generally increase as a stream progresses downstream, it is doubtful that the flows cited above accurately represent the instream flow picture.

During physical stream surveys conducted by ODFW personnel in 1971, stream flows in Rock Creek were measured at 1 mile intervals for the lower 9 miles. During this survey, numerous active water diversions were noted. Despite the loss of flow at 22 diversions, measured instream flows (e.g., 4.8 cfs at RM 2) often exceeded the estimated average natural flow.

Although this comparison can not be considered conclusive, ODFW believes significant evidence exists to cast doubt on the results of the water availability analysis performed for this application and is the basis for our objection to same.

Application 70250; Bridge Creek; RM 19 to 13--WRD's water availability analysis indicates water is not naturally available to meet ODFW's recommended minimum flows 10 months out of 12, May through February. There are no gage records available to us for comparison here. We do, however, have limited instream flow measurements taken in July, 1971, that indicated the estimated average natural flow presented in this technical review underestimate natural flow. WRD; IWR Comments; John Day River January 30, 1995 Page 4

The water availability analysis predicts less than one cfs would be available naturally in Bridge Creek during July. ODFW's measurements during July, 1971, recorded a flow at RM 13 of 7.2 cfs after an observed 7 active diversions. Although not conclusive evidence, these measurements, coupled with anecdotal information obtained from field personnel, leads ODFW to believe sufficient doubt exists as to the accuracy of the water availability analysis completed for Bridge Creek.

#### Application 70263; Bear Creek; RM 11 to 0

The situation on the lower 11 miles of Bear Creek is similar to that of Bridge Creek to which it is tributary. Although no gage data exists for comparison, flow measurements taken by ODFW in July, 1971, recorded flows between 2.2 and 6.2 cfs in this stream section. ODFW district personnel indicate that these observed levels of flow are not extraordinary.

Thank you for this opportunity to review the subject technical reports. We appreciate WRD's efforts to move forward with these applications and encourage you to proceed to certification as quickly as possible.

Sincerely,

(antitude)

 Stephanie Burchfield
 Water Resources Program Manager Habitat Conservation Division

c. Unterwegner, John Day Lauman/Eddy, La Grande WaterWatch of Oregon (public information request)

File: WRD/Instream Water Right/Comments

A David Childs Star Rt., Arlington, OR 97812 (503) 454-2827

March 16, 1988

FOREST SUPERVISOR Umatilla National Forest 2517 S. W. Hailey Avenue Pendleton, Oregon 97801

Written comment on Forest Plan

AUG 1 2 199.

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WATER RESOURCES DE SALEM, OREGON

Rock Creek, Gilliam County, flows northwest from the Blue Mountains and the Umatilla National Forest for about 75 miles and outlets to the main stem of the John Day river at McDonald Ferry, approx. 21 miles upstream from the Columbia at I-84. The headwaters, mostly 4000 ft elevation with a small area up to 5000 ft, are in timber and grazing lands.

The stream gauging station is below all of the major tributaries and all of the mountain drainage. Equally significant, the gauging station is above the out-of-stream withdrawals.

Pertinent information.

Years of record 1975 till present

Max annual flow 90,000 acre feet

Min annual flow 4,500 acre feet

Irrigation withdrawals vary from 1500 to 2500 acre feet depending on when the watershed dries up.

Time between summer dry-up and fall flow-through to mouth, varies from 1 to 6 months.

Mean annual flow 1975 - 1985 is 45,500 acre feet/year (USGS EASTERN OREGON 1985)

Correlation with adjoining gauged streams, of the 1905 to 1965 era, predicted the gauged flow would be under 15,000 acre feet/year. (OREGON STATE ENGINEER 1968)

Pioneer settlement on Rock Creek started in the 1860s. Water rights dated after the 1890s are not now filled beyond June. Others only days longer.

Most years during July, August, September there is no usable flow for

any water right or for resident fishery. Former upper rearing areas are intermittently and sparsely puddled with warm water.

During the drought of the 1930s the stream never dried in places that have dried annually the last few years.

Historically, the bottom lands along the stream were irrigated early in the growing season, with water for all users and a surplus for recharge. Irrigators understood that parts of the stream would be dry for as long as a month during August.

The native runs of anadromous fish adapted with this environment many centuries prior. Even through the drought years of the 1930's the timbered slopes nurtured the headwater trickles and seeps, springs and rivulets, and the fry and fingerlings. The headwater tributaries are no longer viable as rearing areas.

Downstream landowners are getting mud and flood with regularity. High-volume, high-velocity runoff events are annually ripping and devastating the riparian areas and the alluvial unprotected zones behind them. Landowners are discouraged by these events. The devastation saps both energy and creativity in focusing only on repair and salvage. We need enhancement.

Transit water is unruly and apparently unavoidable under present watershed management practices.

Sections of streams that have never gone dry before, now become bone dry; yet are receiving the impact of a twenty year runoff event at intervals of only 2 to 5 years.

A stream that historically annually flowed on the order of two to twenty thousand acre-feet is flowing at a volume of 4,500 to 90,000 acre feet.

A flow of 12,000 ac ft, with a reliability of eight years out of ten, now flows at an average of forty five thousand acre feet annually.

Rock Creek once maintained large resident and anadromous fish populations. Currently there are two remnant steelhead spawning areas, both dependent on downstream basalt and gravel aquifers.

Through both luck and error the genes for restocking the watershed are surviving.

The Forest Plan omits Rock Creek tributaries, in Wheeler and

. ....

Morrow Counties, entirely from its riparian plan, yet five or six Rock Creek tributaries and former rearing areas are in the Umatilla Forest.

The Forest plan states, runoff is tied directly to annual precipitation. This assumption is questionable. The nature of a forest is to buffer flows and to carry groundwater in a reserve account. The present flows are probably dependent on the excellent water years of the early to mid-eighties.

The streams have excellent potential for restored spawning and rearing areas. The potential for both commercial and recreation fishery benefits is considerable. The multi-use benefits for upstream spawning and rearing and downstream recreation, fishery, and agriculture seem to have merit. Upper stream rearing water is the need of fishery. Reduction of devastating floods and drought is the need of agriculture. It would seem that a joint effort would be synergetic: more trees and grass in the uplands, sustained high quality rearing water, reduction of high flows, and dual purpose water for fish and agriculture.

Agriculture users are generally below the rearing areas. The water, after going through rearing areas, could be used to sustain vegetation in the riparian zone.

Currently, highwater devastation is more of a critical problem than summer drought to agriculture. The downstream area ranchers are looking for protection and are taking a new look at a growing problem.

++ The designation of the headwaters of Rock Creek E 1 seems to discourage future improvement or water enhancement.

++ The downstream land owners are being whipsawed by a Jekyll and Hyde water system ( too much in February and March and none after the middle of June) Water once was of great benefit both environmentally and economically.

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|---------------------|--------|-------|---------------|----------|-----------|-------|--------|--------|------------|--------|---------|----------|
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| Work Sheet<br>D-658 |        | Pro   | Dose          | TO       | INST      | YEAH  | n Wa   | iTER   | RIG        | HT     | - (2    | Z)       |
| 1                   |        |       |               |          |           |       |        |        |            |        |         |          |
|                     | act    | NOV   | DEC           | JAN      | FEB       | MARch | April  | MAY    | JUNE       | July   | AUG     | SEPT     |
| F3/sec              | 34     | 34    | 34            | 34       | 57        | 57    | 57     | 57     | 34         | 34     | 34      | 34       |
| Maar Floo           |        |       |               | 1        |           |       |        |        |            | 70     | 77      | 17       |
| 1476/77             | 2.7    | 3.53  | 3.89          | 4.58     | 5.68      | 11.7  | 21.7   | 14.9   | 3.03       | 30     | 1.36    | .12      |
| 1977/78             | .38    | 9.8   | 512           | a12/2    | 134       | TPL   | 5/29   | 28     | 5.47       | 5.51   | ,88     | 2.13     |
|                     | 0      | 1.0   | - Aller and a |          |           | 1.    |        | 20     |            |        |         |          |
| 1978/79             | 2.23   | 3.61  | 340           | 9.86     | 205       | 248   | 204    | 99.8.1 | 8.58       | 2.81   | 6.60    | 1.11     |
| langles             | 5 00   | 07/   | antitent)     | 10.01077 | mandidara | 170   | -7 Q   | 252    | 1111       | 1120   | 130     | 1.90     |
| 19/19/30            | 3,35   | 23.1  | THE.          | Lisp     | 1203      | 127   | 52.7   | 20.3   | 19.1       | 4.50   | 1.30    |          |
| 1980/81             | 3.30   | 757   | 18.0          | 15.0     | 927       | 23.9  | 16034  | 51.5   | 39.9       | 4.04   | .66     | .68      |
|                     |        |       |               |          |           |       |        |        |            |        | 10      |          |
| 1981/82             | - 3.13 | 14.2  | 1813          | the B.   | 342       | 214   | 140    | 39.4   | 14.4       | 4.50   | ,69     | 1.81     |
| 1982/83             | 9.55   | 17.8  | SIA           | 134      | 288       | 4.67  | 158    | 298    | 24.3       | 9.89   | 3.81    | 4.62     |
| $\sum$              |        |       | 0017          |          |           |       |        |        |            | 0      |         |          |
| 1983/84             | 8.4    | 23,1  | Tost          | 1175     | 153       | #39   | 396    | 134    | 283.8      | (14,1) | 5.08    | 9.53     |
| inoulau             | 1,20   | \$2=0 | Hantes        | zimi.    | WENES     | 220   | 2.77   | 222    | 120        | 202    | 210     | 512      |
| 1984/85             | 13.7   | DEDRY | USEE          | Jump     | KU Di     | 6-6-0 | Leikit | 54.0   | 16.7       | 2.02   | 2.10    | 5,62     |
| 1985/86             | 11.8   | 11.8  | 23,9          | WIB3     | #34       | 254   | 52.4   | 28.4   | 10.9       | 3.84   | 2.31    | 5.22     |
|                     | 0.11   | 2 - 7 |               |          | 1110      |       |        |        |            | - 17   | - 1 -   |          |
| 1986/87             | 9.8/   | 20.1  | 21.0          | 24.5     |           | 566   | 613    | 16.6   | 6.72       | 2.62   | 2.07    | 2.24     |
| 1987/84             | 4.3    | 7.06  | 11.9          | 31.4     | 37.6      | 30.4  | 88.3   | 29.5   | 13.5       | 1.59   | . 10/0  | .94      |
| 1987/89             | 2.16   | 7.96  | 15.5          | 31.5     | 65.4      | 326   | 137    | 53.5   | 7.21       | 1.29   | .74     | 1.03     |
| MET                 | 0      | 1     | 7             | 7        | 10        | 10    | \$12   | . 3    | 2          | 0      | 0       | 0        |
| 1. Ursmat           | 0      | 1     | R             | 7        | 6         | 9     | 9      | 2      | 1          | 0      | 0       | 0        |
| total               | 0      | 2     | 10            | 14       | 176       | 20    | 198    | 5      | 3          | 0      | 0       | 0        |
| 244RS               | 0%     | 0.8%  | 40%           | 87 /2%   | 71%       | 84%   | 19%    | 29%    | 17%        | 0%     | 0%      | 0%       |
| - for               | 13     | 9     | 6             | 2        | 2         | 2     | 2      | 7      | 10         | 11     | 11      | 11       |
| )/me                | 12     | 11    | 3             | n h      | 7         | 2 4   | 7      | 3      | 10         | 13     | 13      | 74       |
| - F/-               | 0      | 0     | Y             | V        | V         | V     | V      | N      | N          | Ø      | Ø       | Ø        |
|                     |        |       | /             | /        | /         | /     | /      |        |            |        |         |          |

| Work Sheet<br>D-658 | Ister    | ABOVE  | CAYN  | SE GAN  | vor Pa | & Creak      | ',      |           |                    |      |        |      |
|---------------------|----------|--------|-------|---------|--------|--------------|---------|-----------|--------------------|------|--------|------|
| )                   | 34       | 34     | 34    | 34      | 57     | 57           | 5-7     | 57        | 34                 | 34   | 34     | 34   |
|                     | Ođ       | NOU    | DEC   | JAN     | FeB    | Maech        | April   | MAY       | JUNE               | July | August | Sept |
| Mean                |          | Sec.   |       |         |        |              | -       | /         |                    | /    |        |      |
| Monthly             |          |        |       |         |        |              |         |           |                    |      | 4.     |      |
| 1965 /66            | 3.48     | 6.96   | 6.61  | 16.3    | 12.4   | 111          | HG7     | 5.08      | 2.58               | 1090 | 2.04   | 0.19 |
| 1966/67             | <b>A</b> | 题      | •     |         |        |              |         |           |                    |      |        |      |
| 1916/67             | : 88     | 20.2   | 65.6  | White B | 86.1   | 62:7         | 112     | \$37/     | 7.33               | ,70  | .06    | .06  |
| 1967/68             | 122      | 348    | 126   | 1918    |        |              |         |           |                    |      |        |      |
| 1967/68             | ,39      | 1.16   | 4.06  | 15.9    | 40.1   | 18.3         | 6.86    | 3.41      | 1.62               | v/0  | .00    | ,00, |
| 1968/69             | .64      | 4.3    | 31.8  | 46.9    | 97,5   | 264          | 262     | 34.1      | 14.9               | 3.37 | .33    | .73  |
| 1969/70             | 1.41     | 4.28   | 9.72  | ECH     | 1/25   | 149          | 58      | 22.8      | 6.00               | 1.23 | ,26    | 1.Z/ |
| 1970/71             | 1:56     | 6.71   | 16.2  | 122     | 54.4   | 10h          | al g    | 25.3      | 9.10               | ,92  | .03    | .47  |
|                     | ·        |        |       |         |        |              |         |           | Zday               |      |        |      |
| 1971/22             | .98      | 7.3    | £19.5 | 8519    | \$148  | 2374         | 57.01   | 24.5      | (67)               | .50  | .14    | .15  |
| 1972/73             | .87      | 3.47   | 21.9  | 45.3    | 24.1   | 57.4:        | 26.9    | 4.01      | ,72                | < 10 | Flow   | ~    |
| 1973/74             | ,15      | the la | 247   | 470     | 120    | 19.63        | 17 Car  | 45.Z      | 5.96               | .88  | .20    | . 17 |
| in all              |          | 0.04   |       | - 1 -   |        | at 1 de Dans | 2:51-17 | BAN ARCAS |                    | - 17 |        |      |
| 1979/75             | , (25    | 231    | 4.93  | 31.5    | OL 9   | CT.O.S.      | CCA     | 103-9401  | 6.13               | 2.61 | 012    | 0.12 |
| 1975/76             | ,76      | 4.11   | 15.1  | testa   | 32.8   | V.S.M        | 126     | 17.6      | 4.39               | .26  | 5.84   | 2.73 |
| HAOS KO             |          |        |       |         |        |              |         |           |                    |      |        |      |
| Flow                | 00       | 1      | 3     | 7       | 6      | 9            | 9       | 2         | 2 dy S<br>1-minuth | 0    | 0      | 0    |
|                     |          |        |       |         |        |              |         |           |                    |      |        |      |
| -                   |          |        |       |         |        |              |         |           |                    |      |        |      |
| $\sum$              |          |        | 1.4.5 |         |        |              |         |           |                    |      |        |      |
|                     |          |        |       |         |        |              |         |           |                    |      |        |      |
|                     |          |        |       |         |        |              |         |           |                    |      |        |      |

September 17, 1990

AUG 1 2 1991 To: A David Childs Fax 298-4106

From: E. George Robison OWRD WATER RESOURCES DEPT Salem OR. SALEM OREGON Concerning: "Natural" flows for three streams in John Day Basin Salem OR.

On this page are the tabulations for the streamflows from the streams you asked for. I did not include the figures to save space.

| Rock Cr | at Parkers | Mill (Natural Flows   | Rock Cr. | at Butter I | Milk (Natur | al Flow) |
|---------|------------|---|----------|-------------|-------------|----------|
| Monthe  | Pred5      | Pred? <p %<="" td=""><td>Months</td><td>Pred5</td><td>Pred2</td><td></td></p> | Months   | Pred5       | Pred2       |          |
| TAN     | 11000      | 27 MM   | IAN      | 13.3        | 40.8        |          |
| JAN     | 1.1        | 5.7   | FFR      | 23.1        | 78.4        |          |
| FEB     | 1.9        | 0.9   | MAD      | 378         | 114.4       |          |
| MAR     | 3.1        | 9.6   | ADD      | 317         | 79.0        |          |
| APR     | · 2.5      | 6.9   | APR      | 21.7        | 34.6        |          |
| MAY     | 1.7        | 3.4   | MAY      | 21.2        | 12.7        |          |
| JUN     | 0.6        | 1.3   | JUN      | 1.3         | 15.7        |          |
| JUL     | 0.1        | 0.4   | JUL      | 1.5         | 3.5         |          |
| ALIG    | 0.0        | 0.1   | AUG      | 0.4         | 1.3         |          |
| SED     | 0.0        | 0.1   | SEP      | 0.5         | 13          |          |
| oor     | 0.0        | 0.2   | OCT      | 0.8         | 1.8         |          |
| NOV     | 0.1        | 0.2   | NOV      | 2.2         | 5.2         |          |
| NOV     | 0.2        | 0.5   | DEC      | 5.9         | 14.8        | i        |
| DEC     | 0.5        | 1.3   | DEC      | 2.5         |             |          |

6.0 = Basin No.15.0 = Drainage Area

- 18.0 = Precipitation
- 0.0 = WR Index

6.0 = Basin No. 166.0 = Drainage Area 17.0 = Precipitation 0.0 = WR Index

Buckhorn Cr. at RM 1.6 (Natural Flow) Months Prods Prod?

| WOnus | rieds  | rieuz   |  |
|-------|--|---|--|
| JAN   | 2.5  | 8.4   |  |
| FEB   | 4.4  | 16.6  |  |
| MAR   | 7.3  | 23.6  |  |
| APR   | 5.7  | 15.5  |  |
| MAY   | 3.4  | 6.5   |  |
| JUN   | 1.1  | 2.3   |  |
| JUL   | 0.2  | 0.6   |  |
| AUG   | 0.1  | 0.2   |  |
| SEP   | 0.1  | 0.2   |  |
| OCT   | 0.1  | 0.3   |  |
| NOV   | 0.4  | 1.0   |  |
| DEC   | 1.1  | 2.9   |  |
|       | JAN<br>FEB<br>MAR<br>APR<br>MAY<br>JUN<br>JUL<br>AUG<br>SEP<br>OCT<br>NOV<br>DEC | JAN       2.5         FEB       4.4         MAR       7.3         APR       5.7         MAY       3.4         JUN       1.1         JUL       0.2         AUG       0.1         SEP       0.1         OCT       0.1         NOV       0.4         DEC       1.1 | MonusFredsFredsJAN2.58.4FEB4.416.6MAR7.323.6APR5.715.5MAY3.46.5JUN1.12.3JUL0.20.6AUG0.10.2SEP0.10.2OCT0.10.3NOV0.41.0DEC1.12.9 |

6.0 = Basin No.

- 36.0 = Drainage Area
- 17.0 = Precipitation

These ARE The TRIBUTARY Flows to The GAGE Statud Requesting 34 cts IN July Aug Septydot

### BRELEENEIN

WATER RESOURCES DEPT. SALEM, OREGON 70251

JAN 1 4 1991

Gilliam County Soil and Water Conservation District Courthouse - P.O. Box 106 - Condon, OR 97823 - (503) 384-2671

January 9, 1991

App Amlegate

William H. Young, Director Water Resources Department 3850 Portland Road, NE Salem, Oregon 97310

Dear Mr. Young,

Late in November of 1990, the Oregon Department of Fish and Wildlife requested 35 CFS of water in Rock Creek, a tributary of the John Day River Located in Gilliam and Morrow Counties. We ask you to deny this request.

The Gilliam, Morrow, and Wheeler Soil and Water Conservation Districts (SWCD's) have actively engaged in writing a Coordinated Resource Management Plan (CRMP) for the Rock Creek Watershed. The CRMP is addressing soil and water problems, as well as conservation and improvements of the resource base including fish habitat.

The CRMP process involves extensive input from all watershed users. We have held several meetings in the counties to receive input from the users, including Fish & Wildlife. It is crucial that we continue to get a cooperative effort from the users. To impose a 35 CFS streamflow regulation at this time could severely damage the cooperative spirit necessary to write the CRMP because it singles out a specific watershed user and makes the local work appear futile.



Gilliam County Soil and Water Conservation District Courthouse - P.O. Box 106 - Condon, OR 97823 - (503) 384-2671

As mentioned earlier, one of the goals of the CRMP is to protect and improve existing resource bases, including fish habitat. This also appears to be your goal. We ask that in light of our area developing a CRMP, you note that proper timing and cooperation may do more to promote fish habitat and holistic improvement of the watershed than to impose a streamflow quota.

We urge you to let the CRMP process work and thus deny the water right request at this time.

Sincerely yours,

Paul Bato

Paul Bates, Chairman Gilliam Soil and Water Conservation District

PB/ckr

Y.

cc: Water Resources Commission Morrow SWCD Wheeler SWCD Andy Rose, Rock Creek Watershed Planner

MORROW ten Cons Pit

P. O. BOX 127 HEPPNER, OREGON 97836

JAN 2 2 1991

WATER RESOURCES DEPT. SALEM, OREGON

January 11, 1991

William H. Young, Director Water Resources Department 3850 Portland Road NE Salem, Oregon 97310

Dear Mr. Young,

Late in November 1990, the Oregon Department of Fish and Wildlife requested 35 cfs of water in Rock Creek, a tributary of the John Day river, located in Gilliam and Morrow Counties. We ask you to deny this request in conjunction with Gilliam County Soil and Water Conservation District.

The Gilliam, Morrow, and Wheeler Soil and Water Conservation Districts (SWCD's) are actively engaged in writing a Coordinated Resource Management Plan (CRMP) for the Rock Creek Watershed. The CRMP is addressing soil and water problems as well as conservation and improvements of the resource base including fish habitat.

The CRMP process involves extensive input from all watershed user and several meetings have been held to gather input from the users, including ODF&W. To impose a streamflow regulation could severely damage the cooperative spirit necessary to write the CRMP.

The Board of Directors of Morrow SWCD urge you to let the CRMP process proceed and deny the water right request at this time.

Joe Rietmann, Chairman Morrow SWCD

DEAN MONTHLY FLOWS FOR ROCK CREEK, TRIB JOHN DAY RIVER BASED ON BEAVER CREEK NEAR PAULINA, GAGE 14-0780

-

|     | MEAN    | a       | A      | S     | St   | E      |
|-----|---------|---------|--------|-------|------|--------|
|     | FLOW    |         | 522.00 | 57.90 | 1.42 | 4.60   |
|     |         |         |        |       |      |        |
| OCT | 94.47   | .00134  | 93.98  | 1.00  | .61  | 1.00   |
| NOV | 52.81   | .00303  | 214.67 | 1.00  | .85  | 1.00   |
| DEC | 135.64  | .00328  | 241.77 | 1.00  | .90  | 1.00   |
| JAN | 127.54  | .11     | 306.67 | 1.00  | 1.00 | 1.00   |
| FEB | 205.71  | .928    | 345.39 | 1.00  | 1.00 | 1.00   |
| MAR | 302.56  | 4.26    | 188.23 | 1.00  | 1.00 | .06    |
| APR | 816.51  | .0202   | 351.93 | 1.00  | .84  | 1.00   |
| MAY | 681.61  | .0195   | 472.27 | 2.99  | .88  | 1.00   |
| JUN | 1027.88 | 2.82e-8 | 408.96 | 1.00  | .77  | 137.84 |
| JUL | 196.37  | .00541  | 61.03  | 1.00  | .77  | 1.00   |
| AUG | 93.70   | .00129  | 67.03  | 1.00  | .60  | 1.00   |
| SEP | 84.73   | .000965 | 88.28  | 1.00  | .57  | 1.00   |
|     |         |         |        |       |      |        |

Did Not use these #'s for flow. Do vot book realistic.

29753 mbs @RM40.8 Report for station 14047330 ROCK CREEK AB WHYTE PARK NE CONDON, GREG. 0 GMEAN DISCHARGE ONumber of years retrieved is 16 ROCK CREEK AB WHYTE PARK NE CONDON, GREG. 1 Station 14047390 MEAN DISCHARGE Statistics on Normal monthly means (All days) Feb March Jan Oct Nov Dec April June May By rows (Number, Mean, Variance, Standard Deviation, Skewness, Coefficient of Variation 14.80 ØNumber 14.00 14.00 14.00 14.00 14.00 14.00 14.00 14.00 154.23 OMean 5.39 14.38 45.06 71.37 212.79 132.24 62.34 17.7: OVar 2563.35 15526.32 21791.44 10665.82 2238.22 19.07 176.11 5714.94 451.96 124.60 **GStd** 50.63 147.62 4.37 13.27 47.31 103.28 75.60 21.28 1.39 OSkew 0.75 2.14 2.27 0.22 6.34 1.49 2.70 2.68 6.81 0.71 **ØCvar** 6.69 6.81 0.89 1.95 6.78 1.21 1.19 21.26 0Pavg 2.95 9.84 29.33 18.23 8.59 2.45 6.74 6.21 1 Station 14047390 ROCK CREEK AB WHYTE PARK NE CONDON, GREG. 0 MEAN DISCHARGE Guartiles of Normal monthly means (All days) Oct Nov Dec Jan 0 Twenty-Fifth Percentile 2.18 6.25 15.4 29.7 0 Fiftieth Percentile 3.43 10.8 27.2 55.8 0 Seventy-Fifth Percentile 9.61 21.3 57.5 120.2 April July May June 0 Twenty-Fifth Percentile 55.8 24.5 1.51 6.41 Fiftieth Percentile 0 112.6 30.9 3.32 11.9 Seventy-Fifth Percentile G 169.4 65.1 4.75 16.9 ROCK CREEK AE WHYTE PARK NE CONDON, GREG. 1 Station 14047390 MEAN DISCHARGE 0 144pas ave ennuel 592 RMAD.8 Quartiles of Normal annual means (All days) Lopolat yyule Twenty-Fifth Percentile 0 30.8 0 Fiftieth Percentile 55.3 θ Seventy-Fifth Percentile 79.6 NOTE -- PERCENTILES BASED ON AVAILABLE DATA. 1

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|   | July                |    | Aug              | Sept            |  |
|---|---------------------|----|------------------|-----------------|--|
| , | Percentage<br>14.00 | of | Average<br>14.00 | Value)<br>14.∂0 |  |
| 9 | 4.10                |    | 2.40             | 2.81            |  |
| 5 | 14.24               |    | 4.79             | 6.62            |  |
| 5 | 3.77                |    | 2.19             | 2.57            |  |
| 3 | 1./4                |    | 1.95             | 1.50            |  |
| 5 | 0.32                |    | 0.31             | 6.31            |  |
| 5 | 0.57                |    | 0.00             | 0.00            |  |
|   |                     |    |                  |                 |  |
|   | Feb                 |    | Ma               | arch            |  |
|   | 58.4                |    | 5                | 73.8            |  |
|   | 124.6               |    | 23               | 20.9            |  |
|   | 230.0               |    | 30               | 5.8             |  |
|   |                     |    |                  |                 |  |
|   |                     |    |                  |                 |  |
|   | Aug                 |    | ٤                | Sept            |  |
|   | .683                |    |                  | 1.01            |  |
|   | 1.68                |    |                  | 2.92            |  |
|   | 4.13                |    |                  | 4.77            |  |
|   |                     |    |                  |                 |  |
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BASIN SUMMARY REPORT ROCK CR TRIBUTARY OF JOHN DAYR Jur 2025 Support # 10479

Page 2

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45.31 TOTAL CFS: 0.00 TOTAL ACF:

TOTALS BY USE ------

|       | AGRICULTURE | INDUSTRIAL | MUNICIPAL | DOMESTIC | RECREATIONAL | MISCELLANEOUS |
|-------|-------------|------------|-----------|----------|--------------|---------------|
| (CFS) | 45.31       | 0.00       | 0.00      | 0.00     | 0.00         | 0.00          |
| (ACF) | 0.00        | 0.00       | 0.00      | 0.00     | 0.00         | 0.00          |

BASIN SUMMARY REPORT ROCK CR TRIBUTARY OF JOHN DAY R

Jul 70251

# TOTAL DIVERTED

TOTAL CFS: 37.40 TOTAL ACF: 9.62

TOTALS BY USE



| •     | AGRICULTURE | INDUSTRIAL | MUNICIPAL | DOMESTIC | RECREATIONAL | MISCELLANEOUS |
|-------|-------------|------------|-----------|----------|--------------|---------------|
| (CFS) | 37.30       | 0.00       | 0.00      | 0.00     | 0.00         | 0.10          |
| (ACF) | 5.62        | 0.00       | 0.00      | 0.00     | 0.00         | 4 = 00        |

Page 3

| R | ٨ | S | T | N | S | υ | M | M | A | ĸ  |    | R | E | Ρ | 0 | R | Т |  |
|---|---|---|---|---|---|---|---|---|---|----|----|---|---|---|---|---|---|--|
| U | ~ | 5 | - |   |   |   |   |   |   | -0 | 10 |   |   |   |   |   |   |  |

BASIN JULARY TO JOHN DAY RIVER PRIMARY

|                |        |         |     | RC   | OCK CREEK | ( #10479, | INIDO | Die      | TAVER | PRIMA  | RY   |            |             |        |
|----------------|--------|---------|-----|------|-----------|-----------|-------|----------|-------|--------|------|------------|-------------|--------|
| • CERTIFICATE  | PERMIT | DLC LOT | 1/4 | 1/4  | SECTION   | TOWNSHIP  | RANGE | RATE     | UNITS | P.A.S. | USE  | PRIORITY   | STREAM NAME | STATUS |
|                |        |         |     |      |           |           |       |          |       |        |      |            |             |        |
| 6258 D         | 25/95  |         | NE  |      | 21        |           | 20F   | 0 = 0000 |       | D      | 10   | 12/71/1069 | POCK CR     | V      |
| 46866 D        | 25485  |         | NE  | SE   | 24        | IN        | 205   | 0=0000   |       | P      | IR   | 12/31/1000 | ROCK CR     | v      |
| 25115 D        | 25115  |         | NE  | IN W | 24        | IN        | 201   | 0-0000   |       | P      | IR   | 12/31/1000 | ROCK CR     | v      |
| 43564 D        | 25116  |         | SU  | C.E. | 11        | 1.11      | 10F   | 0 = 0000 |       | P      | IR   | 12/31/1007 | ROCK CR     | v      |
| 24941 D        | 2/9/1  |         | DW  | SE   | 11        | IN        | 196   | 0 = 0000 |       | P      | IR   | 12/31/1009 | ROCK CR     | v      |
| 24851 D        | 2/ 851 |         |     |      | 0         | 0         | 0     | 0 = 0000 |       | P      | LV   | 12/31/10/3 | ROCK CR     | v      |
| 2/852 D        | 24051  |         |     |      | 0         | 0         | 245   | 0 = 0000 |       | P      | LV   | 12/31/10/0 | ROCK CR     | v      |
| 25315 D        | 24052  |         | SE  | SE   | 35        | 50        | 200   | 0-0000   |       | P      | 1 25 | 12/31/10/0 | ROCK CR     | v      |
| 25036 0        | 25034  |         |     |      | 0         | 0         | 0     | 0.0000   |       | P      | 1 74 | 12/31/10/9 | ROCK CR     | V      |
| 30828          | 25050  |         | NE  |      | 0         | 0         | 205   | 0.0000   |       | P      | IL   | 12/31/1000 | ROCK CR     | V      |
| 24954 D        | 22037  |         | NE  | SE   | 24        | IN        | ZUE   | 0 = 0000 |       | P      | IR   | 12/31/1003 | ROCK CR     | V      |
| 24934 0        | 24954  |         |     |      | 0         | 0         | 0     | 0-0000   |       | P      | IR   | 12/31/1884 | RUCK CR     | V      |
|                | 20000  |         |     |      | 0         | 0         | 0     | 0-0000   |       | P      | IR   | 12/31/1004 | RUCK CR     | V      |
| 23023 U        | 20820  |         |     |      | 0         | 0         | 0     | 0_0000   |       | P      | 1*   | 12/31/1884 | RUCK CR     | V      |
| 40807 D        | 25839  |         | NE  | NW   | 24        | 1N        | ZOE   | 0 0000   |       | P      | IR   | 12/31/1884 | RUCK CR     | V      |
| • 25514 U      | 25514  |         |     |      | 0         | 0         | 0     | 0=0000   |       | Р      | IR   | 12/ 3/1885 | RUCK CR     | V      |
| 25061 U        | 25061  |         |     |      | 0         | 0         | 0     | 0.0000   |       | P      | IR   | 12/31/1886 | ROCK CR     | V      |
| 36590 D        | 25991  |         | SW  | SE   | 32        | 1N        | 21E   | 3=2750   | CFS   | P      | I ×  | 12/31/1886 | ROCK CR     | V      |
| 25778 D        | 25778  |         |     |      | 25        | 15        | 21E   | 0.0000   |       | Р      | IR   | 12/31/1887 | ASPR        | V      |
| 25316 D        | 25316  |         |     |      | 0         | 0         | 0     | 0.0000   |       | Р      | I*   | 12/31/1888 | ROCK CR     | V      |
| 24851 D        | 24851  |         |     |      | 0         | 0         | 0     | 0_0000   |       | Р      | IR   | 12/31/1890 | ROCK CR     | V      |
| ● 25214 D      | 25214  |         |     |      | 0         | 0         | 0     | 0_0000   |       | Р      | IR   | 12/31/1890 | ROCK CR     | V      |
| 25988 D        | 25988  |         |     |      | 0         | 0         | 0     | 0.0000   |       | P      | I *  | 12/31/1890 | ROCK CR     | V      |
| 24888 D        | 24888  |         |     |      | 0         | 0         | 0     | 0.0000   |       | Р      | IR   | 12/31/1892 | ROCK CR     | V      |
| ● 25192 D      | 25192  |         |     |      | 0         | 0         | 0     | 0.0000   |       | Р      | IR   | 6/20/1893  | ROCK CR     | V      |
| 25230 D        | 25230  |         |     |      | 0         | 0         | 0     | 0.0000   |       | Р      | IR   | 12/ 3/1893 | ROCK CR     | ۷      |
| 25498 D        | 25498  |         |     |      | 0         | 0         | 0     | 0.0000   |       | Р      | I×   | 12/31/1893 | ROCK CR     | ۷      |
| a 25159 D      | 25159  |         |     |      | 0         | 0         | 0     | 0_0000   |       | Р      | I *  | 12/31/1894 | ROCK CR     | ۷      |
| 25895 D        | 25895  |         |     |      | 0         | 0         | 0     | 0 0000   |       | Р      | IR   | 12/31/1894 | ROCK CR     | ۷      |
| 46868 D        | 25989  |         | NE  | NW   | 24        | 1N        | 20E   | 0 0000   |       | Ρ      | Ι×   | 12/31/1894 | ROCK CR     | V      |
| <b>25113</b> D | 25113  |         |     |      | 0         | 0         | 0     | 0 0000   |       | Р      | IR   | 12/31/1895 | ROCK CR     | ٧      |
| 25113 D        | 25113  |         |     |      | 14        | 15        | 21E   | 0_0000   |       | Ρ      | IR   | 12/31/1895 | SPRINGS     | ٧      |
| 25756 D        | 25756  |         |     |      | 0         | 0         | 0     | 0.0000   |       | Р      | IR   | 12/31/1895 | ROCK CR     | ٧      |
| 25779 D        | 25779  |         |     |      | 0         | 0         | 0     | 0_0000   |       | P      | IR   | 12/31/1895 | ROCK CR     | ٧      |
| 25878 D        | 25878  |         |     |      | 0         | 0         | 0     | 0.0000   |       | Р      | I*   | 12/31/1895 | ROCK CR     | ٧      |
| 25191 D        | 25191  |         |     |      | 0         | 0         | 0     | 0_0000   |       | P      | IR   | 12/31/1896 | ROCK CR     | V      |
| 47603 D        | 25203  |         | SW  | NE   | 15        | 1N        | 20F   | 0_0000   | CES   | Р      | Ι×   | 12/31/1896 | ROCK CR     | V      |
| 25630 D        | 25630  |         |     |      | 0         | 0         | 0     | 0_4700   | CIS   | P      | IR   | 12/31/1897 | ROCK CR     | v      |
| 25744 D        | 25744  |         |     |      | 0         | 0         | 0     | 0_0000   |       | P      | IR   | 12/31/1899 | ROCK CR     | v      |
| - 25673 D      | 25673  |         |     |      | 0         | 0         | 0     | 0.0000   |       | P      | IR   | 12/31/1900 | ROCK CR     | V      |
| • 40744 D      | 25044  |         | NE  | NW   | 17        | 1N        | 205   | 0_0000   |       | P      | TL   | 12/31/1900 | ROCK CR     | V      |
| 43565 D        | 25117  |         | SW  | SE   | 11        | 1N        | 195   | 0.0000   |       | P      | IR   | 12/31/1903 | ROCK CR     | V      |
| 24943 0        | 24943  |         | 0 " |      | 0         | 0         | 0     | 0_0000   |       | P      | IR   | 12/31/1905 | ROCK CR     | V      |
| • (/303 D      | 25001  |         | SW  | SE   | 30        | 1 N       | 215   | 0_0000   |       | P      | T *  | 12/31/1905 | ROCK CR     | V      |
| 2/0/1          | 2/9/1  |         | 51  | 52   | 0         | 0         | CIE O | 0 2200   | CFS   | P      | IR   | 12/31/1004 | ROCK CP     | V      |
| 24741 0        | 25072  |         |     |      | 0         | 0         | 0     | 0 0000   |       | D      | CI   | 12/31/1004 | ROCK CR     | V      |
| • 25032 U      | 25616  |         |     |      | 0         | 0         | 0     | 0 0000   |       | P      | TI   | 12/31/1904 | ROCK CR     | V      |
| 20010 U        | 25056  |         |     |      | 0         | 0         | 0     | 0.0000   |       | P      | DS   | 12/31/1907 | ROCK CR     | V      |
| 25056 D        | 20000  |         |     |      | U         | 0         | 0     | 0_0000   |       | F      | 05   | 15/21/1901 | NUCK CR     | V      |

| • |  |                |   |         |          |          |   |   |  |  |  |                      |  |
|---|--|----------------|---|---------|----------|----------|---|---|--|--|--|----------------------|--|
| • | CERTIFICAT   | E              | PERMIT  | DLC LOT | 1/4      | 1/4      | SECTION   | TOWNSHIP  | RANGE  | RATE   | UNITS  | P.A.S.               | USE  |
| • | 25057<br>25058<br>25213<br>24946<br>43750<br>782<br>1402<br>2029<br>2830<br>3339<br>5325<br>6126 | 00000000000000 | 25057<br>25058<br>25213<br>24946<br>331<br>720<br>138<br>1826<br>1952<br>2057<br>5535<br>6408 |         |          |          | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.2000\\ 0.1600\\ 0.1250\\ 0.6250\\ 0.6250\\ 0.2000\\ 2.0000\\ 2.0000\\ 0.4400\\ 0.1800 \end{array}$ | CFS<br>CFS<br>CFS<br>CFS<br>CFS<br>CFS<br>CFS<br>CFS | Ρ Ρ Ρ Ρ Ρ Ρ Ρ Ρ<br>Ρ | DS<br>DS<br>DS<br>IR<br>IR<br>IR<br>IR<br>IR<br>IR<br>IR<br>IR<br>IR<br>IR |
| • | 12267<br>22203   | S<br>S         | 12379<br>20730  |         | NW<br>NE | NW<br>SE | 24<br>24  | 1S<br>1S  | 21E<br>21E   | 0-5000   | CFS<br>CFS   | P<br>C               | I R<br>I R   |

| 25058 | D | 25058 |   |      | 0  | 0  | 0     | 0.0000                                  |     | P | DS | 12/31/1907 | ROCK CR | V      |
|-------|---|-------|---|------|----|----|-------|---|-----|---|----|------------|---------|--------|
| 2/0/6 | D | 23213 |   |      | 0  | 0  | 0     | 0.0000                                  |     | P | US | 12/31/1907 | ROCK CR | V      |
| 13750 | 0 | 24940 |   |      | 0  | 0  | 0     | 0.2000                                  | CEC | P | IR | 12/31/1900 | ROCK CR | v      |
| 43730 | S | 331   |   |      | 0  | 0  | 0     | 0.1600                                  | CFS | P | IR | 6/22/1910  | RUCK CR | V      |
| 1/02  | 5 | 120   |   |      | 0  | 0  | 0     | 0-1250                                  | CFS | P | IR | 4/22/1911  | RUCK CR | V      |
| 1402  | E | 138   |   |      | 0  | 0  | 0     | 0.6250                                  | CFS | Р | IR | 5/18/1912  | RUCK CR | V      |
| 2029  | 5 | 1826  |   |      | 0  | 0  | 0     | 0 2000                                  | CFS | Р | IR | 11/1//1913 | RUCK CR | v<br>V |
| 2830  | 5 | 1952  |   |      | 0  | 0  | 0     | 2 0000                                  | CFS | Р | IR | 3/19/1914  | RUCK CR | V      |
| 3339  | S | 2057  |   |      | 0  | 0  | 0     | 2.0000                                  | CFS | Р | IR | 6/ 9/1914  | ROCK CR | V      |
| 5525  | S | 5535  |   |      | 0  | 0  | 0     | 0-4400                                  | CFS | Р | IR | 6/ 5/1922  | ROCK CR | V      |
| 6126  | S | 6408  |   |      | 0  | 0  | 0     | 0.1800                                  | CFS | Р | IR | 7/ 5/1924  | ROCK CR | V      |
| 12267 | S | 12379 | N | W NW | 24 | 15 | 21E   | 0.5000                                  | CFS | Р | IR | 9/22/1936  | ROCK CR | V      |
| 22203 | S | 20730 | N | E SE | 24 | 15 | 21E   | 0.8600                                  | CFS | С | IR | 9/11/1951  | ROCK CR | V      |
| 29965 | S | 21310 | S | E NE | 32 | 1N | 21E   | 1.5000                                  | CFS | Р | IR | 9/20/1951  | ROCK CR | V      |
| 21810 | S | 21305 | S | E SW | 3  | 15 | 21E   | 0.2300                                  | CFS | Р | IR | 4/15/1952  | ROCK CR | V      |
| 30166 | S | 22580 | N | E NE | 27 | 25 | 22E   | 2.0000                                  | CFS | Р | IR | 8/ 3/1953  | ROCK CR | V      |
| 30080 | S | 23576 | S | E NE | 25 | 15 | 21E   | 0.0100                                  | CFS | Р | LV | 3/ 7/1955  | A SPR   | V      |
| 30313 | S | 23963 | S | W SW | 11 | 55 | 25E   | 0.2500                                  | CFS | Р | IR | 3/ 5/1956  | ROCK CR | V      |
| 38437 | S | 31948 | N | W NW | 30 | 15 | 22E   | 2.0000                                  | CFS | Р | IR | 10/17/1966 | ROCK CR | V      |
| 38436 | R | 4860  |   |      | 30 | 15 | 22E - | 4.0000                                  | AFT | Ρ | FI | 12/ 5/1966 | A SPR   | V      |
| 38437 | S | 31948 | S | E NW | 30 | 15 | 22E   | 0.1000                                  | CFS | Р | FI | 1/12/1967  | A SPR   | V      |
| 37808 | S | 32337 | N | E SE | 14 | 15 | 21E   | 0.6000                                  | CFS | Р | IR | 2/ 9/1967  | ROCK CR | V      |
| 37916 | S | 32494 | S | E NE | 4  | 15 | 21E   | 0.4500                                  | CFS | Р | IR | 2/24/1967  | ROCK CR | V      |
| 42183 | S | 36278 | N | W SW | 11 | 15 | 21E   | 0.3800                                  | CFS | Ρ | IR | 6/10/1971  | ROCK CR | V      |
| 56572 | S | 38739 | S | E SW | 7  | 1N | 20E   | 0.5000                                  | CFS | Ρ | IR | 10/11/1973 | ROCK CR | V      |
| 54169 | S | 39469 | N | W SW | 11 | 15 | 21E   | 0.0800                                  | CFS | Р | IR | 6/ 2/1975  | ROCK CR | V      |
| 48134 | S | 39932 | N | W SW | 4  | 25 | 22E   | 1.6600                                  | CFS | Р | IR | 8/28/1975  | ROCK CR | V      |
| 0     | S | 39171 | S | E NE | 5  | 25 | 22E   | 1.8000                                  | CFS | Ρ | IR | 9/25/1975  | ROCK CR | V      |
| 47505 | S | 40362 | S | W SW | 33 | 1N | 21E   | 0.5100                                  | CFS | Р | IR | 11/ 5/1975 | ROCK CR | V      |
| 47602 | S | 40175 | N | W NE | 15 | 1N | 20E   | 0.0900                                  | CFS | Р | IR | 12/26/1975 | A SPR   | V      |
| 48653 | S | 40216 | N | W NW | 30 | 15 | 22E   | 0.1600                                  | CFS | Ρ | IR | 2/ 6/1976  | ROCK CR | V      |
| 48654 | S | 40217 | N | E SW | 3  | 15 | 21E   | 0.5700                                  | CFS | Ρ | IR | 2/ 6/1976  | ROCK CR | V      |
| 49027 | S | 40215 | S | E SW | 3  | 15 | 21E   | 0.5800                                  | CFS | P | IR | 2/ 6/1976  | ROCK CR | V      |
| 56641 | S | 40235 | N | W NE | 10 | 15 | 21E   | 0.0900                                  | CFS | Р | IR | 2/19/1976  | ROCK CR | V      |
| 47702 | S | 40468 | S | W SE | 11 | 1N | 19E   | 0.5500                                  | CFS | P | IR | 3/ 1/1976  | ROCK CR | V      |
| 0     | S | 40264 | N | W NW | 24 | 15 | 21E   | 0.5500                                  | CFS | Р | IR | 3/ 8/1976  | ROCK CR | V      |
| 56645 | S | 40844 | N | W SW | 11 | 15 | 21E   | 0.1200                                  | CFS | Р | IR | 6/28/1976  | ROCK CR | V      |
| 0     | S | 40864 | S | W NW | 32 | 15 | 22E   | 0.4200                                  | CFS | Р | IR | 7/ 8/1976  | ROCK CR | V      |
| 54170 | S | 41208 | N | W SW | 11 | 15 | 21E   | 0.9900                                  | CES | Р | IR | 12/ 1/1976 | ROCK CR | v      |
| 0     | S | 44677 | N | W NE | 14 | 15 | 21F   | 0.5700                                  | CES | Р | IR | 6/29/1979  | ROCK CR | V      |
|       |   |       |   |      |    |    |       | 0.2300                                  |     |   |    |            |         |        |
|       |   |       |   |      |    |    |       |   | CES |   |    |            |         |        |
|       |   |       |   |      |    |    |       | 26.0850                                 | AFT |   |    |            |         |        |
|       |   |       |   |      |    |    |       | 4.0000                                  |     |   |    |            |         |        |
| 25573 | D | 25573 |   |      | 0  | 25 | 22E   | 0.000                                   |     | Р | IR | 12/31/1902 | DRY CR  | V      |
|       |   |       |   |      |    |    |       | ======================================= |     |   |    |            |         |        |

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PRIORITY STREAM NAME STATUS

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12/31/1907 ROCK CR

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| Page   | 3   |   |         |                                  |                            |  |   |   |  |                          |   |  |   |   |  |
|--|---|---|---------|----------------------------------|----------------------------|--|---|---|--|--------------------------|---|--|---|---|--|
| • CERTI  | FICATE  | PERMIT  | DLC LOT | 1/4                              | 1/4                        | SECTION  | TOWNSH  | IP RANGE  | RATE   | UNITS                    | P.A.S                                     | USE  | PRIORITY  | STREAM NAME   | STATUS   |
| • 2<br>2<br>2  | 5618 D<br>4942 D<br>5917 D  | 25618<br>24942<br>25917   |         |                                  |                            | 0<br>0<br>0                                    | 0<br>0<br>0   | 0<br>0<br>0   | 0.0000<br>0.0000<br>0.0000   |                          | P<br>P<br>P                               | LV<br>IR<br>IR   | 12/31/1880<br>12/31/1890<br>12/31/1898  | S FK ROCK CR<br>S FK ROCK CR<br>S FK ROCK CR  | V<br>V<br>V                                    |
| • 2  | 5564 D  | 25564   |         |                                  |                            | 0  | 45  | 22E   | 0.0000   |                          | Ρ   | LV   | 12/31/1880  | SIXMILE CAN   | ٧  |
| • 2<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>2<br>5<br>2<br>2<br>3<br>4 | 5357 D<br>5358 D<br>5483 D<br>5483 D<br>5483 D<br>5483 D<br>7697 D<br>5617 D<br>7917 S<br>7803 S<br>0 S | 25357<br>25358<br>25483<br>25483<br>25483<br>25483<br>25682<br>25617<br>33691<br>36175<br>41464 |         | NE<br>SE<br>NW<br>NE<br>SW<br>NW | NW<br>SW<br>SW<br>NE<br>SW | 0<br>0<br>23<br>14<br>31<br>0<br>36<br>5<br>31 | 0<br>0<br>5 S<br>5 S<br>5 S<br>0<br>5 S<br>6 S<br>5 S | 0<br>0<br>23E<br>23E<br>24E<br>0<br>23E<br>24E<br>24E<br>24E<br>24E | 0 - 0000<br>0 - 0000<br>0 - 0000<br>0 - 0000<br>0 - 0000<br>0 - 0000<br>0 - 0000<br>1 - 3200<br>1 - 3800<br>0 - 7300 | CFS<br>CFS<br>CFS        | P<br>P<br>P<br>P<br>P<br>P<br>P<br>P<br>P | I*<br>I*<br>I*<br>I<br>I<br>I<br>I<br>I<br>R<br>I<br>R<br>I<br>R | 12/31/1880<br>12/31/1880<br>12/31/1887<br>12/31/1887<br>12/31/1887<br>12/31/1887<br>12/31/1897<br>12/31/1897<br>12/31/1907<br>6/17/1968<br>4/21/1971<br>1/31/1977 | LONE ROCK CR<br>LONE ROCK CR<br>LONE ROCK CR<br>SPRINGS<br>LONE ROCK CR<br>LONE ROCK CR<br>LONE ROCK CR<br>LONE ROCK CR<br>LONE ROCK CR | V<br>V<br>V<br>V<br>V<br>V<br>V<br>V<br>V<br>V |
| •  |   |   |         |                                  |                            |  |   |   | 3.4300   | ) CFS                    |   |  |   |   |  |
| • 2  | 5476 D  | 25476   | 2       |                                  |                            | 6  | 65  | 24E   | 0.0000   |                          | Ρ   | MU   | 9/ 5/1908   | 2 SPRINGS   | ٧  |
| • 2<br>6   | 1648 S<br>3477 R  | 17353<br>9997   |         | NW<br>SE                         | NW<br>NW                   | 9<br>6   | 6S<br>7S  | 24E<br>25E  | 0.3000<br>3.3000<br>========<br>3.6000   | CFS<br>CFS<br>) CFS      | P<br>P                                    | IR<br>LV   | 10/ 7/1946<br>8/30/1982   | BROWN CR<br>UNN STR   | V<br>V   |
| • 22   | 4972 D<br>4973 D  | 24972<br>24973  |         |                                  |                            | 10<br>10                                       | 65<br>65  | 24E<br>24E  | 0.0000   |                          | P<br>P                                    | IR<br>IR   | 12/31/1884<br>12/31/1884  | BIG DUTCH CAN<br>BIG DUTCH CR   | V<br>V   |
| • 6<br>6   | 1214 R<br>3945 S  | 9046<br>49154   |         | N W<br>N W                       | SW<br>NW                   | 27<br>27                                       | 65<br>65  | 24E<br>24E  | 0.0190<br>0.0030<br>=======<br>0.0030<br>0.0190  | AFT<br>CFS<br>CFS<br>AFT | P<br>P                                    | L V<br>L V   | 8/25/1983<br>8/25/1983  | UNN STR<br>PERRY SPR  | V<br>V   |
| •  | 0 R<br>0 R  | 10161<br>10161  | 1<br>1  | NW<br>NW                         | NW<br>NW                   | 35<br>35                                       | 65<br>65  | 24E<br>24E  | 0 <u>1760</u><br>0 <u>3000</u>   | AFT<br>AFT               | P<br>P                                    | L W<br>L W   | 12/ 7/1983<br>12/ 7/1983  | UNN STR/OLD HO<br>UNN STR/THUNDE  | SS RES V<br>RHD RS V                           |

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|-------|---|--|---------|----------------------------|----------------------------|------------------------|----------------------------|---------------------------------|---|---|------------------|----------------------|--|---|------------------------|--|
| •     | CERTIFICATE                                 | PERMIT                                 | DLC LOT | 1/4                        | 1/4                        | SECTION                | TOWNSHIP                   | RANGE                           | RATE  | UNITS   | P.A.S.           | USE                  | PRIORITY   | STREAM NAME   | STATUS                 |  |
| •     | 0 R<br>0 R<br>0 R<br>0 R                    | 10161<br>10162<br>10163<br>10164       |         | SE<br>SE<br>SW<br>SW       | NW<br>SW<br>SE<br>SE       | 35<br>26<br>26<br>27   | 65<br>65<br>65<br>65       | 24E<br>24E<br>24E<br>24E<br>24E | 0.1620<br>0.0510<br>0.0270<br>0.0740<br>=================================== | AFT<br>AFT<br>AFT<br>AFT<br>0 AFT                 | P<br>P<br>P      |                      | 12/ 7/1983<br>12/ 7/1983<br>12/ 7/1983<br>12/ 7/1983<br>12/ 7/1983 | UNN STR/BRANDEN<br>UNN STR<br>UNN STR<br>UNN STR            | BRG R V<br>V<br>V<br>V |  |
| • • • | 63464 R<br>0 R<br>0 R<br>61210 R<br>61211 R | 9984<br>10105<br>10107<br>9042<br>9043 |         | NW<br>NE<br>NE<br>SE<br>NE | SW<br>NW<br>SW<br>SE<br>NW | 1<br>2<br>6<br>35<br>7 | 7S<br>7S<br>7S<br>6S<br>7S | 24E<br>24E<br>25E<br>24E<br>25E | 0.3600<br>0.0950<br>0.0420<br>0.1080<br>0.0810<br>======<br>0.360<br>0.326  | CFS<br>AFT<br>AFT<br>AFT<br>AFT<br>0 CFS<br>0 AFT | P<br>P<br>P<br>P | LV<br>LW<br>LV<br>LV | 8/30/1982<br>9/30/1982<br>9/30/1982<br>8/25/1983<br>8/25/1983      | UNN STR<br>UNN STR<br>UNN STR<br>CRAWFORD CR<br>CRAWFORD CR | V<br>V<br>V<br>V<br>V  |  |
| •     | 61212 R<br>61213 R                          | 9044<br>9045                           |         | NW<br>NE                   | SW<br>NW                   | 12<br>11               | 7S<br>7S                   | 24E<br>24E                      | 0.0570<br>0.0450<br>=====<br>0.102  | AFT<br>AFT<br>0 AFT                               | P<br>P           | LV<br>LW             | 8/25/1983<br>8/25/1983   | UNN STR<br>UNN STR  | V<br>V                 |  |
| •     | 25357 D<br>25358 D<br>25683 D<br>25683 D    | 25357<br>25358<br>25683<br>25683       |         | SW<br>NW<br>NW             | SW<br>SE<br>NW             | 5<br>8<br>14<br>24     | 65<br>65<br>65<br>65       | 24E<br>24E<br>23E<br>23E        | 0.0000<br>0.0000<br>0.0000<br>0.0000  |   | P<br>P<br>P<br>P | I*<br>I*<br>DS<br>DS | 12/31/1880<br>12/31/1880<br>12/31/1886<br>12/31/1886               | A SPR<br>A SPR<br>A SPR<br>A SPR                            | V<br>V<br>V<br>V       |  |
| •     | 0 R<br>0 R<br>0 R<br>0 R                    | 10118<br>10160<br>10160<br>10119       |         | NW<br>SW<br>NE<br>NW       | NE<br>SW<br>SW<br>SE       | 33<br>27<br>28<br>28   | 65<br>65<br>65<br>65       | 24E<br>24E<br>24E<br>24E<br>24E | 0.0200<br>0.0180<br>0.0590<br>0.0140<br>=========<br>0.111                  | AFT<br>AFT<br>AFT<br>AFT<br>0 AFT                 | P<br>P<br>P<br>P | LW<br>LW<br>LW<br>LW | 9/30/1982<br>12/ 7/1983<br>12/ 7/1983<br>12/19/1983                | UNN STR<br>UNN STR/ROCKY R<br>UNN STR/SEDGE R<br>UNN STR    | ES V<br>ES V<br>V      |  |
| •     | 61222 R<br>61222 R                          | 9055<br>9055                           |         | NW<br>SE                   | SW<br>NE                   | 4<br>8                 | 7S<br>7S                   | 24E<br>24E                      | 0.3380<br>0.0360<br>=========<br>0.374                                      | AFT<br>AFT<br>0 AFT                               | P<br>P           | L V<br>L V           | 8/25/1983<br>8/25/1983   | UNN STR/YELLOW<br>UNN STR/TOWER P                           | J RES V<br>OND R V     |  |
| •     | 0 R   | 10103                                  |         | NE                         | NE                         | 8                      | 75                         | 24E                             | 0.0180<br>===================================                               | AFT<br>0 AFT                                      | Ρ                | LW                   | 9/30/1982  | UNN STR   | V                      |  |

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Page 5

| • | CERTIFICAT     | E<br>- | PERMIT         | DLC LOT | 1/4        | 1/4      | SECTION  | TOWNSHIP   | RANGE      |       | RATE   | UNITS                    | P.A.S. | USE        | PRIORITY                | STREAM NAME STA                             | TUS        |
|---|----------------|--------|----------------|---------|------------|----------|----------|------------|------------|-------|--|--------------------------|--------|------------|-------------------------|---|------------|
| • | 0<br>0         | RR     | 9057<br>9057   |         | S W<br>N E | NW<br>NW | 10<br>9  | 75<br>75   | 24E<br>24E | ====  | 0.0070<br>0.0150<br>=====<br>0.0220            | AFT<br>AFT               | P<br>P | L V<br>L V | 8/25/1983<br>8/25/1983  | UNN STR/UP STAHL RS<br>UNN STR/W STAHL P RS | V<br>5 V   |
| • | 0<br>0         | RR     | 9056<br>9056   |         | SW<br>SE   | SW<br>NE | 3<br>4   | 75<br>75   | 24E<br>24E | ====  | 0.0320<br>0.0220<br>======<br>0.0540           | AFT<br>AFT<br>AFT        | P<br>P | L V<br>L V | 8/25/1983<br>8/25/1983  | UNN STR/E STAHL PON<br>UNN.STR/LWR STAHL R  | ) V<br>5 V |
| • | 0<br>0         | R<br>R | 10104<br>10127 |         | NE<br>SW   | NW<br>NW | 11<br>11 | 75<br>75   | 23E<br>23E |       | 0.0270<br>0.0080<br>======<br>0.0350           | AFT<br>AFT<br>AFT        | P<br>P | LW<br>LW   | 9/30/1982<br>9/30/1982  | UNN STR<br>UNN STR                          | V<br>V     |
| • | 38984          | S      | 33692          |         | SE         | NW       | 16       | 65         | 25E        |       | 3.6800<br>======<br>3.6800                     | CFS<br>CFS               | Ρ      | IR         | 6/17/1968               | E FK JUNIPER CR                             | ٧          |
| • | 38723<br>38723 | R<br>R | 4645<br>4645   |         | N W<br>N W | SW<br>SW | 31<br>31 | 5 S<br>5 S | 25E<br>25E |       | 0.0600<br>0.1200<br>======<br>0.1800           | AFT<br>AFT<br>AFT        | P<br>P | L V<br>L V | 8/26/1965<br>10/26/1965 | LONG HOL<br>LONG HOL                        | V<br>V     |
| • | 0<br>63379     | R<br>R | 6209<br>9605   |         | N E<br>N W | NW<br>SE | 19<br>12 | 65<br>65   | 26E<br>26E | ====  | 3.5000<br>0.2400<br>======<br>0.2400<br>3.5000 | AFT<br>CFS<br>CFS<br>AFT | P<br>P | L V<br>L W | 8/29/1973<br>10/11/1982 | UNN STR<br>UNN STR                          | V<br>V     |
| • | 24850<br>61303 | D<br>R | 24850<br>9365  |         | SW         | NW       | 0<br>31  | 0<br>5 S   | 0<br>27E   | ====; | 0.0000<br>0.0320<br>=====<br>0.0320            | AFT<br>AFT               | P<br>P | IR<br>LV   | 12/31/1890<br>6/18/1982 | TUPPER CR<br>TUPPER CR                      | V<br>V     |
| • | 0              | R      | 9090           |         | SW         | SW       | 29       | 55         | 27E        | ====; | 0.0445<br>======<br>0.0445                     | AFT<br>AFT               | Ρ      | LW         | 1/17/1983               | UNN STR                                     | ٧          |
| • | 61206          | R      | 9038           |         | SE         | NE       | 14       | 65         | 26E        |       | 0.0150   | AFT                      | Ρ      | LV         | 8/25/1983               | WESLER CAN                                  | ٧          |
| •                   |            |
|---------------------|------------|
| Page 6              |            |
| rage 0 =====        |            |
|                     | 0.0150 AFT |
| TOTALS              | •          |
| TOTAL CFS: 37-3980  |            |
|                     |            |
| • TOTAL AFT: 9.6225 | •          |
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| •                   | C          |
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70251



Water Availability Analysis Rock Cr. at Mouth

20251

# Water Availability Rock Cr. at Mouth



WATER AVAILABILITY TABULATION NATURAL Flow

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| Rock Cr. | Rock Cr. at Mouth 50 |       |       |       |       |  |  |  |  |  |
|----------|----------------------|-------|-------|-------|-------|--|--|--|--|--|
| Months   | Pred59               | Pred2 | Inswr | WA5   | WA2   |  |  |  |  |  |
| JAN      | 40.1                 | 122.6 | 0.0   | 40.1  | 122.6 |  |  |  |  |  |
| FEB      | 71.9                 | 250.2 | 0.0   | 71.9  | 250.2 |  |  |  |  |  |
| MAR      | 118.9                | 373.0 | 0.0   | 118.9 | 373.0 |  |  |  |  |  |
| APR      | 96.7                 | 235.5 | 0.0   | 96.7  | 235.5 |  |  |  |  |  |
| MAY      | 57.1                 | 88.1  | 0.0   | 57.1  | 88.1  |  |  |  |  |  |
| JUN      | 18.4                 | 33.6  | 0.0   | 18.4  | 33.6  |  |  |  |  |  |
| JUL      | 3.6                  | 8.1   | 0.0   | 3.6   | 8.1   |  |  |  |  |  |
| AUG      | 1.0                  | 3.1   | 0.0   | 1.0   | 3.1   |  |  |  |  |  |
| SEP      | 1.4                  | 3.4   | 0.0   | 1.4   | 3.4   |  |  |  |  |  |
| OCT      | 2.0                  | 4.8   | 0.0   | 2.0   | 4.8   |  |  |  |  |  |
| NOV      | 6.3                  | 14.5  | 0.0   | 6.3   | 14.5  |  |  |  |  |  |
| DEC      | 16.8                 | 42.5  | 0.0   | 16.8  | 42.5  |  |  |  |  |  |
|          |                      |       |       |       |       |  |  |  |  |  |

- 6.0 = Basin No.522.0 = Drainage Area
- 16.0 = Precipitation
- 0.0 = WR Index

### DEAN MONTHLY FLOWS FOR ROCK CREEK, TRIB JOHN DAY RIVER BASED ON BEAVER CREEK NEAR PAULINA, GAGE 14-0780

|     | MEAN    | a       | A      | S     | St   | E      |  |
|-----|---------|---------|--------|-------|------|--------|--|
|     |         |         | 522.00 | 57.90 | 1.42 | 4.60   |  |
| OCT | 94.47   | .00134  | 93.98  | 1.00  | .61  | 1.00   |  |
| VOV | 52.81   | .00303  | 214.67 | 1.00  | .85  | 1.00   |  |
| DEC | 135.64  | .00328  | 241.77 | 1.00  | .90  | 1.00   |  |
| JAN | 127.54  | .11     | 306.67 | 1.00  | 1.00 | 1.00   |  |
| FEB | 205.71  | .928    | 345.39 | 1.00  | 1.00 | 1.00   |  |
| MAR | 302.56  | 4.26    | 188.23 | 1.00  | 1.00 | .06    |  |
| APR | 816.51  | .0202   | 351.93 | 1.00  | .84  | 1.00   |  |
| MAY | 681.61  | .0195   | 472.27 | 2.99  | .88  | 1.00   |  |
| JUN | 1027.88 | 2.82e-8 | 408.96 | 1.00  | .77  | 137.84 |  |
| JUL | 196.37  | .00541  | 61.03  | 1.00  | .77  | 1.00   |  |
| AUG | 93.70   | .00129  | 67.03  | 1.00  | .60  | 1.00   |  |
| SEP | 84.73   | .000965 | 88.28  | 1.00  | .57  | 1.00   |  |
|     |         |         |        |       |      |        |  |





# BASIN SUMMARY REPORT

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ROCK CR TRIBUTARY OF JOHN DAY R

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| • SOURCE > TRIBUTARY       | TOTAL DIVERTED        | AGRIC.                       | INDUST.      | MUNIC.             | DOMEST.      | RECREAT.           | MISC.              | UNKNOWN |
|----------------------------|-----------------------|------------------------------|--------------|--------------------|--------------|--------------------|--------------------|---------|
| • ROCK CR > JOHN DAY R     | 26.08 CFS<br>4.00 ACF | 25.99                        | 0.00         | 0.00               | 0.00<br>0.00 | 0.00<br>0.00       | 0.104.00           | 48      |
| • DRY CR > ROCK CR         | 0.00 CFS<br>0.00 ACF  | 0 = 0 0<br>0 = 0 0           | 0.00         | 0.00               | 0.00         | 0.00               | 0.00               | 1       |
| S FK ROCK CR > ROCK CR     | 0.00 CFS<br>0.00 ACF  | 0.00                         | 0.00         | 0.00               | 0.00         | 0.00               | 0.00               | 3       |
| • SIXMILE CAN > ROCK CR    | 0.00 CFS<br>0.00 ACF  | 0.00                         | 0.00         | 0.00               | 0.00         | 0.00               | 0 = 0 0<br>0 = 0 0 | 1       |
| • LONE ROCK CR > ROCK CR   | 3.43 CFS<br>0.00 ACF  | 3.43<br>0.00                 | 0.00         | 0.00               | 0.00         | 0.00               | 0.00               | 7       |
| JOHNSON CR > LONE ROCK CR  | 0.00 CFS<br>0.00 ACF  | 0 = 00<br>0 = 00             | 0.00         | 0.00               | 0.00         | 0.00               | 0.00               | 1       |
| BROWN CR > LONE ROCK CR    | 3.60 CFS<br>0.00 ACF  | 3 - 60<br>0 - 00             | 0.00<br>0.00 | 0.00               | 0.00         | 0.00               | 0.00               | 0       |
| BIG DUTCH CAN > BROWN CR   | 0.00 CFS<br>0.00 ACF  | 0 = 00<br>0 = 00             | 0.00         | 0.00               | 0_00<br>0_00 | 0.00               | 0.00               | 2       |
| • UNN STR > BROWN CR       | 0.00 CFS<br>0.02 ACF  | 0.00<br>0.02                 | 0.00         | 0.00               | 0.00<br>0.00 | 0.00               | 0.00               | 0       |
| DRY FK > BROWN CR          | 0.00 CFS<br>0.79 ACF  | 0 <u>0</u> 00<br>0 <u>79</u> | 0.00<br>0.00 | 0.00               | 0.00         | 0 _ 0 0<br>0 _ 0 0 | 0 = 0 0<br>0 = 0 0 | 0       |
| • CRAWFORD CR > BROWN CR   | 0.36 CFS<br>0.33 ACF  | 0 36<br>0 33                 | 0.00         | 0.00               | 0.00<br>0.00 | 0.00               | 0.00               | 0       |
| • UNN STR > CRAWFORD CR    | 0.00 CFS<br>0.10 ACF  | 0.00<br>0.10                 | 0.00         | 0.00               | 0.00         | 0.00               | 0.00               | 0       |
| BUCKHORN CR > LONE ROCK CR | 0.00 CFS<br>0.00 ACF  | 0.00                         | 0.00         | 0 = 0 0<br>0 = 0 0 | 0.00         | 0.00               | 0.00               | 4       |
| • STAHL CAN > BUCKHORN CR  | 0.00 CFS<br>0.11 ACF  | 0.00<br>0.11                 | 0.00         | 0.00               | 0.00         | 0.00               | 0.00               | 0       |
| • UNN STR > WINELAND CAN   | 0.00 CFS<br>0.37 ACF  | 0.00<br>0.37                 | 0.00         | 0 = 0 0<br>0 = 0 0 | 0.00         | 0.00               | 0.00               | 0       |
| • UNN STR > WINELAND CAN   | 0.00 CFS<br>0.02 ACF  | 0.00                         | 0.00         | 0 = 0 0<br>0 = 0 0 | 0.00         | 0.00               | 0.00               | 0       |
| UNN STR > STAHL CAN        | 0.00 CFS<br>0.02 ACF  | 0.00                         | 0.00         | 0.00               | 0.00         | 0.00               | 0.00               | 0       |

## BASIN SUMMARY REPORT

| Page 2                       | ROCK CR TRIBUTARY OF | JOHN DAY                         | R            |        |                    |                    |       |         |
|------------------------------|----------------------|----------------------------------|--------------|--------|--------------------|--------------------|-------|---------|
| SOURCE > TRIBUTARY           | TOTAL DIVERTED       | AGRIC.                           | INDUST.      | MUNIC. | DOMEST.            | RECREAT.           | MISC. | UNKNOWN |
| UNN STR > STAHL CAN          | 0.00 CFS<br>0.05 ACF | 0.00                             | 0.00<br>0.00 | 0.00   | 0.00               | 0.00               | 0.00  | 0       |
| UNN STR > BUCKHORN CR        | 0.00 CFS<br>0.04 ACF | 0.00<br>0.04                     | 0.00         | 0.00   | 0.00               | 0.00<br>0.00       | 0.00  | 0       |
| E FK JUNIPER CR > JUNIPER CR | 3.68 CFS<br>0.00 ACF | 3.68                             | 0.00         | 0.00   | 0.00               | 0.00               | 0.00  | 0       |
| LONG HOL > M FK ROCK CR      | 0.00 CFS<br>0.18 ACF | 0.00<br>0.18                     | 0.00         | 0.00   | 0.00               | 0.00<br>0.00       | 0.00  | 0       |
| INDIAN CR > CHAPIN CR        | 0.24 CFS<br>3.50 ACF | 0.24<br>3.50                     | 0.00         | 0.00   | 0.00               | 0.00               | 0.00  | 0       |
| TUPPER CR > ROCK CR          | 0.00 CFS<br>0.03 ACF | 0.00<br>0.03                     | 0.00         | 0.00   | 0 _ 0 0<br>0 _ 0 0 | 0.00               | 0.00  | 1       |
| HOLLYWOOD CR > TUPPER CR     | 0.00 CFS<br>0.04 ACF | 0 <u>0</u> 0 0<br>0 <u>0</u> 0 4 | 0.00         | 0.00   | 0.00               | 0 = 0 0<br>0 = 0 0 | 0.00  | 0       |
| WESLER CAN > ROCK CR         | 0.00 CFS<br>0.01 ACF | 0.00                             | 0.00         | 0.00   | 0.00               | 0.00               | 0.00  | 0       |

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BASIN SUMMARY REPORT ROCK CR TRIBUTARY OF JOHN DAY R # 2025/

TOTAL DIVERTED

TOTAL CFS: 37.40 TOTAL ACF: 9.62

Page 3

37.40

TOTALS BY USE

| •     | AGRICULTURE | INDUSTRIAL | MUNICIPAL | DOMESTIC | RECREATIONAL | MISCELLANEOUS |
|-------|-------------|------------|-----------|----------|--------------|---------------|
| (CFS) | 37.30       | 0.00       | 0.00      | 0.00     | 0.00         | 0.10          |
| (ACF) | 5.62        | 0.00       | 0.00      | 0.00     | 0.00         | 4.00          |

|          |               |            |            |            |            |                |              |             |          | 70         | 251        |        |
|----------|---------------|------------|------------|------------|------------|----------------|--------------|-------------|----------|------------|------------|--------|
| Report   | for station   | 14047200   |            |            |            |                | · · ·        |             |          | l          |            |        |
| ROCK CR  | REEK AB WHYTH | E PARK NE  | CONDON, OR | EG.        |            |                |              |             |          |            |            |        |
| GMEAN DI | SCHARGE       |            |            |            |            |                |              |             | 0        |            | ł          |        |
| 0Number  | of years ret  | trieved is | 5 16       |            |            | UTT DARK N     | R CONDAN     | 5           | 1 40.0   |            | read       |        |
| 9        | STAT<br>MFAI  | LION 1404  | 1/390      | ROCK C     | REEK AB WH | YIE PART I     | CONDON, O    | REG. K      | p. v in  | las to cu  |            |        |
|          | Star          | tistics or | n Normal m | onthiv mea | ng (Ail da | YE)            |              | 1           | 9758 000 | ,975 000   |            |        |
|          |               |            |            |            |            |                |              | 0           | ~ ~ ~ ~  | 1          |            |        |
|          | Oct           | Nov        | Dec        | Jan        | Feb        | March          | April        | May         | June     | July       | Aug        | Sept   |
|          | By rows (Nu   | umber, Mea | an. Varian | ce. Standa | rd Deviati | on, Skewne     | ss, Coeffi   | clent of Va | riation. | Percentage | of Average | Value) |
| ØNumber  | 14.00         | 14.00      | 14.20      | 14.20      | 14.00      | 14.00          | 14.00        | 14.00       | 14.00    | 14.00      | 14.00      | 14.00  |
| OMean    | 5.39          | 14.88      | 45.06      | 71.37      | 154.23     | 212.79         | 132.24       | 62.34       | 17.79    | 4.10       | 2.40       | 2.81   |
| OVar     | 19.07         | 176.11     | 2238.22    | 2563.35    | 15526.32   | 21791.44       | 10665.82     | 5714.94     | 451.96   | 14.24      | 4.79       | 6.62   |
| OStd     | 4.37          | 13.27      | 47.31      | 50.63      | 124.60     | 147.62         | 103.28       | 75.60       | 21.26    | 3.77       | 2.19       | 2.57   |
| USKew    | 0.75          | 2.14       | 2.27       | 0.22       | 1.09       | 6.34           | 1.49         | 2.70        | 2.68     | 1.74       | 1.06       | 1.56   |
| OCVAL    | 0.81          | 0.89       | 1.05       | 0.71       | 6.81       | 20 33          | 6.78         | 1.21        | 1.19     | 0.32       | 0.31       | 0.31   |
| 1        | Sta           | z.05       | 47.390     | POCK C     | REEK AR WH | YTE PARK N     | E CONDON O   | 8.59<br>RFG | 2.45     | 0.57       | 0.00       | 0.09   |
| 0        | MEAL          | N DISCHARO | GE         | NOON C     | KEEK ND HI | 112 11111 1    | e compon, or | MLC.        |          |            |            |        |
|          | Quar          | rtiles of  | Normal mos | nthly mean | s (All day | 2)             |              |             |          |            |            |        |
|          |               | C+         |            |            |            |                |              |             |          | -          |            |        |
| G        |               | OCT        |            | NOA        |            | Dec<br>Twenty- | Fifth Perce  | Jan         |          | reb        | E.         | arcn   |
|          |               | 2.18       |            | 6.25       |            | 15.4           | 1100 10100   | 29.7        |          | 58.4       |            | 73.8   |
| 0        |               |            |            |            |            | Fifti          | eth Percent  | tile        |          |            |            |        |
|          |               | 3.43       |            | 10.8       |            | 27.2           |              | 55.8        | 1        | 124.6      | 2.         | 20.9   |
| 9        |               | 9 61       |            | 21 3       |            | Seventy        | -Fifth Perc  | centile     |          | 220 0      | 3          | 25 3   |
|          |               | 5.01       |            | 21.0       |            | 5:.5           |              | 120.2       | -        | 200.0      | 0.         | 20.0   |
|          |               |            |            |            |            |                |              |             |          |            |            |        |
|          |               |            |            |            |            |                |              |             |          |            |            |        |
|          |               |            |            |            |            |                |              |             |          |            |            |        |
|          | A             | oril       |            | May        |            | June           |              | July        |          | Aug        | :          | Sept   |
| 0        |               |            |            |            |            | Twenty-        | Fifth Perce  | entile      |          |            |            |        |
|          | -             | 55.8       |            | 24.5       |            | 6.41           |              | 1.51        |          | .683       |            | 1.81   |
| 9        | 1 7           |            |            | 20.0       |            | Fifti          | eth Percent  | tile        |          | 1 10       |            |        |
| 9        | 13            | 12.0       |            | 30.9       |            | 11.9           | Rifth Dar    | 3.32        |          | 1.58       |            | 2.92   |
|          | 16            | 59.4       |            | 65.1       |            | 16.9           | -Filon Fer   | 4.75        |          | 4.13       |            | 4 77   |
| 1        | Stat          | tion 1404  | 17390      | ROCK CI    | REEK AB WH | YTE PARK NI    | R CONDON, OI | REG.        |          |            |            |        |
| 0        | MEAN          | DISCHARC   | GE         |            |            | mick m         |              |             |          |            |            |        |
|          | Quar          | ctiles of  | Normal and | nual means | (All days  | )              |              |             |          |            |            |        |
| 0        | T             | nto Dift   | Demantit   | 10         |            |                |              |             |          |            |            |        |
| 9        | 1 % 6         | 20 g       | Fercentl   | Le         |            |                |              |             |          |            |            |        |
| 9        | Fi            | Litieth Pe | ercentile  |            |            |                |              |             | 4        |            |            |        |
|          |               | 55.3       |            |            |            |                | 1A, 10as     | 0           | 59-      |            |            |        |
| 0        | Seve          | enty-Fifth | Percentil  | e          |            |                | 144          | gunnel      | -        |            |            |        |
|          |               | 73.6       |            |            |            |                | ave          |             |          |            |            |        |
|          |               |            |            |            |            |                |              |             |          |            |            |        |

NOTE -- PERCENTILES BASED ON AVAILABLE DATA.

| DATE                 | LOCATION   | GAGE-HEIGHT | DISCHARGE<br>SECOND-FEET |
|----------------------|--|-------------|--------------------------|
| Mar. 10, 1966        | SE4SW4 sec.15, T.2 S., R.22 E.,                        |             | 153                      |
| Oct. 25, 1966        | above bridge<br>Sec.36, T.3 S., R. 22 E., ab bridge    |             |                          |
| Oct 01 7011          | Hwy 206  |             | 3.47                     |
| 000. 20, 1966        | Sec.6, T.4 S., R.23 E., at Murtah<br>Ranch             |             | 0.67                     |
| Dec. 6, 1966         | Sec.26, T.2 S., R.22 E., bl Dry Cr.                    |             | 51.6                     |
| do                   | Sec.15, T.2 S., R.22 E., 9/10 mile                     |             | 50.7                     |
| Dec. 3, 1970         | $SE_{\mu}^{1}SW_{\mu}^{1}$ sec.15, T.2 S., R.22 E.     |             | 14.6                     |
| Dec. 3, 1970         | $NE_{14}^{1}$ sec.10, T.1 S., R.21 E.                  |             | 13.1                     |
| Mar.25, 1971         | NWINEI sec.10, T.1 S.,R.21 E.                          |             | 284                      |
| Mar 26, 1971         | NWTNET sec.13, T.1 N., R.19 E.                         |             | 277                      |
| Mar.26, 1971         | $SE_{1}^{L}SW_{1}^{L}$ sec.15, T.1 N., R.20 E.         |             | 245                      |
| May 25, 1971         | $SE_{4}^{I}SW_{4}^{I}$ sec.15, T.2 S., R.22 E.         |             | 9.34                     |
| do                   | $NW_{4}^{\perp}NE_{4}^{\perp}$ sec.10, T.1 S., R.21 E. |             | 9.28                     |
| Oct. 28, 1975        | NW4NE4 sec.10, T.1 S., R.21 E. at                      |             | 0.52                     |
| Nov. 25, 1975        | Hwy brdg at Olex                                       |             | 0.84                     |
|                      | 1 tran   |             |                          |
| STATE PRINTING 50716 |  | _           |                          |
|                      | bace   |             |                          |

|   | LOCATION   | GAGE-HEIGHT | DISCHARGE<br>SECOND-FEET   |
|---|--|-------------|--|
| June 6, 1976<br>June 22, 1976<br>Aug. 24, 1976  | do<br>do<br>do   |             | 0.77<br>0.77<br>2.21   |
| Aug. 24, 1976<br>Oct.28, 1975<br>Dec. 23, 1976<br>Jan. 27, 1976<br>Feb. 25, 1976<br>Mar. 23, 1976<br>May 6, 1976<br>May 24, 1976<br>June 9, 1976<br>June 22, 1976<br>July 27, 1976<br>Aug. 24, 1976 | SW4NE4 sec.24, T.1 N., R.20 E., 6<br>mi nw of Olex<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do |             | 0.38<br>0.30<br>0.51<br>38.0<br>31.5<br>107<br>20.8<br>0.20<br>2.0<br>1.19<br>0.51<br>0.43 |
| SP*23940-119  | 1  | 1           |  |

| HISCELLANEOUS ST  | TRIBUTARY TO OR DIVERTING FROM      |             | COUNTY                   |
|-------------------|-------------------------------------|-------------|--------------------------|
| MEASUREMENT NO. D | D4 17070201                         |             |                          |
|                   | John Day River                      | Grant       | Co                       |
| Rock Creek        | LOGATION                            | GAGE-HEIGHT | DISCHARGE<br>SECOND-FEET |
| DATE              |                                     |             | -                        |
| a 1 77 7010       | Mouth, 6 mi northwest of Dayville   |             | 0                        |
| Sept. 1/, 1949    | Mouth                               |             | 0.8 Est                  |
| Aug. 31, 1951     | Mouth in Et sec. 18. T.12 S., R.26  |             | 0.36                     |
| Aug. 23, 1951     | Moutin, In 12 booties, and          |             | 0.83                     |
| Aug.4, 1952       | do                                  |             | 20.4                     |
| Auly 15, 1953     |                                     |             | 2.15                     |
| Sept. 8, 1953     | do                                  |             | * 1.5 Est                |
| July 27, 1955     |                                     |             |                          |
|                   | Drainage area, 292                  |             | 1 0 03                   |
| Sent. 18, 1956    | 0.5 mi abo mouth                    |             | * 9.00                   |
| July 16 1057      | At mouth                            |             | 10.0                     |
| July 10, 1991     | do                                  |             | 3.30                     |
| Aug. 10, 1959     |                                     |             | 2.19                     |
| Aug. 12, 1960     | NE4 sec.21, T.12 S., R.25 E.        | mi          |                          |
| July 18, 1961     | NEt sec. 18, T.12 S., R.20 E., 0.9  | all >       | 7 07                     |
|                   | horthwest of Dayville(292 sq mi Dr. | Ar.)        | 1.01                     |
| 1110 24 1962      |                                     |             | 1.05                     |
| Tul 70 1067       |                                     |             | 7.22                     |
| July 30, 1903     |                                     |             | 38.0                     |
| Jan. 6, 1964      |                                     |             | 32 6                     |
| Feb. 11. 1964     |                                     |             | 12.0                     |

| 0.17<br>0.56<br>0.56<br>0.56<br>0.55<br>32.8<br>0.55<br>38.0<br>32.8<br>0.55<br>38.0<br>38.0<br>38.0<br>55<br>38.0<br>55<br>38.0<br>55<br>38.0<br>55<br>38.0<br>55<br>38.0<br>55<br>55<br>38.0<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55 | GAGE-HEIGHT | Ĵŝ | ) E* | R.20  | ••N  | 0p<br>0p<br>0p<br>0p<br>0p<br>0p | ° <u>c</u> | ec.le        | ላን ይኒ.<br>ለጉ ይኒ. | 서H<br>V <sup>9</sup> EMS | 926<br>926<br>926<br>926<br>926<br>926<br>926<br>926<br>926<br>926 | L 'L'<br>L 'Z'<br>L 'Z'<br>Sol '<br>Sol '<br>'<br>Sol '<br>'<br>Sol '<br>'<br>'<br>Sol '<br>'<br>Sol '<br>'<br>'<br>'<br>Sol '<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>'<br>' | 2226 | to0<br>νοΝ<br>πεύ<br>γελ<br>γελ<br>γελ<br>γεν<br>γεν<br>γεν<br>γεν<br>γεν<br>γεν<br>γεν<br>γεν<br>γεν<br>γεν |
|--|-------------|----|------|-------|------|----------------------------------|------------|--------------|------------------|--------------------------|--|---|------|--|
| тииоэ<br>ШБГГГРД   | E           | 25 | ЕВОМ | 1 Ver | A KE |                                  |            | іят<br> <br> | h                | C wya                    | ars ) &  | Cree  | K I  | BOC  |
|  | 1-          |    |      |       |      |                                  |            |              |                  |                          |  |   |      |  |

| MISCELLANEOUS<br>MEASUREMENT No. BO<br>Rock Creek  | EAM DY 17070 204 JOHN DAY RIVER  | 3 <sup>3</sup> |  |
|--|--|----------------|--|
| NOCK OF CCK  |  | GAGE-HEIGHT    | DISCHARGE  |
| DATE   | LOCATION   | FEET           | SECOND-FEET  |
| Dec. 23, 1975<br>Jan. 27, 1976<br>Feb. 25, 1976<br>Mar. 23, 1976<br>May 6, 1976<br>May 26, 1976<br>June 7, 1976<br>June 22, 1976<br>July 27, 1976<br>Aug. 24, 1976<br>Dec. 23, 1975<br>Jan. 27, 1976<br>Feb. 25, 1976<br>Mar. 23, 1976<br>May 6, 1976<br>May 26, 1976<br>June <b>6</b> | NW¼NE¼ sec.10, T.1 S., R.21 E.<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do<br>do |                | 6.49<br>41.2<br>34.7<br>114<br>33.2<br>13.6<br>6.22<br>2.96<br>0.40<br>5.09<br>4.32<br>37.6<br>31.7<br>108<br>32.4<br>9.65 |

| MISCELLANEOUS<br>MEASUREMENT NO. 3 6 | DY TRIBUTARY TO OR DIVERTING FROM (C<br>JOhn Day River | 63<br>Gill  | COUNTY      |
|--------------------------------------|--|-------------|-------------|
| ROCK OF BER                          |  | GAGE-HEIGHT | DISCHARGE   |
| DATE                                 | LOCATION   | FEET        | SECOND-FEET |
| Apr. 28, 1931                        | At Condon  |             | 14.1        |
| May 24, 1934                         | Bl springs .5 mi ab West's Dam, 2.3                    |             | 1 1         |
|                                      | mi ab mouth, nr klondike                               |             | 1.1         |
| May 24, 1934                         | 300 yds ab West's dain                                 |             | 1.1         |
| June 1948                            | At mouth, nr Rock Creek station                        |             | * 163       |
| Nov. 10. 1965                        | SWANWA sec. 32, T.1 S., R.22 E.,                       |             | 4.33        |
| Mar. 8, 1966                         | NEISWI sec. 36, T.3 S., R.22 E. ab                     |             |             |
| Mai . 0, 1/00                        | Heppner Condon Hwy                                     |             | 2].11       |
| Mar. 8, 1966                         | SEASEA sec.22, T.2 S., R.22 E., bl                     |             |             |
| 1101. 09 2700                        | Dry Cr., nr Dam site (Condon)                          |             | 21.5        |
| Mar. 8, 1966                         | SW1NE1 sec.24, T.1 S., R.21 E.,                        |             |             |
|                                      | nr Condon  |             | 19.9        |
| ob                                   | SEANWA sec. 32, T.1 N., R.21 E., 300                   |             |             |
| uo                                   | ft bl barn.  |             | 18.2        |
| do                                   | NE1NW1 sec.24, T.1 N., R.20 E., ab                     |             |             |
| uo                                   | Rock Cr. 2.5 mi.                                       |             | 17.8        |
| do                                   | SWHNEH sec. 15. T.1 N., R.20 E.,                       |             |             |
| ·                                    | Rock Creek, 30 ft ab bridge                            |             | 35.5        |

| RECEIVI            | ED .                           | STATE OF ORECON                    |   |
|--------------------|--------------------------------|------------------------------------|---|
| AUG 1 2 199        | 1<br>WATER F                   | RESOURCES DEPART                   | MENT                                    |
| SALEM, OREGO       | Application                    | for Instream W                     | ater Right OREGC                        |
| ie veli pr         | 2 pissto more r by             | a State Agency                     | int capities in entrer ofs              |
|                    | There is                       | no fee required for this applicati | on.                                     |
| AApplicant:        | Randy Fisher                   | for_ <u></u> _                     | egon Deptof Fish & Wildlife<br>(Agency) |
| Mailing Add        | ress: 2501 S.W. F              | irst Ave., P. O. Box               | 59                                      |
|                    | Portland<br>City               | OR 97<br>State 2                   | 7207 229-5400 Ext. 438<br>Op Phone No:  |
| 3. Applicant:      |                                | for                                |   |
| Mailing Add        | (Director)                     |                                    | (Agency)                                |
|                    | City                           | State Z                            | p Phone No.                             |
| C. Applicant:      |                                | for                                |   |
|                    | (Director)                     |                                    | (Agency)                                |
| Mailing Add        | ess:                           |                                    |   |
|                    | City                           | State Z                            | p Phone No.                             |
|                    |                                |                                    |   |
| . The name of Rock | stream or lake of the<br>Creek | proposed instream wate             | er right is                             |
| a tributary or     | source (if lake) of            | John Day River                     | •                                       |
| . The public us    | e(s) this instream wa          | ter right is based upon i          | nclude:                                 |
| Upstream           | passage of adult a             | and juvenile fish incl             | uding summer steelhead and              |
|                    |                                |                                    |   |

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er ex

:

Instream Application No. \_\_\_\_\_\_

### CARCELLAND CONSIGNAD DUTA C

Certificate No.

3. The amount of water needed by month and/or year for each category of public use. If more space is needed, use a separate sheet of paper. avitability of A

| List      | quantiti | es in ei | ther cf | s, acre | -feet, c | r lake e | elevati | on abo       | ve Mea         | n Sea | Level |      |
|-----------|----------|----------|---------|---------|----------|----------|---------|--------------|----------------|-------|-------|------|
| Use(s)    | Jan      | Feb      | Mar     | Apr     | May      | Jun      | Jul     | Aug          | Sept.          | Oct   | Nov   | Dec  |
| Migration | of Anad  | romous   | fish    | and re  | sident   | fish     |         | * 13         |                |       |       |      |
|           |          |          |         |         |          |          |         |              |                |       |       |      |
|           | 34       | 57       | 57      | 57      | 57       | 34       | 34      | 34           | 34             | 34    |       | .34  |
|           |          |          |         | •       | • • •    |          |         | the Analysis | * *** **** *** |       | •     |      |
|           |          |          |         |         |          |          |         |              |                |       |       |      |
|           |          |          |         |         |          |          |         |              |                | 2250  | oh mm | 1.24 |
|           |          |          |         |         |          |          |         |              |                |       |       |      |
|           |          |          |         | •       |          |          |         |              |                |       |       |      |

4. The reach of the stream identified for an instream water right is from the:

upstream end at USGS Guaging station @ White Park (Station #14047390) ...

- River Mile (if known) RM 40.0
  - within the \_\_\_\_\_ 1/4 of the \_\_\_\_\_ SW\_\_\_ 1/4 of .\_\_\_\_\_
  - Section \_\_\_\_\_\_ Township \_\_\_\_\_\_ Range \_\_\_\_\_ 22E \_\_\_\_ W.M.,
- County \_\_\_\_\_Gilliam \_\_\_\_\_.

downstream end at \_\_\_\_\_ The mouth

River Mile (if known) \_\_\_\_\_0.0

within the \_\_\_\_\_ NE\_\_ 1/4 of the \_\_\_\_\_ SW\_\_\_ 1/4 of

Section \_\_\_\_\_ Township \_\_\_\_N Range \_\_\_\_9E \_\_\_W.M., County \_\_\_\_\_Gilliam \_\_\_\_\_.

Lake identified for an instream water right is

within the \_\_\_\_\_ 1/4 of the \_\_\_\_\_ 1/4 of

Section \_\_\_\_\_ Township \_\_\_\_\_ Range \_\_\_\_\_ W.M., County \_\_\_\_\_

5. Method(s) used to determine the requested amounts:

<u>Elow required to operate proposed fish passage facilities during migration</u> <u>period for adults and juveniles. Required flows are based on engineering determin</u> <u>using USGS data and passage facility design.</u>

| stroom   | Anotantia  | A la |
|----------|------------|------|
| Nu balli | ADDICALION | NO.  |

Certificate No.

6. When were the following state agencies notified of the intent to file for the instream water right?

| Department of Environmental Quality             | Date <u>2-7-90</u>  |
|---|---|
| Department of Fish and Wildlife                 | Date  |
| Parks and Recreation Division and Diversion     | Date Date Descut227-90in them equilate be and the   |
|   | The state of the Out Dist, Added the filles   |
| · · · · · · · · · · · · · · · ·                 | and the state of the second |
| 7. If possible, include recommendations for mea | suring locations or methods:  |

Measure @ USGS station 14047390 and by staff gauge @ the mouth RM 0.0

and the constant of press and press and press and the second second second second second second second second s

8. If possible, include recommendations for assisting the Water Resources Department (WRD) in measuring and monitoring procedures:

\_local\_watermaster\_will\_measure w/ periodic\_assistance\_from\_ODEW\_\_Monitoring\_\_\_\_ plan to be developed.

If possible, include other recommendations for methods or conditions necessary for managing the water right to protect the public uses (see OAR 690-77-020 (5)(c)): Monitoring plan to be developed.

Remarks: The Department of Fish and Wildlife is aggressively persuing the completion of a series of passage facilities at eight existing irrigation diversion structures. Once adult steelhead have access to the upper reaches of Rock Creek we expect an annual return of 1000 adults. Upstream passage of juvenile fish will be a critical component of the passage facilities function.

This application must be accompanied by a basin map with the applicable lake or stream reach identified.

An instream water right may be allowed for an instream beneficial use of water subject to existing water rights with an effective date prior to the filing date of this application.

This type of beneficial use is for the benefit of the public and a certificate issued confirming an instream water right shall be held in trust by the Water Resources Department for the people of the State of Oregon, pursuant to ORS 537.341.

3/21/90

Agency

Mancy M. Machush Signature

Oregon Dept. of Fish & Wildlife Assistant Director Title

| 70%                               | ani entrati a construit a                                 | . estiles componistion en  | name and principal and france          |
|-----------------------------------|---|--|--|
|                                   |   | ati yashi Ismamoni   | mitte memoringett                      |
| This is to certifing maps and the | y that I have examined the,<br>lata, and return them for: | foregoing application, toget   | her with the accompa                   |
|                                   | enhadenen en analian i ani                                |  |  |
| In order to re                    | tain its priority, this applic                            | cation must be returned t  | o the Water Resour                     |
| Department wi                     | th corrections on or before                               | and a second paralleline bas   | ponuseron autoria                      |
| Date:                             | , 19  | · · · · · · · ·  | ······································ |
| •                                 |   | · • • • • • • • • • • • • • • • • • • •  | · · · · ·                              |
|                                   | and can a car a c<br>a me contain a car a                 | Water Resource   | s Department                           |
|                                   |   | Title  |  |
|                                   | •   | · · · · · · · · · · · · · · · · · · ·  | · · · · · · · · · ·                    |
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| This document the $2151$          | was first received at the Wa<br>day of                    | ater Resources Department 19 $\underline{90}$ , at $\underline{2:50}$  | in Salem, Oregon, or<br>o'clock N      |
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| in the states                     | Liber Chinattis and a down                                | a set of a s |  |



R 20 E

R 22 E

| RECEIPT # 7   | STATE OF<br>WATER RESOURC<br>158 12TH<br>SALEM, OR<br>378-8455 / 378 | OREGON<br>ES DEPARTM<br>ST. N.E.<br>97310-0210<br>3-8130 (FAX) | ENT<br>INVOICE #. |                     |
|---------------|--|--|-------------------|---------------------|
| RECEIVED FROM | M: Moon Consul   | ting   | APPLICATION       | 70251               |
| BY:           |  | 1  | PERMIT            |                     |
|               |  |  | TRANSFER          |                     |
| CASH: CHE     | CK: # OTHER: (IDENTIFY)  | T  | OTAL REC'D        | \$200 <sup>20</sup> |
| 0417          | WRD MISC CASH ACCT   |  |                   | A State State       |
|               | ADJUDICATIONS  |  |                   | s                   |
|               | PUBLICATIONS / MAPS  | VED  |                   | s                   |
|               | OTHER: (IDENTIFY RECEI   | COUNTER  |                   | s                   |
|               | OTHER: ONER THE  | LUUM   |                   | s                   |
| BEDUC         | TION OF EXPENSE  |  |                   |                     |
| ILLDOO        | THOM OF EXI ENDE   | CASH AC  | CT.               | s                   |
|               | PCA AND OBJECT CLASS   | VOUCHE   | R #               | <u> </u>            |
| 0427          | WRD OPERATING ACCT   |  |                   |                     |
|               | MISCELLANEOUS  |  |                   |                     |
| 0407          | COPY & TAPE FEES   |  |                   | 5                   |
| 0410          | RESEARCH FEES  |  |                   | S                   |
| 0408          | MISC REVENUE: (IDENTIFY)   | A STATE OF A   |                   | s                   |
| 10105         | DEPOSIT LIAB. (IDENTIFT)   |  | San Star          | ÷                   |
|               | WATER RIGHTS:  | EXAM FEE   |                   | RECORD FEE          |
| 0201          | SURFACE WATER  | S  | 0202              | S                   |
| 0203          | GROUND WATER   | \$   | 0204              | S                   |
| 0205          | TRANSFER   | \$   | 0206              | S                   |
|               | WELL CONSTRUCTION  | EXAMPLE  | 0219              | CICENSE FEE         |
| 0218          | LANDOWNER'S REPAIL   | 5  | 0220              | s                   |
| 0223          | OTHER (IDENTIFY)   | otest  | -\$1              | 00000               |
| 0437          | WELL CONST. START FEE  |  | -                 |                     |
| 0211          | WELL CONST START FEE   | S  | CARD #            |                     |
| 0210          | MONITORING WELLS   | S  | CARD #            | and the second      |
| 1.1           | OTHER (IDENTIFY)   | -  |                   |                     |
| 0539          | LOTTERY PROCEEDS   |  |                   | CHARLES             |
| 1302          | LOTTERY PROCEEDS   |  |                   | S                   |
| 0467          | HYDRO ACTIVITY   | LIC NUMBER   |                   |                     |
| 0233          | POWER LICENSE FEE (FW/WRD)   |  |                   | S                   |
| 0231          | HYDRO LICENSE FEE (FW/WRD)   |  |                   | \$                  |
|               | HRDRO APPLICATION  | 5.000 CC2  |                   | S                   |
| RECEIPT # 7   | 176 DATED: 10  | - 4-96<br>opy-Fiscal, Blue Copy                                | BY:               | Stan                |



DEPARTMENT OF FISH AND WILDLIFE 2501 SW First Ave., P.O. Box 59 Portland, Oregon 97207



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Mike Mattick Water Resources Dept. 158 12th Street, NE Salem, OR 97310

97310-0705

Helialanda Harallillanda and Haralda helialada helialada

| INS MODEL                             |
|---------------------------------------|
| Application No.                       |
| Permit No                             |
| 3-21-90                               |
| Name OR Dept. of Fish & Wildlife      |
| Address PO Box 59, Portland, OR 97207 |
| Assigned                              |
| Address                               |
| Beginning construction                |
| Completion of construction            |
| Extended to                           |
| Complete application of water         |
| Extended to                           |
|                                       |

Form 111