WATER RESOURCES DEPARTMENT

MEN	10							Ang	just s	14,	20/0/10
TO: FROM	M: ÆCT:	GW:	J 63	h H	91 Re Cackett Name) terferen						
	_YES _NO	The so	ource of	approp	riation i	s within	or abov	ve a Sce	nic Wa	terway	
	_YES	Use th	e Scenie	c Water	way cor	ndition (Conditi	on 7J)			
	interfection interfection interfection that the period interfection in the period in t	erence wated into a service was 390. Erence was epartmente prop	with surfice rene 835, the with surfice of us	Ground ace water Ground ace water to will me	d Water er that coributed d Water er that confind the ree-flow	ontribut below. Section ontribut at ther bly red	is unal tes to a s e is a pu uce the	Scenic Vole to cascenic weeponde	Waterwallculate vaterwalerance (e water	ground y; there of evide flows	water
Calcula calcula informin Exerci Watery	ite the per ted, per c ng Water se of th way by	rcentage riteria in Rights th is permi the follo	390.835, at the De t is calc	iptive use do not fil partment ulated t nounts	CE by mont. If in the to is unable o reduce expresse	able but c to make e month	heck the a Prepon ly flows	"unable" derance (s in	option a of Eviden	bove, thu ce finding	s g. Scenic
Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec

PUBLIC INTEREST REVIEW FOR GROUND WATER APPLICATIONS

TO:		Water	Rights S	ection				Date	e Au	gust 2	24, 2010		
FROM	:	Groun	d Water/	Hydrology	Section _								
SUBJE	CT:	Applie	cation G-	17291			ewer's Name persedes re	view of	De		er 9, 200 Date of Re		
OAR 69 welfare, to deter	90-310-1 safety and mine who umption	30 (1) T and healt ether the criteria.	The Depart h as descr presumpt	ibed in ORS ion is establi ew is based	resume th 537.525, shed. OA upon ava	at a propos Department R 690-310- ilable infor	ed groundwa t staff review 140 allows th mation and	ater use will ground wate ne proposed agency poli neta	er applica use be ma icies in p	e prese ations u odified lace at	ervation of under OA or condi	of the pub R 690-31 tioned to of evalu	10-140 meet
													Basin,
A1.			om River	CIS IFOI				illamette Riv ad Map:V				_	_ Dasiii,
A2. A3.	Propose	ed use: _	M ₁	ınicipal		Seas	sonality:	Year-roun	d	such 1	ınder log	gid):	
Well	Logi	id	Applican Well #		oposed quifer*	Propos Rate(c		Location			n, metes N, 1200' E		
1	LAN		12		luvium	0.5		/R-S QQ-Q) 5W-30 SE N			, 1751' E		
2 3	68919)**											
4													
5 * Alluvi	um, CRB,	Bedrock	:										
Well	Well Elev ft msl	First Water ft bls	SWL ft bls	SWL Date	Well Depth (ft)	Seal Interval (ft)	Casing Intervals (ft)	Liner Intervals (ft)	Perfora Or Sci	eens	Well Yield (gpm)	Draw Down (ft)	Test Type
12	417	74	74	07/31/2008	160	0-27	+2 - 82 152 - 160	(11)	80-100, 111, 111 131-152	00-	223	24.4	P
A4.	• • •	ents: <u>**</u>		t submitted			_	See conceptu					tails on
A5. 🛚	manage (Not all Comme	ment of basin rents:	ground wales contains The applications	n such provi	cally com sions.) develops	nected to sur water from	rface water n an unconfi	ales relative t are, or ined aquifer apply.	are no	t, activ	ated by th	nis applic than ¼ n	ation. nile
A6. 🗌	Well(s) Name of Comme	# of admin ents:	istrative a	rea: NA		,	, ta	p(s) an aquit	fer limite	d by an	administ	trative re	striction.

Version: 08/15/2003

pplic	ation (G- <u>17291_2</u>	continued	Date	August 24, 2010
. <u>GR</u>	ROUN	ND WATER AVAII	LABILITY CONSIDERATIONS	, OAR 690-310-130, 4	<u>00-010, 410-0070</u>
1.	Bas	sed upon available da	ta, I have determined that ground wate	<u>r</u> * for the proposed use:	
	a.	period of the pro	ted, is not over appropriated, or posed use. * This finding is limited to prescribed in OAR 690-310-130;	cannot be determined the ground water portion	to be over appropriated during any of the over-appropriation
	b.		vill likely be available in the amounts reground water portion of the injury		
	c.	☐ will not or ☐ v	vill likely to be available within the cap	pacity of the ground water	resource; or
	d.	i. ⊠ The per moniton ii. □ The per	conditioned, avoid injury to existing mit should contain condition #(s)	B – Interference, 7N – A	nnual WL, 7P - Well Tag, + large
2.	a.	Condition to all	ow ground water production from no d	eeper than	ft. below land surface;
	b.	Condition to all	ow ground water production from no s	hallower than	ft. below land surface;
	c.	Condition to allowater reservoir b	ow ground water production only from etween approximately ft.	the ft. below	ground y land surface;
	d.	occur with this u issuance of the p Water Section. Describe injury -	tion is necessary to accomplish one or se and without reconstructing are cited ermit until evidence of well reconstruc as related to water availability—that is	below. Without reconstruction is filed with the Department of the	uction, I recommend withholding artment and approved by the Ground ell reconstruction (interference w/
		semor water rights,	not within the capacity of the resource	, etc).	
3.	ma	terial ground water s	ty remarks: <u>Wells in the area deve</u> ystem. Surface water and ground w	ater are hydraulically co	onnected in this environment.
	Ver dov	neta at well #4 (LAN) wnward trend (See at ombination of both.	on, long term supplies should be related 13505), #9 (LANE 2340), #10 (LANE tached graph). This could be related to its very important for the City of V	NE 58439), and #11 (LAN I to climate trends, the a eneta to collect good qu	NE 68918) show a slight mount of water being pumped, or ality water levels on all of their
			ource. Interference with nearby user without spending considerable time leading to the leading t		t is impossible to predict if
	_				

C. GROUND WATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. **690-09-040** (1): Evaluation of aquifer confinement:

Well	Aquifer or Proposed Aquifer	Confined	Unconfined
12	Younger Alluvial (sand and gravel)		

Basis for aquifer confinement evaluation: The sand and gravel aquifer is unconfined in this area because the water level is below the overlying clay layer.

C2. **690-09-040 (2) (3):** Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¼ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	GW Elev ft msl	SW Elev ft msl	Distance (ft)	Hydraulically Connected? YES NO ASSUMED	Potential for Subst. Interfer. Assumed? YES NO
12	1	Un-Named Trib to Fern Ridge	350	374	1450		
12	2	Un-Named Trib to Fern Ridge	350	374	3100		
12	3	Long Tom River	350	374	4640		
12	4	Fern Ridge Reservoir	350	374*	3600		

Basis for aquifer hydraulic connection evaluation: *The water level listed for Fern Ridge is the maximum stage level. Stage levels vary through the year. The ground water listed on the well log for well #12 is considerably lower than the water level measured for well #4 nearby. Using the water level for well #4, well #12 water levels would be above the streams.

Water Availability Basin the well(s) are located within: 114: LONG TOM R > WILLAMETTE R - AB MOUTH

C3a. 690-09-040 (4): Evaluation of stream impacts for each well that has been determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that surface water source, and not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% natural flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < ½ mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
12	3						32.1	\boxtimes	< 25%	\boxtimes
12	4	\boxtimes					32.1	\boxtimes	< 25%	
								1 -	_	
					=====		_			
									_	

C3b. 690-09-040 (4): Evaluation of stream impacts by total appropriation for all wells determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Complete only if Q is distributed among wells. Otherwise same evaluation and limitations apply as in C3a above.

Date

SW #	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?

The model does not work well with a lake rather than a stream and the location of the well in relation to the lake shore. The younger alluvial material is hydraulically connected to the lake and the Long Tom River. The upper clay tends to delay the impact.

C4a. 690-09-040 (5): Estimated impacts on hydraulically connected surface water sources greater than one mile as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

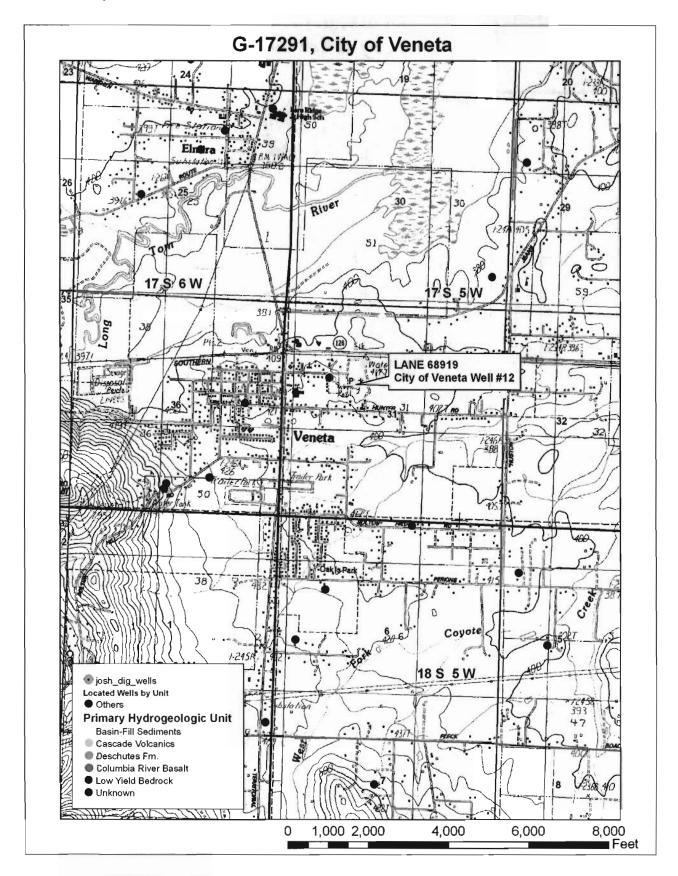
	stributed												
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	9/
Well Q a	is CFS												
Interfere	nce CFS												
			0.00										
	uted Well												
Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	<u>%</u> _	%	%
Well Q a													
Interfere	nce CFS												
		%	%	%	%	%	%	%_	%	%	%	%	%
Well Q a	is CFS												
Interfere	nce CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q a	is CFS												
Interfere	nce CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q a	as CFS												
Interfere	nce CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q a	as CFS			-									
Interfere	nce CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q a	as CFS												
Interfere	nce CFS												
(A) = Tot	al Interf.												
												_	
	% Nat. Q							_					
(C) = 1 %	6 Nat. Q												
(D) = (A)) > (C)		1	1	V	1	1	1	1	1	7	1	1
. , . ,	/ B) x 100	%	%	%	%	%	%	%	%	%	%	%	9/

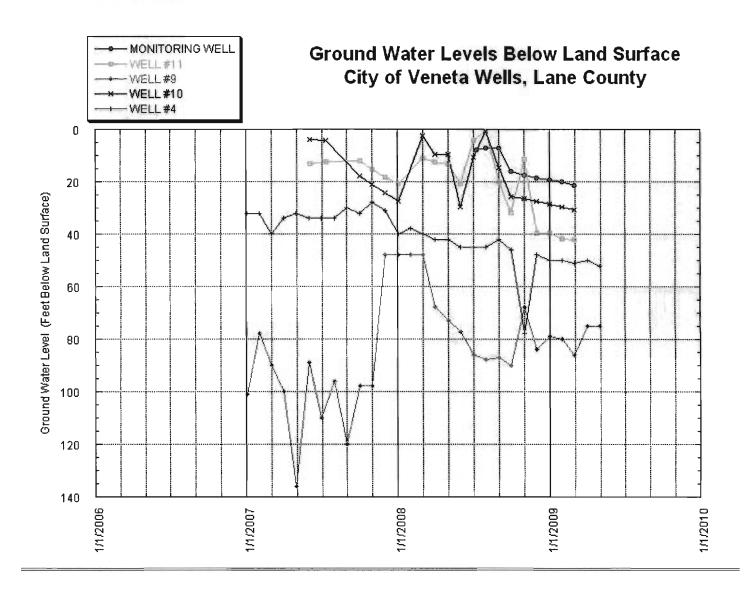
(A) = total interference as CFS; (B) = WAB calculated natural flow at 80% exceed, as CFS; (C) = 1% of calculated natural flow at 80% exceed, as CFS; (D) = highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage.

plication G-17291_2 continued	Date	August 24, 201
Basis for impact evaluation:		
basis for impact evaluation.		
_		
		17.7
-		
690-09-040 (5) (b) The potential to impair or detrimental Rights Section.	ly affect the public interest is to b	oe determined by the W
☐ If properly conditioned, the surface water source(s) can be as under this permit can be regulated if it is found to substantially i. ☐ The permit should contain condition #(s) ii. ☐ The permit should contain special condition(s) as	interfere with surface water:	ce, and/or ground water
ii. \(\) The permit should contain special condition(s) as	indicated in "Remarks" below;	
SW / GW Remarks and Conditions		
Para service process		
	-	
References Used: See conceptual model discussion for more of	details.	
Gannett and Caldwell, 1998, Geologic Framework of the Willamet Professional Paper 1424-A	te Lowland Aquifer System, Orego	n and Washington, USC
Woodward, Gannett and Vaccaro, 1998, Hydrogeologic Framewor Washington, USGS Professional Paper 1424-B	k of the Willamette Lowland Aqui	fer System, Oregon and
Walton, William, 1962, Selected Analytical Methods for Well and Resources.	Aguifer Evaluation, Bulletin 49, Il	linois State Water
Freeze and Cherry, 1979, Groundwater, Prentice-Hall, Inc.		
Conlon and Others, 2005, Ground-Water Hydrology of the Willam	ette Basin, Oregon, Scientific Repo	ort 2005-5168, USGS.
Frank, F. J., 1973, Ground Water in the Eugene-Springfied Area, S Water-Supply Paper 2018.	Southern Willamette Valley, Oregon	n, U.S. Geological Surve

Applic	cation <u>G-17291_2</u>	continued	Date	August 24, 2010
D. <u>W</u>]	ELL CONSTRUC	ΓΙΟΝ, OAR 690-200		
D1.	Well #:	Logid:		
D2.	a. review ofb. field inspect. report of 0	not meet current well construction standthe well log; ction by		
D3.	a.	ruction deficiency: s a health threat under Division 200 rules; es water from more than one ground water e loss of artesian head; e de-watering of one or more ground wate ecify)	r reservoirs;	
D4.		ruction deficiency is described as follow		
	1			
D5.	THE WELL	 a. was, or was not constructed a original construction or most received. b. I don't know if it met standards a orcement Section. I recommend withhold 	ent modification. at the time of construction.	
	is filed with the De	partment and approved by the Enforcement	nt Section and the Ground Water Se	ection.
THIS	S SECTION TO BI	E COMPLETED BY ENFORCEME	ENT PERSONNEL	
D7.	☐ Well construction of	deficiency has been corrected by the follow	ving actions:	
				, 200
	(Enforcen	nent Section Signature)		
D8.	Route to Water I	Rights Section (attach well reconstruction	on logs to this page).	

Well Location Map





Water Availability Tables

LONG TOM R > WILLAMETTE R - AB MOUTH WILLAMETTE BASIN

Water Availability as of 7/22/2009

Watershed ID #: 114

Exceedance Level:

Time: 3:04 PM

80%

Date: 7/22/2009

Water Availability Calculation | Consumptive Uses and Storages | Instream Flow Requirements | Reservations | Water Rights

Watershed Characteristics

Water Availability Calculation

Monthly Streamflows in Cubic Feet per Second Storage at 50% Exceedance in Acre-Feet

Mont h	Natural Stream Flow	Consumptive Uses and Storages	Expected Stream Flow	Reserved Stream Flow	Instream Flow Requirement	Net Water Available
JAN	568.00	149.00	419.00	0.00	0.00	419.00
FEB	697.00	388.00	309.00	0.00	0.00	309.00
MAR	596.00	555.00	40.90	0.00	0.00	40.90
APR	373.00	249.00	124.00	0.00	0.00	124.00
MAY	215.00	63.80	151.00	0.00	0.00	151.00
JUN	105.00	29.60	75.40	0.00	0.00	75.40
JUL	50.60	47.90	2.67	0.00	0.00	2.67
AUG	35.40	38.70	-3.28	0.00	0.00	-3.28
SEP	32.10	21.20	10.90	0.00	0.00	10.90
OCT	35.30	5.32	30.00	0.00	0.00	30.00
NOV	82.50	5.08	77.40	0.00	0.00	77.40
DEC	364.00	105.00	259.00	0.00	0.00	259.00

Application G-17291 2 continued

Date______August 24, 2010

Conceptual Model -- Generalized Ground Water Flow Systems. Marc Norton January 8, 2004

Based on:

OWRD GRID - Ground water Resource Information Distribution

OWRD Ground Water Database

Memo on Recommended Vertical Hydraulic Conductivity Values for the Willamette Silt Hydrogeologic Unit When Using the Hunt Analytical Model, Karl Wozniak, January 6, 2004.

Ground-Water Resources of the Willamette Valley, Oregon, 1942, Water-Supply Paper 890, Piper.

Hydrogeologic Framework of the Willamette Lowland Aquifer System, Oregon and Washington, 1998, US Geological Survey Professional Paper 1424 B, Woodward, Gannett, and Vaccaro.

GENERALIZED GEOLOGY

The Willamette Lowland in Oregon and Washington encompasses 3,700 square mile and includes the low-lying parts of the Willamette Valley in Oregon and most of Clark county in Washington. About 70% of the population of Oregon and Clark County reside in the lowlands. The lowland is 145 miles long and averages 10 to 15 miles in width. Water is recharged to the Willamette Lowland aquifer system primarily through the direct infiltration of precipitation on the lowland. The regional water-table map shows an overall pattern of groundwater flow to the major streams, indicating that the base flow of these streams is sustained by ground water discharge. This ground-water discharge fully supports the base flow of streams that head in the lowland and partially support the base flow of the other streams.

HYDROGEOLOGIC UNITS

The aquifer system is composed of five hydrogeologic units, from oldest to youngest:

- 1) the basement confining unit,
- 2) the Columbia River basalt aquifer,
- 3) the Willamette confining unit,
- 4) the Willamette aguifer, and
- 5) the Willamette silt unit.

The basement-confining unit forms the lateral and basal boundary to the Willamette aquifer system. The basement-confining unit includes all the stratigraphic units that underlie either the Columbia River Basalt Group in the northern part of the basin or the basin-fill deposits in the southern part. The unit is composed of marine sedimentary rocks and volcanic rocks of the Coast and Cascade ranges. The basement-confining unit is generally a low yielding aquifer where wells develop water primarily from fractures in the rock. Ground water can be found under unconfined conditions in the highlands and under confined conditions with greater depth and lower elevations. Yields are generally less than 10 gpm and usually decrease over time. The deeper the well, the greater the chance of brackish water being encountered.

The Columbia River basalt aquifer overlies the basement-confining unit and consists of layers of basalt flows of the Columbia River Basalt Group. The thickness of the aquifer generally is several hundred feet but locally is as much as 1000 feet. Ground water in the basalts is generally under confined conditions except in the foot-hills

continued

Date

where they may be unconfined. Well yields vary from tens to hundreds of gallons per minutes. Brackish water has been encountered in several areas, particularly with depth.

The Willamette confining unit consists primarily of fine-grained, distal alluvial fan and low-gradient stream deposits. The fine-grained deposits are considered a regional confining unit because of their wide spread occurrence and low permeability. Ground water in the Willamette confining unit is generally under confined conditions and well yields are very low to "dry".

The Willamette aquifer consists primarily of coarse-grained proximal alluvial-fan and braided-stream deposits. The greatest thickness, and coarsest materials of the Willamette aquifer outside of the Portland Basin occur in six major alluvial fans that were deposited where major streams from the Cascade Range enter the Willamette Lowland. Ground water in the Willamette aquifer unit varies from unconfined to confined conditions, depending on location and depth. Vertical gradients are usually downward except near major streams. Deposits of lower permeable material can act as a confining layer but are generally of limited aerial extent.

The Willamette silt unit is deposited throughout much of the Willamette Lowland by glacial-outburst floods. The deposits range in thickness from 0 to 130 feet. They consist primarily of silt and fine sand of relatively uniform lithology. Ground water in the Willamette silt unit is generally under unconfined conditions and well yields are low, less than 5 to 10 gpm.

STRUCTURAL BASINS

Outcrops of folded and faulted basalt within the Willamette Valley divide the lowland into four separate areas or structural basins -- from north to south, **the Portland Basin**, **the Tualatin Basin**, **the central Willamette Valley**, **and the southern Willamette valley**. Each of these areas has decidedly different hydrologic and hydrogeologic properties. The aquifer system in each basin, although hydraulically connected through a series of restrictive water gaps, is distinctive.

<u>Tualatin Basin.</u> The Columbia River basalt aquifer and the Willamette confining unit are the only regional hydrogeologic units above the basement-confining unit in the Tualatin Basin. The Columbia River basalt aquifer underlies the entire basin, and its upper surface forms a sediment-filled bowl-like depression.

The Central Willamette Valley All five of the hydrogeologic units occur in the central Willamette Valley. The Columbia River basalt aquifer underlies the entire central Willamette Valley, except for small areas along the far eastern margin. A number of faults have been mapped in the central Willamette Valley, some of which offset the aquifer, and numerous other faults have been mapped in the uplands surrounding the basin where the aquifer crops out. The Willamette aquifer in the central Willamette Valley contains three major alluvial fans -- the Salem fan, the Molalla fan, and the Canby fan. The Willamette Silt unit overlies most of the central valley with a maximum thickness of about 130 feet near the center and thins towards the south and near the margins of the basin.

The Southern Willamette Valley In the southern Willamette Valley, all of the regional hydrogeologic units are present; however, the Columbia River basalt aquifer occurs only in the Stayton area. The Willamette confining unit is thinner in the southern Willamette Valley than elsewhere in the Willamette Lowland. The Willamette aquifer contains the Lebanon fan and the Stayton fan. The Willamette aquifer is much thinner (averaging only about 20 to 40 feet thick) between the alluvial fans of the southern Willamette Valley. The Willamette Silt unit covers most of the southern Willamette Valley and generally thin towards the south.