### PUBLIC INTEREST REVIEW FOR GROUND WATER APPLICATIONS

TO:		Water	Rights S	ection				Date	e August	14, 2009		
FROM	<b>I</b> :	Groun	nd Water/	Hydrology	Section _		Norton					
SUBJE	ECT:	Appli	cation G-	17244			ewer's Name persedes re	view of				
		11	•							Date of Re	view(s)	
OAR 6 welfare to deter	90-310-1 e, safety ar rmine who	30 (1) 7 and healt ther the	The Depart th as descr e presumpt	ribed in ORS tion is establ	resume the 537.525. ished. OA	at a propos Departmen R 690-310-	red groundwe t staff reviev 140 allows t	v ground wat the proposed	ensure the pre- er applications use be modific icies in place a	under OA	AR 690-3 itioned to	10-140 meet
A. <u>GE</u>	NERAL	INFO	RMATIO	<u>ON</u> : A	pplicant's	Name:	James Pie	rce		County:_	Yamhi	1
A1.	Applica	nt(s) se	ek(s) <u><b>0.0</b></u>	4 cfs froi	m <u>1</u>	well	(s) in the	Willamette	e River			_Basin,
		Spring 1	Brook			subb	asin Qu	ad Map: <u>N</u>	ewberg			
A2. A3.	Propose Well an	ed use: _ d aquife	Nu er data (att	rsery (11.3 tach and nu	acres) mber logs	Seas	sonality:	March 1 -	October 31 I wells as such	under lo	gid):	
Wel l	Log	id	Applican s Well #	Pro Ac	Proposed Aquifer*		Proposed Rate(cfs) (T/		Locatio 2250'	Location, metes and bounds, e.g. 2250' N, 1200' E fr NW cor S 36		
1 2	YAMH	54107	1	C	RBG	0.04	03S/0	2W-22 SE N	(W 650' S,	920' E fr	SE cor D	LC 51
3												
5												
* Alluvi	ium, CRB,	Bedrock	(			•	•					
Well	Well Elev ft msl	First Water ft bls	I II his	SWL Date 06/08/05	Well Depth (ft)	Seal Interval (ft) 0 - 96	Casing Intervals (ft) +1 - 142	Liner Intervals (ft)	Perforations Or Screens (ft) 122 - 142	Well Yield (gpm) 120	Draw Down (ft)	Test Type
	233	71	71	00/00/05	172	0-70	11-142		122 - 142	120		All
Use data	a from app	lication 1	for proposed	d wells.								
A4.	Commo	ents: <u>Se</u>	e concept	ual model d	iscussion	for more d	etails on ge	ology and gr	round water.			
Reques	sted disch	narge ra	ate is 20 g	pm = 0.04 c	fs.							
A5. 🖂	manage (Not all Comme	ment of basin r nts:	ground wules contain The well	in such provi	ically conr isions.) velop wate	nected to su er from an	rface water	are, or	o the developn <b>I are not</b> , action ore this portion	vated by t	his appli	cation.
A6. 🗌	. ,	f admin	istrative a	rea: NA					er limited by ar			

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### B. GROUND WATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070

a.	ed upon available data, I have determined that ground water* for the proposed use:
	is over appropriated, is not over appropriated, or is cannot be determined to be over appropriated during any period of the proposed use. * This finding is limited to the ground water portion of the over-appropriation determination as prescribed in OAR 690-310-130;
b.	will not <i>or</i> will likely be available in the amounts requested without injury to prior water rights. * This finding is limited to the ground water portion of the injury determination as prescribed in OAR 690-310-130;
c.	$\square$ will not or $\square$ will likely to be available within the capacity of the ground water resource; or
d.	will, if properly conditioned, avoid injury to existing ground water rights or to the ground water resource:  i. The permit should contain condition #(s)
a.	Condition to allow ground water production from no deeper than ft. below land surface;
b.	Condition to allow ground water production from no shallower than ft. below land surface;
c.	Condition to allow ground water production only from the water reservoir between approximately ft. and ft. below land surface;
	water reservoir between approximatery it. and it. below faild surface,
	by the Ground Water Section. <b>Describe injury</b> —as related to water availability— that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc):
	ound water availability remarks: The well is outside of two ground water limited areas. Water levels in nearby
	ound water availability remarks: The well is outside of two ground water limited areas. Water levels in nearby is that are similar elevation are not indicating overdraft at this time.

#### C. GROUND WATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. **690-09-040** (1): Evaluation of aquifer confinement:

Wel 1	Aquifer or Proposed Aquifer	Confined	Unconfined
1	CRBG		$\boxtimes$

Basis for aquifer confinement evaluation: The water level in the well is where it was encountered during drilling.

C2. **690-09-040 (2) (3):** Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¼ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	GW Elev ft msl	SW Elev ft msl	Distance (ft)	Hydraulically Connected? YES NO ASSUMED	Potential for Subst. Interfer. Assumed? YES NO
1	1	Un-Named trib. to Spring Bk.	210	200	1500		
	2	Spring Brook		120	2700		

Basis for aquifer hydraulic connection evaluation: <u>Ground water levels are above nearby streams and well develop</u> water from an unconfined aquifer.

Water Availability Basin the well(s) are located within: WILLAMETTE R > COLUMBIA R - AB MOLALLA R

C3a. **690-09-040 (4):** Evaluation of stream impacts for <u>each well</u> that has been determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that surface water source, and not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% *natural* flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < 1/4 mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
									< 25 %	

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C3b. **690-09-040 (4):** Evaluation of stream impacts <u>by total appropriation</u> for all wells determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. **Complete only if Q is distributed among wells**. Otherwise same evaluation and limitations apply as in C3a above.

SW #	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?

<b>Comments:</b>	The well is over 1/4 mile from the closest stream and the natural flow of the Willamette River far exceeds
the requested	l amount of water.

C4a. **690-09-040 (5):** Estimated impacts on **hydraulically connected surface water sources greater than one mile** as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

	istributed	Wells											
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
Interfer	ence CFS												
Distril	buted Well	ls											
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
Interfer	rence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
Interfer	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well O	as CFS												
	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well O	as CFS												
í	rence CFS												
						· '			I				
$(\mathbf{A}) = \mathbf{T}\mathbf{c}$	otal Interf.												
(B) = 80	% Nat. Q												
(C) = 1	% Nat. Q												
( <b>D</b> ) = (A	<b>A</b> ) > (C)	<b>√</b>	√	<b>√</b>	<b>√</b>								
$(\mathbf{E}) = (\mathbf{A}$	( / B) x 100	%	%	%	%	%	%	%	%	%	%	%	%

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CFS; (D) = highlight the check	mark for each month where (A) is g	v at 80% exceed. as CFS; (C) = 1% of calculated greater than (C); (E) = total interference divided by	
545 <b>600 00 040 (5)</b> (5)	The petential to impair or do	tuimentally effect the public interest is to be	no determined by the Weste
C4b. 690-09-040 (5) (b) Rights Section.	The potential to impair or de	trimentally affect the public interest is to b	e determined by the wate
under this permit ca	n be regulated if it is found to su	s) can be adequately protected from interferent substantially interfere with surface water: s)ition(s) as indicated in "Remarks" below;	•
C6. SW / GW Remarks an	d Conditions		
References Used: Sec	e conceptual model discussion	for more details.	
Gannett and Caldwell, 1 Professional Paper 1424		e Willamette Lowland Aquifer System, Oreg	on and Washington, USGS
Woodward, Gannett and Washington, USGS Pro		Framework of the Willamette Lowland Aqu	ifer System, Oregon and
Walton, William, 1962, Resources.	Selected Analytical Methods for	r Well and Aquifer Evaluation, Bulletin 49, I	llinois State Water
Freeze and Cherry, 1979	, Groundwater, Prentice-Hall, In	nc.	

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9	Conlon and Others,	2005, Ground-Water Hydrology of the	Willamette Basin, Oregon, Scientific Repo	ort 2005-5168, USGS.
D. <u>V</u>	VELL CONSTRU	<u>UCTION, OAR 690-200</u>		
D1.	Well #:	Logid:		
D2.	<ul><li>a.  review</li><li>b.  field ir</li></ul>	oes not meet current well construction of the well log; aspection byof CWRE	n standards based upon:	
D3.	a. constit b. commi c. permit d. permit	onstruction deficiency: utes a health threat under Division 200 ingles water from more than one ground is the loss of artesian head; s the de-watering of one or more ground (specify)	water reservoir;  I water reservoirs;	
D4.	THE WELL co	onstruction deficiency is described as	follows:	
D5.	THE WELL	a. was, or was not construction or mo	acted according to the standards in effect a st recent modification.	t the time of
		b. I don't know if it met stand	lards at the time of construction.	
D6.			chholding issuance of the permit until evid cement Section and the Ground Water Sec	
THI	S SECTION TO	BE COMPLETED BY ENFORCE	EMENT PERSONNEL	
D7.	☐ Well construction	on deficiency has been corrected by the	following actions:	

D8. 

Route to Water Rights Section (attach well reconstruction logs to this page).

(Enforcement Section Signature)

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Duic	11ugust 14, 2007

## Water Availability Analysis

# **Detailed Reports**

# WILLAMETTE R > COLUMBIA R - AB MOLALLA R WILLAMETTE BASIN

Water Availability as of 8/14/2009

Watershed ID #: 182

Exceedance Level:

80%

Date: 8/14/2009

Time: 2:43 PM

Water Availability Calculation	Consumptive Uses and Storages	Instream Flow Requirements	Re <u>s</u> ervations	Water Rights	

Watershed Characteristics

### **Water Availability Calculation**

Monthly Streamflows in Cubic Feet per Second Storage at 50% Exceedance in Acre-Feet

Mont h	Natural Stream Flow	Consumptive Uses and Storages	Expected Stream Flow	Reserved Stream Flow	Instream Flow Requirement	Net Water Available
JAN	21,400.00	2,250.00	19,100.00	0.00	1,500.00	17,600.00
FEB	23,200.00	7,440.00	15,800.00	0.00	1,500.00	14,300.00
MAR	22,400.00	7,220.00	15,200.00	0.00	1,500.00	13,700.00
APR	19,900.00	6,870.00	13,000.00	0.00	1,500.00	11,500.00
MAY	16,600.00	4,200.00	12,400.00	0.00	1,500.00	10,900.00
JUN	8,740.00	2,050.00	6,690.00	0.00	1,500.00	5,190.00
JUL	4,980.00	1,870.00	3,110.00	0.00	1,500.00	1,610.00
AUG	3,830.00	1,720.00	2,110.00	0.00	1,500.00	614.00
SEP	3,890.00	1,470.00	2,420.00	0.00	1,500.00	918.00
OCT	4,850.00	717.00	4,130.00	0.00	1,500.00	2,630.00
NOV	10,200.00	851.00	9,350.00	0.00	1,500.00	7,850.00
DEC	19,300.00	924.00	18,400.00	0.00	1,500.00	16,900.00

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Conceptual Model -- Generalized Ground Water Flow Systems. Marc Norton January 8, 2004

Based on:

OWRD GRID - Ground water Resource Information Distribution

OWRD Ground Water Database

Memo on Recommended Vertical Hydraulic Conductivity Values for the Willamette Silt Hydrogeologic Unit When Using the Hunt Analytical Model, Karl Wozniak, January 6, 2004.

Ground-Water Resources of the Willamette Valley, Oregon, 1942, Water-Supply Paper 890, Piper.

Hydrogeologic Framework of the Willamette Lowland Aquifer System, Oregon and Washington, 1998, US Geological Survey Professional Paper 1424 B, Woodward, Gannett, and Vaccaro.

### **GENERALIZED GEOLOGY**

The Willamette Lowland in Oregon and Washington encompasses 3,700 square mile and includes the low-lying parts of the Willamette Valley in Oregon and most of Clark county in Washington. About 70% of the population of Oregon and Clark County reside in the lowlands. The lowland is 145 miles long and averages 10 to 15 miles in width. Water is recharged to the Willamette Lowland aquifer system primarily through the direct infiltration of precipitation on the lowland. The regional water-table map shows an overall pattern of groundwater flow to the major streams, indicating that the base flow of these streams is sustained by ground water discharge. This ground-water discharge fully supports the base flow of streams that head in the lowland and partially support the base flow of the other streams.

### **HYDROGEOLOGIC UNITS**

The aquifer system is composed of five hydrogeologic units, from oldest to youngest:

- 1) the basement confining unit,
- 2) the Columbia River basalt aquifer,
- 3) the Willamette confining unit,
- 4) the Willamette aquifer, and
- 5) the Willamette silt unit.

The basement-confining unit forms the lateral and basal boundary to the Willamette aquifer system. The basement-confining unit includes all the stratigraphic units that underlie either the Columbia River Basalt Group in the northern part of the basin or the basin-fill deposits in the southern part. The unit is composed of marine sedimentary rocks and volcanic rocks of the Coast and Cascade ranges. The basement-confining unit is generally a low yielding aquifer where wells develop water primarily from fractures in the rock. Ground water can be found under unconfined conditions in the highlands and under confined conditions with greater depth and lower elevations. Yields are generally less than 10 gpm and usually decrease over time. The deeper the well, the greater the chance of brackish water being encountered.

The Columbia River basalt aquifer overlies the basement-confining unit and consists of layers of basalt flows of the Columbia River Basalt Group. The thickness of the aquifer generally is several hundred feet but locally is as much as 1000 feet. Ground water in the basalts is generally under confined conditions except in the foot-

hills where they may be unconfined. Well yields vary from tens to hundreds of gallons per minutes. Brackish water has been encountered in several areas, particularly with depth.

The Willamette confining unit consists primarily of fine-grained, distal alluvial fan and low-gradient stream deposits. The fine-grained deposits are considered a regional confining unit because of their wide spread occurrence and low permeability. Ground water in the Willamette confining unit is generally under confined conditions and well yields are very low to "dry".

The Willamette aquifer consists primarily of coarse-grained proximal alluvial-fan and braided-stream deposits. The greatest thickness, and coarsest materials of the Willamette aquifer outside of the Portland Basin occur in six major alluvial fans that were deposited where major streams from the Cascade Range enter the Willamette Lowland. Ground water in the Willamette aquifer unit varies from unconfined to confined conditions, depending on location and depth. Vertical gradients are usually downward except near major streams. Deposits of lower permeable material can act as a confining layer but are generally of limited aerial extent.

The Willamette silt unit is deposited throughout much of the Willamette Lowland by glacial-outburst floods. The deposits range in thickness from 0 to 130 feet. They consist primarily of silt and fine sand of relatively uniform lithology. Ground water in the Willamette silt unit is generally under unconfined conditions and well yields are low, less than 5 to 10 gpm.

### **STRUCTURAL BASINS**

Outcrops of folded and faulted basalt within the Willamette Valley divide the lowland into four separate areas or structural basins -- from north to south, **the Portland Basin**, **the Tualatin Basin**, **the central Willamette Valley**, **and the southern Willamette valley**. Each of these areas has decidedly different hydrologic and hydrogeologic properties. The aquifer system in each basin, although hydraulically connected through a series of restrictive water gaps, is distinctive.

<u>Tualatin Basin.</u> The Columbia River basalt aquifer and the Willamette confining unit are the only regional hydrogeologic units above the basement-confining unit in the Tualatin Basin. The Columbia River basalt aquifer underlies the entire basin, and its upper surface forms a sediment-filled bowl-like depression.

The Central Willamette Valley All five of the hydrogeologic units occur in the central Willamette Valley. The Columbia River basalt aquifer underlies the entire central Willamette Valley, except for small areas along the far eastern margin. A number of faults have been mapped in the central Willamette Valley, some of which offset the aquifer, and numerous other faults have been mapped in the uplands surrounding the basin where the aquifer crops out. The Willamette aquifer in the central Willamette Valley contains three major alluvial fans -- the Salem fan, the Molalla fan, and the Canby fan. The Willamette Silt unit overlies most of the central valley with a maximum thickness of about 130 feet near the center and thins towards the south and near the margins of the basin.

<u>The Southern Willamette Valley</u> In the southern Willamette Valley, all of the regional hydrogeologic units are present; however, the Columbia River basalt aquifer occurs only in the Stayton area. The Willamette confining unit is thinner in the southern Willamette Valley than elsewhere in the Willamette Lowland. The Willamette aquifer contains the Lebanon fan and the Stayton fan. The Willamette aquifer is much thinner (averaging only about 20 to 40 feet thick) between the alluvial fans of the southern Willamette Valley. The Willamette Silt unit covers most of the southern Willamette Valley and generally thin towards the south.