Groundwater Application Review Summary Form

Application # G- <u>19398</u>
GW Reviewer Steve Ahlquist Date Review Completed: 4/16/2024
Summary of GW Availability and Injury Review:
Groundwater for the proposed use is either over appropriated, will not likely be available in the amounts requested without injury to prior water rights, OR will not likely be available within the capacity of the groundwater resource per Section B of the attached review form.
Summary of Potential for Substantial Interference Review:
There is the potential for substantial interference per Section C of the attached review form.
Summary of Well Construction Assessment:
☐ The well does not appear to meet current well construction standards per Section D of the attached review form. Route through Well Construction and Compliance Section.
This is only a summary. Documentation is attached and should be read thoroughly to understand the

basis for determinations and for conditions that may be necessary for a permit (if one is issued).

WATER RESOURCES DEPARTMENT

MEM	(O	_April 16, 2024_								
TO:		Application G19398_								
FRO	М:	GW: Steve Ahlquist (Reviewer's Name)								
SUBJ	ECT: S	cenic Waterway Interference Evaluation								
\boxtimes	YES	The source of appropriation is hydraulically connected to a State Scenic								
	NO	Waterway or its tributaries								
\boxtimes	YES									
	NO	Use the Scenic Waterway Condition (Condition 7J)								
	interfe	RS 390.835, the Groundwater Section is able to calculate ground water rence with surface water that contributes to a Scenic Waterway. The calculated rence is distributed below								
	interfer Depar propos	RS 390.835, the Groundwater Section is unable to calculate ground water rence with surface water that contributes to a scenic waterway; therefore , the tment is unable to find that there is a preponderance of evidence that the sed use will measurably reduce the surface water flows necessary to ain the free-flowing character of a scenic waterway								

DISTRIBUTION OF INTERFERENCE

Calculate the percentage of consumptive use by month and fill in the table below. If interference cannot be calculated, per criteria in 390.835, do not fill in the table but check the "unable" option above, thus informing Water Rights that the Department is unable to make a Preponderance of Evidence finding.

Exercise of this permit is calculated to reduce monthly flows in <u>Rogue</u> Scenic Waterway by the following amounts expressed as a proportion of the consumptive use by which surface water flow is reduced.

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
0.083	0.083	0.083	0.083	0.083	0.083	0.083	0.083	0.083	0.083	0.083	0.083

PURUIC INTEREST	REVIEW FOR	GROUNDWATER	APPI ICATIONS

TO:	Water	r Rights Secti	on		Date	<u>4</u>	/16/2024		
FROM:	: Groui	ndwater Secti	on	Steve Ah					
CLIDIE	COTT. A 1'	· · · · ·	2200		r's Name				
SUBJE	CI: Appli	cation G- <u>19</u>	9398_	Supersedes	review of		Date of	Daviand	(a)
							Date of	Keview((8)
PUBLI	C INTEREST	PRESUMP	TION; GROUN	NDWATER					
					groundwater use will e	ensure the	preservation	n of the	e public
welfare,	safety and healt	th as described	l in ORS 537.525.	Department sta	aff review groundwate	r applicati	ons under O	AR 69	0-310-140
					allows the proposed				
the presi	umption criteria.	This review i	s based upon ava	ilable informa	ation and agency poli	cies in pla	ce at the tin	me of e	evaluation.
A. GEN	NERAL INFO	RMATION:	Annlicant's	Name: Sa	nh Di Ton and Hoa k	Kim Ton	County	· Jac	kson
110 <u>GE</u> 1	(LILLIE II (I O	THE PROPERTY OF THE PROPERTY O	i ippiieum s	Traine. Da		1111 1011	county	. <u>- 540</u>	115011
A1.	Applicant(s) se	ek(s) <u>0.84</u>	cfs from 4	well(s)	in the Rogue				Basin,
	Middle	Rogue		subbasii	n				
	Wilddic .	Rogue		subbasii	11				
A2.	Proposed use	Nurser	y (65.5 ac, 164 af)	Season	ality: Year-round				
	1 _		, , , , , , , , , , , , , , , , , , , ,		, <u> </u>				
A3.	Well and aquife	er data (attach	and number logs	s for existing v	vells; mark proposed	wells as s	uch under	logid):	
POA		Applicant's		Propose	ed Location		Location, met	tes and	hounds e a
Well	Logid	Well #	Proposed Aquife	Rate(cf:			2250' N, 1200		
1	JACK 56114	1	Bedrock	0.84	T36S/R1W-27 S	ENW	3635' N, 146	0' E fr S	SW cor S 27
2	Proposed	2	Bedrock	0.84	T36S/R1W-27 S			O' E from SW cor S 27	
3 4	Proposed Proposed	3 4	Bedrock Bedrock	0.84 0.84	T36S/R1W-27 S T36S/R1W-27 N		2765' N, 2000' 2350' N, 2000'		
	ım, CRB, Bedrock		Dedrock	0.64	1305/K1W-271	IE 5 W	2330 IN, 2000	L Hom	3 W COI 3 27
7 1114 116	ini, ereb, bedroer	_							
POA	Well Depth	Seal Interval	Casing Intervals	Liner Intervals	Perforations Or Screen	s Well Yi	ield Draw	down	Test Type
Well	(ft)	(ft)	(ft)	(ft)	(ft)	(gpm			
2	160 200	0 - 20 0 - 20	+1 - 45 +1 - 45	0 - 160 0 - 200	120 - 160 120 - 200	20 TPD	20 160 TBD TBD		Air TBD
3	200	0 - 20	+1 - 45	0 - 200	120 - 200	TBD			TBD
4	200	0 - 20	+1 - 45	0 - 200	120 - 200	TBD			TBD
POA	Land Surface Ele		Depth of First Wat		SWL		ence Level	Refe	rence Level
Well 1	(ft an		(ft bls) 125	(ft bls) 22	Date 06/09/2003		(ft bls)		Date TBD
2	138		TBD	TBD	TBD		TBD TBD		TBD
3	138		TBD	TBD	TBD		TBD		TBD
4	138		TBD	TBD	TBD		TBD		TBD
Use data	from application	for proposed we	lls.						
A4.	Comments: T	his annlication	is for year-round	irrigation/nurs	ery use of 65.5 acres a	nd 1 acre f	foot of stora	ge in I	ackson
Д.					ain water from one exi				
					200 feet deep to provi				
			d total annual volu						
					n descriptions and the	latitude aı	nd longitude	coord	inates (GPS
	locations) prov	ided for each p	proposed POA in the	he application i	map. This review assu	mes the pr	oposed POA	As are !	located at
	the provided la	titude and long	titude coordinates.						
A5. 🗆	Provisions of t	he Rogue			Basin rules relative to	the devel	lopment, cla	ıssifica	tion and/or
	management of	groundwater 1	hydraulically conn	nected to surfac	e water \square are, or \boxtimes	are not	activated by	this a	pplication
	(Not all basin r	-	•					u	rr
				OAR 690-515)	does not contain such	orovisions			

В. <u>GR</u>		DWATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070
B1.	Bas	ed upon available data, I have determined that groundwater* for the proposed use:
	a.	□ is over appropriated, \boxtimes is not over appropriated, or □ cannot be determined to be over appropriated during any period of the proposed use. * This finding is limited to the groundwater portion of the over-appropriation determination as prescribed in OAR 690-310-130;
	b.	\square will not or \square will likely be available in the amounts requested without injury to prior water rights. * This finding is limited to the groundwater portion of the injury determination as prescribed in OAR 690-310-130;
	c.	\boxtimes will not or \square will likely to be available within the capacity of the groundwater resource; or
	d.	 □ will, if properly conditioned, avoid injury to existing groundwater rights or to the groundwater resource: i.
B2.	a.	☐ Condition to allow groundwater production from no deeper than ft. below land surface;
	b.	☐ Condition to allow groundwater production from no shallower than ft. below land surface;
	c.	Condition to allow groundwater production only from the groundwater reservoir between approximately ft. and ft. below land surface;
	d.	☐ Well reconstruction is necessary to accomplish one or more of the above conditions. The problems that are likely to occur with this use and without reconstructing are cited below. Without reconstruction, I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Groundwater Section.
		Describe injury —as related to water availability— that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc):
В3.	POA (see	bundwater availability remarks: The proposed POAs would produce water from the fractured-rock aquifer of the estin formation (Western Cascades Volcanics; Wiley, 1993). Water in this aquifer system is transmitted via secondary obsity in interconnected fractures. The OWRD well report database contains records for 15 water wells near the proposed As (Sec. 27, T36S R1W). According to the well reports, the median and maximum yields are 22 and 40 gpm, respectively attached Well Statistics). The requested rate of 375 gpm (0.84 cfs) is much higher than reported well yields in the area. In the four proposed POAs will achieve the requested rate so the proposed use is found to not likely be itable within the capacity of the groundwater resource.

closest residences with potential wells are located approximately 225 feet west of proposed POA 1 and approximately 240 northeast of proposed POA 2. Theis (1935) drawdown analyses were conducted to assess potential well-to-well interference at the potential nearby domestic wells due to pumping at the proposed POAs. Permits issued for nearby POAs contain the standard condition requiring curtailment of pumping when interference with a neighboring well exceeds 25 feet of drawdown; any permit pursuant to this application would be conditioned similarly. Therefore, the potential for interference to nearby wells was evaluated based on the likelihood of well-to-well interference exceeding 25 feet due to pumping at the proposed POAs. Hydraulic parameters used in the Theis analyses are within the typical range of values for the hydrogeologic

regime (Freeze and Cherry, 1979). The applicant did not indicate well-specific rates and annual volumes for the proposed POAs so each well was evaluated individually at the maximum requested rate (0.84 cfs/375 gpm) until reaching the requested annual volume of 164 acre-feet, which would take approximately 99 days. Results of the Theis analyses indicate drawdown at the adjacent residential properties would exceed 25 feet as a result of pumping at the maximum requested rate at any of the POAs. Due to the expected well-to-well interference, the proposed use is found to not likely be available within the capacity of the groundwater resource. If the pumping rate was reduced to 0.22 cfs (annual volume [164 sf] spread over 365 days), drawdown would still exceed 25 feet at the neighboring properties as a result of pumping at proposed POA 1 and POA 2. A pumping rate of 0.22 cfs at POA 3 and POA 4 would likely not result in well-to-well interference greater than 25 feet at neighboring properties.

C. GROUNDWATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. **690-09-040** (1): Evaluation of aquifer confinement:

Well	Aquifer or Proposed Aquifer	Confined	Unconfined
1	Fractured Bedrock of Colestin Formation		⊠
2	Fractured Bedrock of Colestin Formation		×
3	Fractured Bedrock of Colestin Formation		×
4	Fractured Bedrock of Colestin Formation		⊠

Basis for aquifer confinement evaluation: Water in this fractured bedrock aquifer system is primarily transmitted through interconnected fractures that generally extend near the surface and is therefore under atmospheric pressure/unconfined conditions.

C2. **690-09-040** (2) (3): Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ½ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	Surface Water Name GW SW Elev Elev ft msl ft msl Distance (ft) Hydraulically Connected? YES NO ASSUMED					Potentia Subst. Int Assum YES	terfer.	
1	1	Whetstone Creek	1362	1343	4875	\boxtimes				\boxtimes
2	1	Whetstone Creek	1362	1343	5420	\boxtimes				⊠
3	1	Whetstone Creek	1362	1343	5375	\boxtimes				⊠
4	1	Whetstone Creek	1362	1343	5490	×				\boxtimes
1	2	Dry Creek	1362	1358	7430	×				⊠
2	2	Dry Creek	1362	1358	7100	\boxtimes				\boxtimes
3	2	Dry Creek	1362	1359	7845	×				\boxtimes
4	2	Dry Creek	1362	1360	8025	×				⊠

Basis for aquifer hydraulic connection evaluation: Groundwater elevations in proposed POA 1 and nearby wells are similar and above surface water elevations indicating that groundwater is flowing towards and discharging to nearby streams. The unnamed tributary to Whetstone Creek that flows through Hoover Ponds County Park is reportedly intermittent and does not appear to receive groundwater baseflow.

Water Availability Basin the well(s) are located within:

SW#1: ROGUE R> PACIFIC OCEAN-AB CURRY AB CURRY G AT GAGE 14359000 (WID #270)

SW#2: ANTELOPE CR > LITTLE BUTTE CR - AT MOUTH (WID #248)

C3a. **690-09-040** (4): Evaluation of stream impacts for <u>each well</u> that has been determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water (SW) source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that SW source, not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% *natural* flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked ⋈ box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < 1/4 mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
1	1			NA	NA		1130		>25	⊠

C3b. **690-09-040 (4):** Evaluation of stream impacts by total appropriation for all wells determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. **Complete only if Q is distributed among wells.** Otherwise same evaluation and limitations apply as in C3a above.

		11 /							
	SW #	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?

Comments: Impact to Whetstone Creek from the proposed use was estimated using the Hunt (1999) stream depletion model using hydrogeologic parameters representative of bulk aquifer properties (see attached Hunt Model Stream Depletion Analysis).

C4a. **690-09-040 (5):** Estimated impacts on **hydraulically connected surface water sources greater than one mile** as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

Non-Di	istributed	Wells											
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
4	2	3 %	18 %	33 %	42 %	49 %	53 %	57 %	60 %	62 %	64 %	65 %	67 %
Well Q	as CFS	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22
Interference CFS		0.00	0.04	0.07	0.09	0.11	0.12	0.13	0.13	0.14	0.14	0.15	0.15
Distrib	uted Well	ls											
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	9/
Well Q	as CFS												
Interfere	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	9/
Well Q	as CFS	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.22
Interfere	ence CFS	0.00	0.04	0.07	0.09	0.11	0.12	0.13	0.13	0.14	0.14	0.15	0.15
(A) = To	otal Interf.	0.00	0.04	0.07	0.09	0.11	0.12	0.13	0.13	0.14	0.14	0.15	0.15
(B) = 80	% Nat. Q	17.50	29.00	31.70	34.70	11.70	6.62	5.74	5.92	3.31	1.06	2.21	5.47
(C) = 1	% Nat. Q	0.175	0.29	0.317	0.347	0.117	0.0662	0.0574	0.0592	0.0331	0.0106	0.0221	0.0547
(D) = ($(\mathbf{A}) > (\mathbf{C})$	√	√	\checkmark	√	√	V	V	V	V	V	V	✓
$(\mathbf{E}) = (\mathbf{A})$	/B) x 100	0.0 %	0.1 %	0.2 %	0.3 %	0.9 %	1.8 %	2.3 %	2.2 %	4.2 %	13 %	6.8 %	2.7 %

(A) = total interference as CFS; (B) = WAB calculated natural flow at 80% exceed. as CFS; (C) = 1% of calculated natural flow at 80% exceed. as CFS; (D) = highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage.

	Basis for impact evaluation: Impacts to Dry Creek were estimated using the Hunt (1999) stream depletion model with bulk
	aquifer parameters representative of the local geology. Dry Creek is located within the most limited WAB (Antelope Creek) in the vicinity. The table above shows the stream depletion for Dry Creek due to pumping at the farthest proposed POA (Well 4).
	The pumping rate of 0.22 cfs assumes that the requested annual volume (164 af) is evenly distributed over the period of use
	(365 days/year). Modeled interference exceeds 1% of the 80% exceedance streamflow for Dry Creek from June through
	December. Stream interference is expected to be greater at the other proposed wells which are closer to Dry Creek. The
	estimated impacts on Dry Creek result in a finding of PSI per OAR 690-009.
C4b.	690-09-040 (5) (b) The potential to impair or detrimentally affect the public interest is to be determined by the Water Rights Section.
C5. [☐ If properly conditioned , the surface water source(s) can be adequately protected from interference, and/or groundwater use under this permit can be regulated if it is found to substantially interfere with surface water: i. ☐ The permit should contain condition #(s) ;
	ii. The permit should contain special condition(s) as indicated in "Remarks" below;
	ii. — The permit should contain special condition(s) as indicated in Remarks below,
<u>r</u> <u>p</u>	SW / GW Remarks and Conditions: Results of the stream depletion (Hunt 1999) modeling indicate the proposed use would esult in greater than 25% stream depletion at Whetstone Creek within 30 days of pumping and therefore is found to have the otential for substantial interference (PSI). Reducing the pumping rate would not change the PSI finding for Whetstone Creek. Additionally, stream depletion of Dry Creek would exceed 1% of the 80% exceedance natural streamflow from June through December. The proposed use is found to have PSI with Whetstone Creek and Dry Creek per OAR 690-009.
_	
S	The OWRD Water Availability Reporting System (WARS) has determined that groundwater use has measurably reduced the urface water flows necessary to maintain the free-flowing character of the Rogue Scenic Waterway as per ORS 390.835. The proposed groundwater use would further reduce surface water flow to the Rogue Scenic Waterway.
<u> </u>	roposed groundwater use would ruriner reduce surface water now to the rogue beeme waterway.
_	
_	
I	References Used:
<u> </u>	Application File: G-19398
E	Freeze, R.A. and Cherry, J.A., 1979, Groundwater, Prentice Hall, Englewood Cliffs, New Jersey, 604 p.
<u>I</u>	Hunt, B. 1999. Unsteady Stream Depletion from Ground Water Pumping. Journal of Hydrologic Engineering, Vol 8(1), pp12-19
	Theis, C.V., 1935. The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using groundwater storage, Am. Geophys. Union Trans., vol. 16, pp. 519-524.
<u>q</u>	Wiley, T.J., and Smith, J.G., 1993, Preliminary geologic map of the Medford East, Medford West, Eagle Point, and Sams Valley undrangles, Jackson County, Oregon: Oregon Department of Geology and Mineral Industries, Open-File Report 93-13, scale :24,000.

D. WELL CONSTRUCTION, OAR 690-200

D1.	Well #:	Logid:							
D2.	THE WELL does not appear to meet current well construction standards based upon:								
	a. \square review of	of the well log;							
	b. field insp	pection by	;						
	c. \square report of	f CWRE	,						
		pecify)							
D3.	THE WELL con	astruction deficiency or other comment is described as follows:							
D4.	Route to the W	ell Construction and Compliance Section for a review of existing wo	ell construction.						

Water Availability Tables

ROGUE R > PACIFIC OCEAN - AB CURRY G AT GAGE 14359000 ROGUE BASIN

Water Availability as of 3/20/2024

Watershed ID #: 270 (Map) Date: 3/20/2024 Exceedance Level: 80% V
Time: 3:48 PM

Water Availability Calculation

Monthly Streamflow in Cubic Feet per Second Annual Volume at 50% Exceedance in Acre-Feet

Month	Natural Stream Flow	Consumptive Uses and Storages	Expected Stream Flow	Reserved Stream Flow	Instream Flow Requirement	Net Water Available
JAN	2,180.00	1,130.00	1,050.00	0.00	1,200.00	-149.00
FEB	2,710.00	2,050.00	663.00	0.00	1,200.00	-537.00
MAR	2,750.00	1,820.00	932.00	0.00	1,200.00	-268.00
APR	2,810.00	1,040.00	1,770.00	0.00	1,200.00	573.00
MAY	2,750.00	368.00	2,380.00	0.00	1,200.00	1,180.00
JUN	1,760.00	344.00	1,420.00	0.00	1,200.00	216.00
JUL	1,330.00	369.00	961.00	0.00	1,200.00	-239.00
AUG	1,160.00	331.00	829.00	0.00	1,200.00	-371.00
SEP	1,130.00	276.00	854.00	0.00	1,200.00	-346.00
OCT	1,160.00	228.00	932.00	0.00	1,200.00	-268.00
NOV	1,370.00	345.00	1,020.00	0.00	1,200.00	-175.00
DEC	1,810.00	563.00	1,250.00	0.00	1,200.00	47.30
ANN	1,900,000.00	529,000.00	1,370,000.00	0.00	869,000.00	532,000.00

ANTELOPE CR > LITTLE BUTTE CR - AT MOUTH ROGUE BASIN

Water Availability as of 3/20/2024

Watershed ID #: 248 (Map)

Date: 3/20/2024

Exceedance Level: 80% V

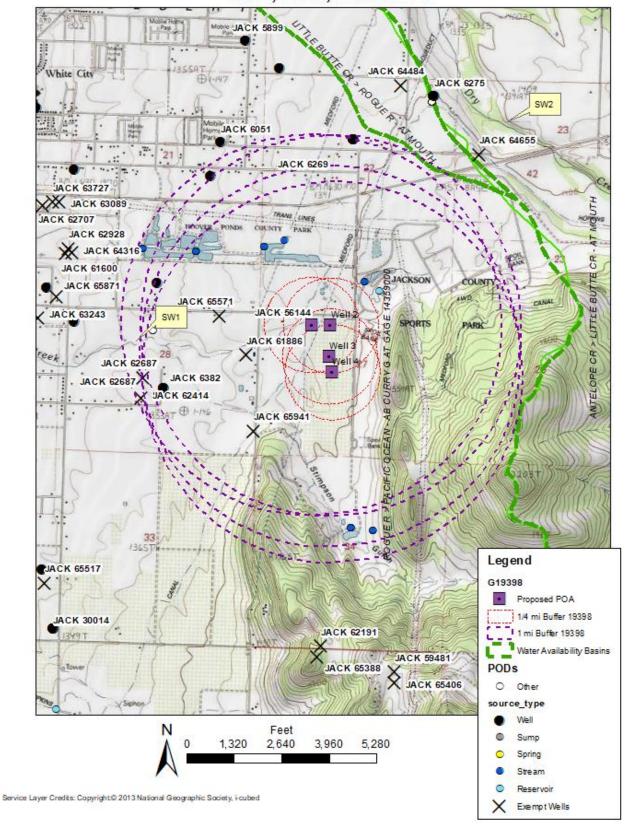
Water Availability Calculation

Monthly Streamflow in Cubic Feet per Second Annual Volume at 50% Exceedance in Acre-Feet

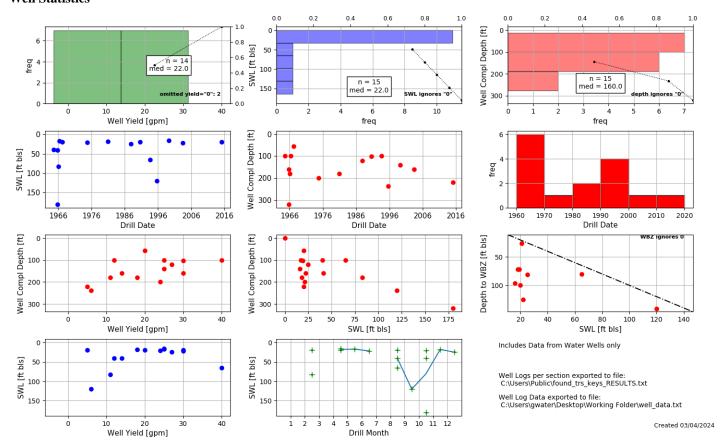
Month	Natural Stream Flow	Consumptive Uses and Storages	Expected Stream Flow	Reserved Stream Flow	Instream Flow Requirement	Net Water Available
JAN	17.50	4.93	12.60	0.00	50.10	-37.50
FEB	29.00	6.19	22.80	0.00	60.00	-37.20
MAR	31.70	5.92	25.80	0.00	60.00	-34.20
APR	34.70	0.66	34.00	0.00	57.80	-23.80
MAY	11.70	1.36	10.30	0.00	28.00	-17.70
JUN	6.62	2.12	4.51	0.00	8.71	-4.20
JUL	5.74	3.00	2.74	0.00	5.70	-2.96
AUG	5.92	2.44	3.48	0.00	5.00	-1.52
SEP	3.31	1.54	1.77	0.00	20.00	-18.20
OCT	1.06	0.24	0.83	0.00	20.00	-19.20
NOV	2.21	0.51	1.70	0.00	25.00	-23.30
DEC	5.47	3.08	2.39	0.00	31.30	-28.90
ANN	19,100.00	1,920.00	17,100.00	0.00	22,300.00	0.00

Well Location Map

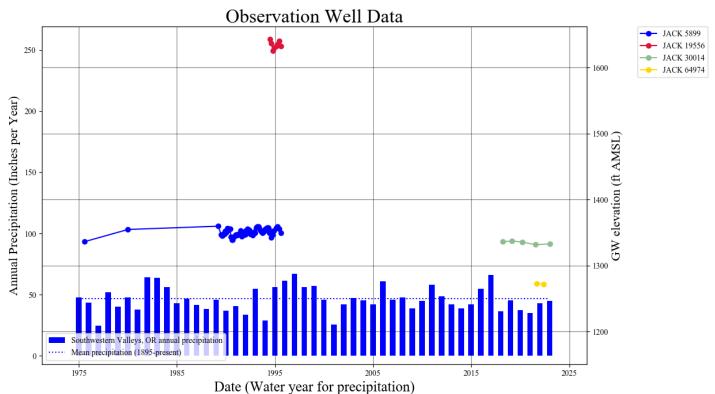
Application G19398 Sanh Di Ton and Hoa Kim Ton T36S, R1W, Section 27



Well Statistics



Water-Level Measurements in Nearby Wells



Theis Interference Analysis Theis Time-Drawdown Worksheet v.5.00 Calculates Theis nonequilibrium drawdown and recovery at any arbitrary radial distance, r, from a pumping well for 3 different T values and Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 142560 minutes = 99.00 d radial distance, r, from a pumping well for 3 different T values and 2 different S values. Written by Karl C. Wozniak September 1992. Last modified December 17, 2019 20.00 Input Data: Total pumping time Radial distance from pumped well: feet Q conversions Pumping rate Hydraulic conductivity 376.99 gpm 0.84 cfs 50.40 cfm 60.00 Drawo Aquifer thickness Storativity 72 576 00 cfd 100 00 Transmissivity Conversions _f2pd 100 50 0.069444 0.34722 ft2/day 0.694444 Recalculate ft2/min 7480 gpd/ft Elapsed Time Since Pumping Started, days Use the Recalculate button if recalculation is set to manua Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 142560 minutes = 99.00 days Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 142580 minutes = 99.00 days Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 142560 minutes = 99.00 days 0.00 0.00 100.00 100.00 feet <u>B</u> 200.00 feet 200.00 200 00 Drawdown, 홍 300.00 300.00 Draw 400 00 400.00 500.00 500.00 600.00 600 00 600.00 200000 400000 600000 800000 100 1000 10000 100000 1000000 Elapsed Time Since Pumping Started, minutes Flansed Time Since Pumping Started minutes Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 142560 minutes = 99.00 days Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 142560 minutes = 99.00 days Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 142560 minutes = 99.00 days 0.00 0.00 0.00 100.00 100.0 100.00 ₹ 200.00 feet feet 200.00 200.00 Drawdown. 통 용300.00 300.0 300.00 Dra 5 400 00 400 00 400 00 500.00 500.00 500.0 600.00 600.00 100 000 200,000 300,000 400,000 0.010 0.100 1000.000 10.000 Elapsed Time Since Pumping Started, days Elapsed Time Since Pumping Started, days Theis Time-Drawdown Worksheet v.5.00 Theis Drawdown and Recovery at r = 240 ft From Pumping Well Calculates Theis nonequilibrium drawdown and recovery at any arbitrary radial distance, r, from a pumping well for 3 different T values and radial distance, r, from a pumping well for 3 different T values and 2 different S values. Written by Karl C. Wozniak September 1992. Last modified December 17, 2019 0.00 5.00 Var Name Scenario 1 Scenario 2 10.00 feet Total pumping time Radial distance from pumped well: Pumping rate Hydraulic conductivity 15.00 98.74 gpm 0.22 cfs 13.20 cfm 20.00 25.00 Aquifer thickness Storativity 30.00 S_2 T_f2pd 35.00 Transmissivity Conversions ft2/day 0.3472 0.694444 10000.000 7480 gpd/ft 0.100 Elapsed Time Since Pumping Started, days Use the Recalculate button if recalculation is set to manual Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 525600 minutes = 365.00 days Theis Drawdown and Recovery at r = 240 ft From Pumping Well Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 525600 minutes = 365.00 day: Pump on = 525600 0.00 20.00 20.00 20.00 40.00 40.00 40.00 feet feet 60.00 60.00 60.00 80.00 80.00 80.00 100.00 100.0 100.00 120.00 120.00 120.00 140 00 140 00 140 00 160.00 160.00 10000 100000 100000010000000 100 1000 10000 Elapsed Time Since Pumping Started, minutes Elapsed Time Since Pumping Started, minutes Theis Drawdown and Recovery at r = 240 ft From Pumping Well Theis Drawdown and Recovery at r = 240 ft From Pumping Well Theis Drawdown and Recovery at r = 240 ft From Pumping Well Pump on = 525600 i utes = 365.00 day Pump on = 525600 minutes = 365.00 days Pump on = 525800 minutes = 365.00 days 0.00 0.00 20.00 20.00 20.00 40.00 40.00 40.00 feet feet 60.00 60.00 60.00 Drawdown, 80 00 80.00 80.00 100.00 100.00 100.00 120.00 120.00 120.00 140.00 140.00 160.00 160.00 160.00 100 t/t 200.000 300.000 400.000 0.100 10.000 100.000 1000.000 10000.000 1.000 10 1000 10000 Elapsed Time Since Pumping Started, days Elapsed Time Since Pumping Started, days

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Stream Depletion (Hunt) Model Analysis

	Application type:									G						
	Application number:									19398						
	Well number:									1						
	Stream Number:									1						
	Pumping rate (cfs):									0.22						
	Pumping duration (days):									365						
	Pumping start month number (3=March							:March)	ĺ	1						
									,							
	Parameter							nario 1	Sc	Scenario 2 S		nario 3	Units			
Distanc	Distance from well to stream						4900		49	4900		4900		ft		
Aquifer	Aquifer transmissivity						100		50	500		1000		ft2/day		
Aquifer	Aquifer storativity						.001		.0	.0005		01	-			
Aquitard vertical hydraulic conductivity						9	0.0)1	0.	05	0.1		ft/day			
Not used						0		0	0		0					
Aquitard thickness below stream						babs		4		3		2		ft		
Not use	Not used						0		0		0					
Stream	Stream width		ws		10		20	20		30		ft				
				Stre	am dep	letio	n fo	or Scena	rio 2:							
Days	1	31	62	92	122	153		183	213	244	274	304	335	365		
Depletion (%)	0	35	49	57	62	66		68	70	72	74	75	76	77		
Depletion (cfs)	0.00	0.08	0.11	0.13	0.14	0.1	4	0.15	0.16	0.16	0.16	0.16	0.17	0.17		

