PUBLIC INTEREST REVIEW FOR GROUND WATER APPLICATIONS

<u>1 UDI</u>										<u>_</u>			
TO:		Water	Rights S	ection				Dat	e	Novemb	<u>er 20, 20</u>	008	
FROM	[:	Groun	d Water/	Hydrology	Section	Marc	Norton						
	CT.					Dovi	ower's Name						
SUBJE	ECT:	Applic	cation G-	17109		Su	persedes re	view of			Date of Rev	view(s)	
OAR 6 welfare to deter the pres	90-310-1 , <i>safety an</i> mine whe	30 (1) <i>The distribution</i> 10 <i>The althory the criteria.</i>	he Depart h as descr presumpt	<i>ibed in ORS</i> ion is establ ew is based	<i>ished.</i> OA	DWATE at a propos Departmen R 690-310- ilable info	R ed groundwa t staff review 140 allows t rmation and	ater use will v ground wa he proposed l agency pol rothers	<i>ensur</i> ter apj use b icies i	the press plications be modified in place at	ervation of under OA d or cond t the time	of the put AR 690-3 itioned to e of evalu	<i>blic</i> 10-140 o meet uation .
A1.	Applica	nt(s) see	ek(s) <u>0.3</u>	<u>3</u> cfs from	m <u>2</u>	well	(s) in the	Willamett	e Rivo	er			_Basin,
]	Fualatin	River			subb	asin Qu	ad Map: <u>S</u>	cholls	& Hillsb	oro		
A2. A3.	Propose Well an	ed use: d aquife	r data (att	ach and nu	mber logs	Seas for existin	onality: ng wells; ma	rk proposed	l well	s as such	under log	gid):	
Wel 1	Logi	id	Applican s Well #	PIC	oposed Juifer*	Propose Rate(cf		Location /R-S QQ-Q)			i, metes a l, 1200' E		
1	WASH	64048	1	All	uvium	0.167	015/02	2W-8 NW N	W		5, 1170' E		
2	Propo	sed	2	All	uvium	0.167	01S/0	2W-8 SW N	W	1770' S	6, 1140' E	fr NW co	or S 8
3													
4 5													
	um, CRB,	Bedrock											
Well	Well Elev ft msl	First Water ft bls	SWL ft bls	SWL Date	Well Depth (ft)	Seal Interval (ft)	Casing Intervals (ft)	Liner Intervals (ft)	Or	forations Screens (ft)	Well Yield (gpm)	Draw Down (ft)	Test Type
1	150	80	0	6/1/2006	163	0 – 65	+1 - 163		123	- 90 - 110 - 133 - 158	36 – 52		Air
2	155				200								
Use data	from app	lication f	or proposed	wells									
Use uala	anom app		or proposed	1 wells.									

A4. Comments: See conceptual model discussion for more details on geology and ground water.

Requested discharge rate is 150 gpm = 0.33 cfs, 0.167 cfs from each well.

- <u>apply.</u>
- A6. Well(s) #____

Name of administrative area: <u>N.A.</u> Comments: _____

, ____, ___, ___, ___, ___, ___, tap(s) an aquifer limited by an administrative restriction.

B. GROUND WATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070

- B1. **Based upon available data**, I have determined that ground water* for the proposed use:
 - **is** over appropriated, **is not** over appropriated, or **is cannot be determined to be** over appropriated during any a. period of the proposed use. * This finding is limited to the ground water portion of the over-appropriation determination as prescribed in OAR 690-310-130;
 - will not or will likely be available in the amounts requested without injury to prior water rights. * This finding b. is limited to the ground water portion of the injury determination as prescribed in OAR 690-310-130;
 - will not or will likely to be available within the capacity of the ground water resource; or c.
 - **will, if properly conditioned**, avoid injury to existing ground water rights or to the ground water resource: d. i.
 - The permit should contain condition #(s) 7N Annual Water Level Measurement + large measurement and reporting with totalizing flow meters on both wells
 - The permit should be conditioned as indicated in item 2 below. ii.
 - iii. The permit should contain special condition(s) as indicated in item 3 below;
- Condition to allow ground water production from no deeper than ______ ft. below land surface; B2. a.
 - **Condition** to allow ground water production from no shallower than ______ ft. below land surface; b.
 - Condition to allow ground water production only from the Alluvial _____ ground C. ft. below land surface; water reservoir between approximately ft. and
 - d. Well reconstruction is necessary to accomplish one or more of the above conditions. The problems that are likely to occur with this use and without reconstructing are cited below. Without reconstruction, I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Ground Water Section.

Describe injury –as related to water availability– that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc):

B3. Ground water availability remarks: The wells develop water from an alluvial aquifer that is hydraulically connected to the Tualatin River.

Date

C. GROUND WATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. 690-09-040 (1): Evaluation of aquifer confinement:

Wel 1	Aquifer or Proposed Aquifer	Confined	Unconfined
1	Alluvium	\boxtimes	
2	Alluvium	\boxtimes	

Basis for aquifer confinement evaluation: Ground water level rose above where it was encountered.

C2. 690-09-040 (2) (3): Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¹/₄ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	GW Elev ft msl	SW Elev ft msl	Distance (ft)	Hydraulically Connected? YES NO ASSUMED	Potential for Subst. Interfer. Assumed? YES NO
1	1	Tualatin River	150	120	3870		
2	1	Tualatin River	150	120	3800		

Basis for aquifer hydraulic connection evaluation: Ground water levels are above the elevation in the Tualatin River. Impacts to the river are minimized because of the Willamette Silt that overlies the water bearing sands and gravels.

Water Availability Basin the well(s) are located within: TUALATIN R> WILLAMETTE R- AT GAGE 14206500

C3a. 690-09-040 (4): Evaluation of stream impacts for <u>each well</u> that has been determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that surface water source, and not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% natural flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked 🖂 box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < ^{1/4} mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
1	1			IS73538	100		44.3		< 25%	
2	1			IS73538	100		44.3		< 25%	

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C3b. **690-09-040 (4):** Evaluation of stream impacts by total appropriation for all wells determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Complete only if Q is distributed among wells. Otherwise same evaluation and limitations apply as in C3a above.

Buille evaluatio								
SW #	Qw > 5 cfs?	InstreamInstreamWaterWaterRightRight QID(cfs)		Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
		IS73538	100		44.3		< 25%	

Comments: ______ The requested discharge rate of 0.33 cfs is below the 1% values of the in-stream and natural flow.

C4a. **690-09-040 (5):** Estimated impacts on **hydraulically connected surface water sources greater than one mile** as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

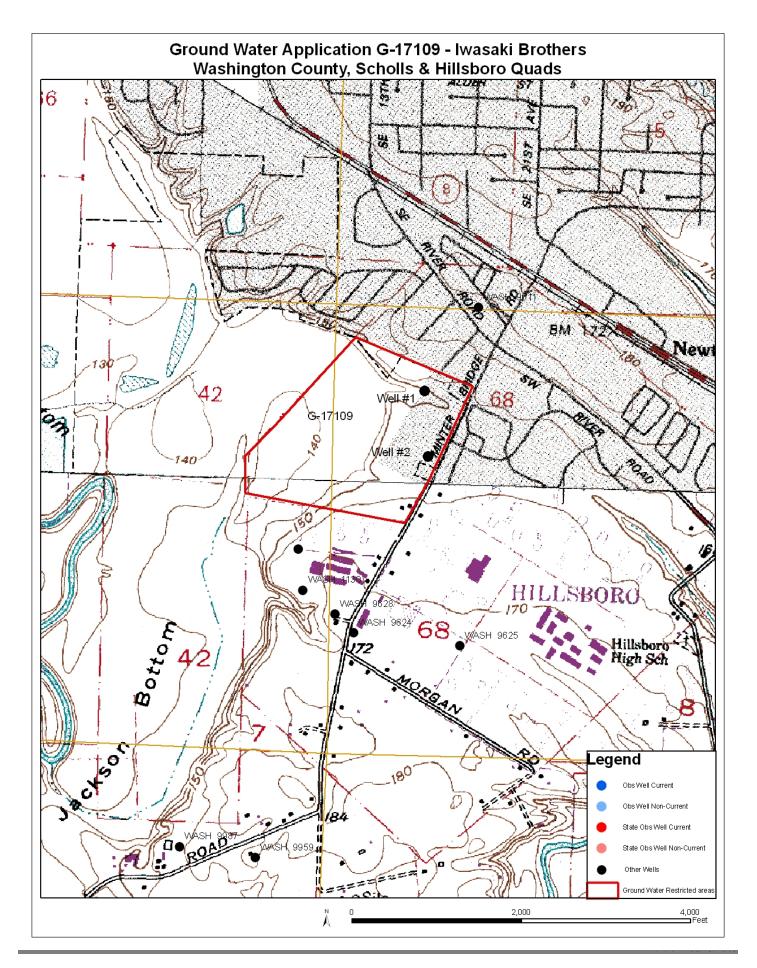
	istributed													
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
		%	%	%	%	%	%	%	%	%	%	%	%	
Well Q	as CFS													
Interfer	ence CFS													
Distrib	Distributed Wells													
Distric														
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
		%	%	%	%	%	%	%	%	%	%	%	%	
Well Q														
Interfer	ence CFS													
		%	%	%	%	%	%	%	%	%	%	%	%	
Well Q	as CFS													
Interfer	ence CFS													
		%	%	%	%	%	%	%	%	%	%	%	%	
Well Q														
Interfer	ence CFS													
		%	%	%	%	%	%	%	%	%	%	%	%	
Well Q	as CFS													
Interfer	ence CFS													
		%	%	%	%	%	%	%	%	%	%	%	%	
Well Q	as CFS													
Interfer	ence CFS													
		%	%	%	%	%	%	%	%	%	%	%	%	
Well Q	as CFS													
Interfer	ence CFS													
$(\Lambda) = T_0$	tal Interf.													
	% Nat. Q													
(C) = 1	% Nat. Q													
$(\mathbf{D}) = (\mathbf{A})$	(C) > (C)	\sim	\sim	\sim	\sim	\checkmark	\checkmark	\checkmark	\sim	\sim	\checkmark	\sim	\checkmark	
(E) = (A	/ B) x 100	%	%	%	%	%	%	%	%	%	%	%	%	

	terference as CFS; (B) = WAB calculated natural flow at 80% exceed. as CFS; (C) = 1% of calculated natural flow at 80% exceed highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage for impact evaluation:
Dasis	
	09-040 (5) (b) The potential to impair or detrimentally affect the public interest is to be determined by the W Rights Section.
If F unc	properly conditioned , the surface water source(s) can be adequately protected from interference, and/or ground water this permit can be regulated if it is found to substantially interfere with surface water: i. \Box The permit should contain condition #(s)
	ii. The permit should contain special condition(s) as indicated in "Remarks" below;
SW / G	W Remarks and Conditions
Referei	nces Used: <u>See conceptual model discussion for more details.</u>
	and Caldwell, 1998, Geologic Framework of the Willamette Lowland Aquifer System, Oregon and Washington, US ional Paper 1424-A
	ard, Gannett and Vaccaro, 1998, Hydrogeologic Framework of the Willamette Lowland Aquifer System, Oregon and gton, USGS Professional Paper 1424-B
	William 1062 Selected Analytical Matheda for Well and Assiftan Evolution. Dullatin 40 Illinois State Water
	William, 1962, Selected Analytical Methods for Well and Aquifer Evaluation, Bulletin 49, Illinois State Water ces.
Resourc	

Con	lon and Others, 2005, Ground-Water Hydrology of the Willamette Basin, Oregon, Scientific Report 2005-5168, USGS.
D. <u>WE</u>	LL CONSTRUCTION, OAR 690-200
D1.	Well #: Logid:
D2.	THE WELL does not meet current well construction standards based upon: a. review of the well log; b. field inspection by; c. report of CWRE; d. other: (specify);
D3.	THE WELL construction deficiency: a. constitutes a health threat under Division 200 rules; b. commingles water from more than one ground water reservoir; c. permits the loss of artesian head; d. permits the de-watering of one or more ground water reservoirs; e. other: (specify)
D4.	THE WELL construction deficiency is described as follows:
D6.	THE WELL a. was, or was not constructed according to the standards in effect at the time of original construction or most recent modification. b. I don't know if it met standards at the time of construction. Route to the Enforcement Section. I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Enforcement Section and the Ground Water Section.
THIS S	ECTION TO BE COMPLETED BY ENFORCEMENT PERSONNEL
D7.	Well construction deficiency has been corrected by the following actions:
	, 200,
D8. 🗌	(Enforcement Section Signature) Route to Water Rights Section (attach well reconstruction logs to this page).

Application G-17109_____continued

Date_____November 20, 2008



Detailed Reports for Watershed ID #30201013

TUALATIN R> WILLAMETTE R- AT GAGE 14206500 WILLAMETTE BASIN

Water Availability as of 11/20/2008

Watershed ID #: 30201013 Date: 11/20/2008 Exceedance Level:

Time: 10:34 AM

Water Availability Calculation

Monthly Streamflows in Cubic Feet per Second Storage at 50% Exceedance in Acre-Feet

Month	Natural Stream Flow	Consumptive Use and Storage	Expected Stream Flow	Reserved Stream Flow	Instream Requirement	Net Water Available
Jan	1,090.00	500.00	590.00	0.00	100.00	490.00
Feb	1,420.00	563.00	857.00	0.00	100.00	757.00
Mar	1,140.00	424.00	716.00	0.00	100.00	616.00
Apr	676.00	324.00	352.00	0.00	100.00	252.00
May	332.00	268.00	63.80	0.00	100.00	-36.20
Jun	179.00	297.00	-118.00	0.00	100.00	-218.00
Jul	80.90	329.00	-248.00	0.00	100.00	-348.00
Aug	44.30	312.00	-268.00	0.00	100.00	-368.00
Sep	54.20	267.00	-213.00	0.00	94.50	-307.00
Oct	69.40	151.00	-82.00	0.00	100.00	-182.00
Nov	160.00	258.00	-97.90	0.00	100.00	-198.00
Dec	758.00	483.00	275.00	0.00	100.00	175.00

Detailed Report of Instream Requirements Instream Requirements in Cubic Feet per Second

Арр	lication #	Status	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
	IS73538C	CERTIFICATE	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	94.50	100.00	100.00	100.00
	IS73539A	CERTIFICATE	75.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00	75.00
	IS73540A	CERTIFICATE	25.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00
	IS73541A	CERTIFICATE	30.00	30.00	30.00	30.00	30.00	30.00	30.00	30.00	30.00	30.00	30.00	30.00
	S86704A	PFO	10.40	10.40	10.40	10.40	10.40	10.40	10.40	10.40	10.40	10.40	10.40	10.40
	Maximum		100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	94.50	100.00	100.00	100.00

November 20, 2008 Date

Conceptual Model -- Generalized Ground Water Flow Systems. Marc Norton

January 8, 2004

Based on:

OWRD GRID - Ground water Resource Information Distribution

OWRD Ground Water Database

Memo on Recommended Vertical Hydraulic Conductivity Values for the Willamette Silt Hydrogeologic Unit When Using the Hunt Analytical Model, Karl Wozniak, January 6, 2004.

Ground-Water Resources of the Willamette Valley, Oregon, 1942, Water-Supply Paper 890, Piper.

Hydrogeologic Framework of the Willamette Lowland Aquifer System, Oregon and Washington, 1998, US Geological Survey Professional Paper 1424 B, Woodward, Gannett, and Vaccaro.

GENERALIZED GEOLOGY

The Willamette Lowland in Oregon and Washington encompasses 3,700 square mile and includes the low-lying parts of the Willamette Valley in Oregon and most of Clark county in Washington. About 70% of the population of Oregon and Clark County reside in the lowlands. The lowland is 145 miles long and averages 10 to 15 miles in width. Water is recharged to the Willamette Lowland aquifer system primarily through the direct infiltration of precipitation on the lowland. The regional water-table map shows an overall pattern of groundwater flow to the major streams, indicating that the base flow of these streams is sustained by ground water discharge. This ground-water discharge fully supports the base flow of streams that head in the lowland and partially support the base flow of the other streams.

HYDROGEOLOGIC UNITS

The aquifer system is composed of five hydrogeologic units, from oldest to youngest:

- 1) the basement confining unit,
- 2) the Columbia River basalt aquifer,
- 3) the Willamette confining unit,
- 4) the Willamette aquifer, and
- 5) the Willamette silt unit.

The basement-confining unit forms the lateral and basal boundary to the Willamette aquifer system. The basement-confining unit includes all the stratigraphic units that underlie either the Columbia River Basalt Group in the northern part of the basin or the basin-fill deposits in the southern part. The unit is composed of marine sedimentary rocks and volcanic rocks of the Coast and Cascade ranges. The basement-confining unit is generally a low yielding aquifer where wells develop water primarily from fractures in the rock. Ground water can be found under unconfined conditions in the highlands and under confined conditions with greater depth and lower elevations. Yields are generally less than 10 gpm and usually decrease over time. The deeper the well, the greater the chance of brackish water being encountered.

The Columbia River basalt aquifer overlies the basement-confining unit and consists of layers of basalt flows of the Columbia River Basalt Group. The thickness of the aquifer generally is several hundred feet but locally is as much as 1000 feet. Ground water in the basalts is generally under confined conditions except in the foothills where they may be unconfined. Well yields vary from tens to hundreds of gallons per minutes. Brackish water has been encountered in several areas, particularly with depth.

The Willamette confining unit consists primarily of fine-grained, distal alluvial fan and low-gradient stream deposits. The fine-grained deposits are considered a regional confining unit because of their wide spread occurrence and low permeability. Ground water in the Willamette confining unit is generally under confined conditions and well yields are very low to "dry".

The Willamette aquifer consists primarily of coarse-grained proximal alluvial-fan and braided-stream deposits. The greatest thickness, and coarsest materials of the Willamette aquifer outside of the Portland Basin occur in six major alluvial fans that were deposited where major streams from the Cascade Range enter the Willamette Lowland. Ground water in the Willamette aquifer unit varies from unconfined to confined conditions, depending on location and depth. Vertical gradients are usually downward except near major streams. Deposits of lower permeable material can act as a confining layer but are generally of limited aerial extent.

The Willamette silt unit is deposited throughout much of the Willamette Lowland by glacial-outburst floods. The deposits range in thickness from 0 to 130 feet. They consist primarily of silt and fine sand of relatively uniform lithology. Ground water in the Willamette silt unit is generally under unconfined conditions and well yields are low, less than 5 to 10 gpm.

STRUCTURAL BASINS

Outcrops of folded and faulted basalt within the Willamette Valley divide the lowland into four separate areas or structural basins -- from north to south, **the Portland Basin, the Tualatin Basin, the central Willamette Valley, and the southern Willamette valley**. Each of these areas has decidedly different hydrologic and hydrogeologic properties. The aquifer system in each basin, although hydraulically connected through a series of restrictive water gaps, is distinctive.

<u>Tualatin Basin</u>. The Columbia River basalt aquifer and the Willamette confining unit are the only regional hydrogeologic units above the basement-confining unit in the Tualatin Basin. The Columbia River basalt aquifer underlies the entire basin, and its upper surface forms a sediment-filled bowl-like depression.

<u>The Central Willamette Valley</u> All five of the hydrogeologic units occur in the central Willamette Valley. The Columbia River basalt aquifer underlies the entire central Willamette Valley, except for small areas along the far eastern margin. A number of faults have been mapped in the central Willamette Valley, some of which offset the aquifer, and numerous other faults have been mapped in the uplands surrounding the basin where the aquifer crops out. The Willamette aquifer in the central Willamette Valley contains three major alluvial fans -- the Salem fan, the Molalla fan, and the Canby fan. The Willamette Silt unit overlies most of the central valley with a maximum thickness of about 130 feet near the center and thins towards the south and near the margins of the basin.

<u>The Southern Willamette Valley</u> In the southern Willamette Valley, all of the regional hydrogeologic units are present; however, the Columbia River basalt aquifer occurs only in the Stayton area. The Willamette confining unit is thinner in the southern Willamette Valley than elsewhere in the Willamette Lowland. The Willamette aquifer contains the Lebanon fan and the Stayton fan. The Willamette aquifer is much thinner (averaging only about 20 to 40 feet thick) between the alluvial fans of the southern Willamette Valley. The Willamette Silt unit covers most of the southern Willamette Valley and generally thin towards the south.