WATER RESOURCES DEPARTMENT

MEMO **22 July 2013**

TO: **Application G-17686**

FROM: **GW: Gerald H. Grondin**
(Reviewer's Name)

SUBJECT: Scenic Waterway Interference Evaluation

☐ YES
The source of appropriation is within or above a Scenic Waterway
☒ NO

☐ YES
Use the Scenic Waterway condition (Condition 7J)
☒ NO

☐ Per ORS 390.835, the Groundwater Section is **able** to calculate ground water interference with surface water that contributes to a Scenic Waterway. The calculated interference is distributed below.

☒ Per ORS 390.835, the Groundwater Section is **unable** to calculate ground water interference with surface water that contributes to a scenic waterway; **therefore, the Department is unable to find that there is a preponderance of evidence that the proposed use will measurably reduce the surface water flows necessary to maintain the free-flowing character of a scenic waterway.**

DISTRIBUTION OF INTERFERENCE
Calculate the percentage of consumptive use by month and fill in the table below. If interference cannot be calculated, per criteria in 390.835, do not fill in the table but check the "unable" option above, thus informing Water Rights that the Department is *unable to make a Preponderance of Evidence finding.*

Exercise of this permit is calculated to reduce monthly flows in _____ Scenic Waterway by the following amounts expressed as a proportion of the consumptive use by which surface water flow is reduced.

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec

PUBLIC INTEREST REVIEW FOR GROUND WATER APPLICATIONS

TO: Water Rights Section Date **22 July 2013**

FROM: Ground Water/Hydrology Section **Gerald H. Grondin**
Reviewer's Name

SUBJECT: Application G- **17686** Supersedes review of
Date of Review(s)

PUBLIC INTEREST PRESUMPTION; GROUNDWATER

OAR 690-310-130 (1) *The Department shall presume that a proposed groundwater use will ensure the preservation of the public welfare, safety and health as described in ORS 537.525.* Department staff review ground water applications under OAR 690-310-140 to determine whether the presumption is established. OAR 690-310-140 allows the proposed use be modified or conditioned to meet the presumption criteria. **This review is based upon available information and agency policies in place at the time of evaluation**.

A. GENERAL INFORMATION: Applicant's Name: **Fitzgerald Ranch, Inc.** County: **Lake**

A1. Applicant(s) seek(s) **0.85 cfs (383 gpm)** cfs from **2** well(s) in the **Goose & Summer Lakes** Basin, **Warner Lakes** subbasin Quad Map: **Plush**

A2. Proposed use: **Primary Irrigation (68.2 acres)** Seasonality: **1 March to 31 October (245 days)**

A3. Well and aquifer data **(attach and number logs for existing wells; mark proposed wells as such under logid)**:

Well	Logid	Applicant's Well #	Proposed Aquifer*	Proposed Rate(cfs)	Location (T/R-S QQ-Q)	Location, metes and bounds, e.g. 2250' N, 1200' E fr NW cor S 36
1	**LAKE 1839**	**Well 1**	**Basalt**	**0.85**	**T36s/R24E-sec 17 dad**	**2140' N, 230' W fr SE cor S 17**
2	**No Log**	**Well 2**	**Basalt**	**0.85**	**T36s/R24E-sec 17 dad**	**2140' N, 220' W fr SE cor S 17**
3						

* Alluvium, CRB, Bedrock

Well	Well Elev ft msl	First Water ft bls	SWL ft bls	SWL Date	Well Depth (ft)	Seal Interval (ft)	Casing Intervals (ft)	Liner Intervals (ft)	Perforations Or Screens (ft)	Well Yield (gpm)	Draw Down (ft)	Test Type
1	**4489**	**50**	**20**	**08/20/49**	**128**	**?**	**0-75**	**?**	**?**	**1000**	**20**	**P**
2	**4489**	**?**	**17.5**	**??/??/60**	**135**	**?**	**?**	**?**	**?**	**2500**	**?**	**?**

Use data from application for proposed wells.

A4. **Comments:**

The application requests a total maximum pumping rate of 0.85 cfs (383 gpm) and a total maximum annual volume of 204.6 acre-feet from a combined use of the two proposed POA wells.

Information for the two proposed POA wells comes from a combination of sources that include water well report LAKE 1839, final proof survey notes in file U-297 (permit U-273, certificate 31171), and USGS Professional Paper 1044-I by Sammel and Craig (1981). The two wells are located about 10 feet apart. Well LAKE 1839 has 10 inch casing, the other has 16 inch.

A5. ☐ **Provisions of the in general OAR 690-513; particularly OAR 690-513-0040 (Warner Lakes sub-basin)** Basin rules relative to the development, classification and/or management of ground water hydraulically connected to surface water ☐ **are**, *or* ☒ **are not**, activated by this application. (Not all basin rules contain such provisions.)
Comments:

A6. ☐ **Well(s) # N.A.** , , , , , tap(s) an aquifer limited by an administrative restriction.
Name of administrative area:
Comments: **Currently, there is no administrative area.**

B. GROUND WATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070

B1. **Based upon available data**, I have determined that ground water* for the proposed use:

a. ☐ **is** over appropriated, ☐ **is not** over appropriated, *or* ☒ **cannot be determined to be** over appropriated during any period of the proposed use. * This finding is limited to the ground water portion of the over-appropriation determination as prescribed in OAR 690-310-130;

b. ☐ **will not** *or* ☐ **will** likely be available in the amounts requested without injury to prior water rights. * This finding is limited to the ground water portion of the injury determination as prescribed in OAR 690-310-130;

c. ☐ **will not** *or* ☐ **will** likely to be available within the capacity of the ground water resource; or

d. ☒ **will, if properly conditioned**, avoid injury to existing ground water rights or to the ground water resource:
   i. ☒ The permit should contain condition #(s) **7B, 7N, 7T**;
   ii. ☐ The permit should be conditioned as indicated in item 2 below.
   iii. ☒ The permit should contain special condition(s) as indicated in item 3 below;

B2. a. ☐ **Condition** to allow ground water production from no deeper than _____ ft. below land surface;

b. ☐ **Condition** to allow ground water production from no shallower than _____ ft. below land surface;

c. ☐ **Condition** to allow ground water production only from the _____ ground water reservoir between approximately_____ ft. and_____ ft. below land surface;

d. ☐ **Well reconstruction** is necessary to accomplish one or more of the above conditions. The problems that are likely to occur with this use and without reconstructing are cited below. Without reconstruction, I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Ground Water Section.

Describe injury –as related to water availability– that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc): _____

B3. **Ground water availability remarks:**

The state observation well with long term data (early 1960s to 2013) closest to the proposed POA wells is state observation well 377 (well LAKE 1886) located in T36S/R24E-sec 33 abb. It is about 2.5 miles southeast of the proposed POA wells. The water level data shows long term climate influences as well as annual seasonal influences. Before the 1990s, peak annual groundwater levels were generally between 15 and 17 feet below land surface at the well. After 1990, the peak annual groundwater level has often been from 17 to 19 feet below land surface. Climate may be partly to entirely responsible for the lower annual peak levels after 1990. Ongoing groundwater level measurements will help that determination.

If a permit is issued, the following conditions should be included: 7B, 7N, 7T, and

The "large" water use condition: (require a totalizing flow meter at each well. Each flow meter shall be located within 50 feet of the wellhead and adjacent to each flow meter shall be a clearly visible monument with a sign noting the flow meter. Lastly, require for every flow meter the reading, recording (monthly at minimum), and annual reporting of the flow meter data, all flow meters).

Special Condition for groundwater production: "All POA wells under this permit shall comply with existing well construction standards. Groundwater production shall occur from the predominantly basalt unit below the predominantly basin fill unit by continuous casing and continuous seal through the predominantly basin fill unit and into the predominantly basalt unit."

C. GROUND WATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. **690-09-040 (1):** Evaluation of aquifer confinement:

Well	Aquifer or Proposed Aquifer	Confined	Unconfined
1	**Basalt**	☐	☒
2	**Undetermined (likely Basalt)**	☐	☒
		☐	☐
		☐	☐

Basis for aquifer confinement evaluation:

Walker (1973) and Walker and Repenning (1965) respectively map the surface geology at the proposed POA wells as Qs (lacustrine sedimentary rocks) and QTs (lacustrine, fluviatile, and Aeolian sedimentary rocks, interstratified tuff, ashy diatomite and unconsolidated clay, sand, and gravel). Sand dune deposits are noted near the wells as well as basalt (Tb) exposed in the uplands to the west of the wells.

The groundwater system is identified as generally unconfined with discontinuous low permeability layers causing local (discontinuous, limited) confinement. Generally, lower transmissivity (lower permeability) sediment (predominantly basin-fill sediment unit) of varying thickness overlies higher transmissivity (higher permeability) basalt (predominantly basalt unit). Groundwater occurs in both the predominantly basin-fill sediment unit and the predominantly basalt unit. Groundwater is vertically connected within each unit and between each unit. This is based upon investigations by Sammel and Craig (1981) for Warner Valley, Morgan (1988) for Goose Lake Valley and Miller (1984 and 1986) for the Fort Rock and Christmas Valley area. Sammel and Craig (1981) particularly note the similarity of the hydrogeology in the Warner lakes Valley to the Klamath Basin.

The predominant basin-fill sediment unit thickness can vary. For example, the depth to the top of the predominantly basalt unit is about 75 feet at the proposed POA well LAKE 1839; the depth to the top of the predominantly basalt unit is less than 20 feet at nearby well LAKE 1840 located about 500 feet west of the proposed POA wells; and the depth to the top of the predominantly basalt unit is about 150 feet at state observation well 377 (LAKE 1886) located about 2.5 miles southeast of the proposed POA wells.

C2. **690-09-040 (2) (3):** Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¼ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	GW Elev ft msl	SW Elev ft msl	Distance (ft)	Hydraulically Connected? YES	NO	ASSUMED	Potential for Subst. Interfer. Assumed? YES	NO
1	1	**Hart Lake**	**4469**	**4473**	**11400**	☒	☐	☐	☐	☒
2	1	**Hart Lake**	**4469**	**4473**	**11400**	☒	☐	☐	☐	☒
1	2	**Honey Creek**	**4469**	**4505**	**9300**	☒	☐	☐	☐	☒
2	2	**Honey Creek**	**4469**	**4505**	**9300**	☒	☐	☐	☐	☒

Basis for aquifer hydraulic connection evaluation:

Available reports indicate groundwater and surface water are connected in the Warner lakes Valley, and groundwater flows from south to north in the valley.

Groundwater at the proposed POA wells is downgradient of Honey Creek and somewhat coincident (parallel) to Hart Lake.

The distance to Honey Creek is to the perennial flow portion of the creek.

Water Availability Basin the well(s) are located within: HONEY CR > HART L – AT MOUTH

C3a. **690-09-040 (4):** Evaluation of stream impacts for each well that has been determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that surface water source, and not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% *natural* flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked ☒ box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < ¼ mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
		☐	☐			☐		☐		☐
		☐	☐			☐		☐		☐
		☐	☐			☐		☐		☐
		☐	☐			☐		☐		☐

C3b. **690-09-040 (4):** Evaluation of stream impacts by total appropriation for all wells determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. **Complete only if Q is distributed among wells**. Otherwise same evaluation and limitations apply as in C3a above.

	SW #		Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
			☐			☐		☐		☐
			☐			☐		☐		☐
			☐			☐		☐		☐
			☐			☐		☐		☐

Comments:

No analysis in this section given the proposed POA wells are more than 1.0 mile from Honey Creek and Hart Lake.

C4a. **690-09-040 (5):** Estimated impacts on **hydraulically connected surface water sources greater than one mile** as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

Non-Distributed Wells Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	2	0.2%	0.2%	0.0%	0.0%	0.0%	0.0%	0.1%	0.1%	0.1%	0.1%	0.2%	0.2%
Well Q as CFS		0.00	0.00	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.42	0.00	0.00
Interference CFS		0.001	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001	0.001

Distributed Wells Well	SW#	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q as CFS													
Interference CFS													
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q as CFS													
Interference CFS													

(A) = Total Interf.	0.001	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001	0.001
(B) = 80 % Nat. Q	5.06	6.64	12.6	41.5	53.8	26.8	4.32	2.27	2.07	2.14	3.01	3.74
(C) = 1 % Nat. Q	0.0506	0.0664	0.1260	0.4150	0.5380	0.2680	0.0432	0.0227	0.0207	0.0214	0.0301	0.0374
(D) = (A) > (C)	No	No	No	No	No	No	No	No	No	No	No	No
(E) = (A / B) x 100	0.0198	0.0151	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0467	0.0332	0.0267

(A) = total interference as CFS; (B) = WAB calculated natural flow at 80% exceed. as CFS; (C) = 1% of calculated natural flow at 80% exceed. as CFS; (D) = highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage.

Basis for impact evaluation:

Analysis is done in this section given the proposed POA wells are more than 1.0 mile from Honey Creek and Hart Lake.

The Table above was used for interference with Honey Creek only given it is the water body with water availability data. All the pumping was assigned to one of the POA wells only given the two wells are similar and about 10 feet apart.

A pro-rated pumping rate of 0.42 cfs (189 gpm) was used for the pumping rate. The pro-rated rate is the maximum annual volume of water allowed (204.6 ac-ft) divided the total time (245 days). This distributes the pumping over the entire proposed irrigation season.

Hunt (2003) was used to calculate the interference:

Used pro-rated pumping rate = 0.42 cfs (189 gpm),
Used aquifer transmissivity = 10,000 ft2/day based on specific capacity of LAKE 1840, LAKE1825, and LAKE 1839. The value is within the range noted by Sammel and Craig (1981)
Used, an intermediate storage coefficient = 0.001
Used, sediment hydraulic conductivity Kv = 1.00 ft/day (horizontal conductivity (Kh) divided by 100)
Used sediment thickness below lake = 150 feet (based on LAKE 1888 near Honey Creek)
Used stream width = 20 feet.

The Theis equation (Theis, 1935) was used to calculate the groundwater level drawdown at Hart Lake using the same values above. The calculated drawdown at the end of 30 days pumping was 1.02 feet for continuous pumping at the maximum rate and 0.51 feet for continuous pumping at the pro-rated rate. The calculated drawdown at the end of 245 days pumping was 2.20 feet for continuous pumping at the maximum rate and 1.09 feet for continuous pumping at the pro-rated rate.

C4b. **690-09-040 (5) (b) The potential to impair or detrimentally affect the public interest is to be determined by the Water Rights Section.**

C5. ☒ **If properly conditioned**, the surface water source(s) can be adequately protected from interference, and/or ground water use under this permit can be regulated if it is found to substantially interfere with surface water:

i. ☒ The permit should contain condition #(s) **7B, 7N, 7T**;

ii. ☒ The permit should contain special condition(s) as indicated in "Remarks" below;

C6. **SW / GW Remarks and Conditions**

If a permit is issued, the following conditions should be included: 7B, 7N, 7T, and

The "large" water use condition: (require a totalizing flow meter at each well. Each flow meter shall be located within 50 feet of the wellhead and adjacent to each flow meter shall be a clearly visible monument with a sign noting the flow meter. Lastly, require for every flow meter the reading, recording (monthly at minimum), and annual reporting of the flow meter data, all flow meters).

Special Condition for groundwater production: "All POA wells under this permit shall comply with existing well construction standards. Groundwater production shall occur from the predominantly basalt unit below the predominantly basin fill unit by continuous casing and continuous seal through the predominantly basin fill unit and into the predominantly basalt unit."

The groundwater system is identified as generally unconfined with discontinuous low permeability layers causing local (discontinuous, limited) confinement. Generally, lower transmissivity (lower permeability) sediment (predominantly basin-fill sediment unit) of varying thickness overlies higher transmissivity (higher permeability) basalt (predominantly basalt unit). Groundwater occurs in both the predominantly basin-fill sediment unit and the predominantly basalt unit. Groundwater is vertically connected within each unit and between each unit. This is based upon investigations by Sammel and Craig (1981) for Warner Valley, Morgan (1988) for Goose Lake Valley and Miller (1984 and 1986) for the Fort Rock and Christmas Valley area. Sammel and Craig (1981) particularly note the similarity of the hydrogeology in the Warner lakes Valley to the Klamath Basin.

Application G- 17686 continued Date 22 July 2013

References Used:

References consulted were:

Hampton, E.R., 1964, Geologic factors that control the occurrence and availability of ground water in the Fort Rock Basin, Lake County, Oregon: USGS Professional Paper 383-B, 29 p.

Hunt, B., 2003, Unsteady stream depletion when pumping from semiconfined aquifer: Journal of Hydrologic Engineering, January/February, 2003.

McFarland, W.D. and Ryals, G.N., 1991, Adequacy of available hydrogeologic data for evaluation of declining ground-water levels in the Fort Rock Basin, south-central Oregon: USGS Water Resources Investigations Report 89-4057, 47 p.

Miller, D.W., 1984, Appraisal of ground-water conditions in the Fort Rock Basin, Lake County, Oregon: OWRD Open File Report, 157 p.

Miller, D.W., 1986, Ground-water conditions in the Fort Rock Basin, northern Lake County, Oregon: OWRD Ground Water Report No. 31, 196 p.

Morgan, D.S., 1988, Geohydrology and numerical model analysis of ground-water flow in the Goose Lake Basin, Oregon and California: USGS Water Resources Investigations Report 87-4058, 92 p.

Oregon Water Resources Department, 1989, Goose and Summer Lakes Basin report: OWRD Basin Report, 112 p.

Peterson, N.V. and McIntyre, J.R., 1970, The reconnaissance geology and mineral resources of eastern Klamath County and western Lake County, Oregon: DOGAMI Bulletin 66, 70 p.

Phillips, K.N. and VanDenburgh, A.S., 1971, Hydrology and geochemistry of Abert, Summer, and Goose Lakes, and other closed-basin lakes in south-central Oregon: USGS Professional Paper 502-B, 86p.

Sammel, E.A. and Craig, R.W., 1981, The geothermal hydrology of Warner Valley, Oregon: a reconnaissance study: USGS Professional Paper 1044-I, 147 p.

Theis, C.V. 1935. The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using groundwater storage. American Geophysical Union Transactions, 16 annual meeting, vol. 16, pg. 519-524.

Walker, G.W., 1963, Reconnaissance geologic map of the eastern half of the Klamath Falls (AMS) quadrangle, Lake and Klamath Counties, Oregon: USGS Mineral Investigations Field Studies Map MF-260.

Walker, G.W. and Repenning, C.A., 1965, Reconnaissance geologic map of the Adel quadrangle, Lake, Klamath, and Malheur Counties, Oregon: USGS Miscellaneous Geologic Investigations Map I-446.

Walker, G.W., 1973, Preliminary geologic and tectonic maps of Oregon east of the 121st meridian: USGS Miscellaneous Field Studies Map MF-495

Waring, G.A., 1908, Geology and water resources of a portion of south-central Oregon: USGS Water Supply Paper 220, 85 p.

Goose and Summer Lakes Basin Program rules (OAR 690-513).

Old State Obesrvation Well SOW 377 (LAKE 1886).

Water well reports for wells in Township 36 South/Range 24 East

Application G- 17686 continued Date 22 July 2013

D. WELL CONSTRUCTION, OAR 690-200

D1. Well #: 1 Logid: LAKE 1839
Well #: 2 Logid: No Log

D2. **THE WELL does not meet current well construction standards based upon:**
a. ☐ review of the well log;
b. ☐ field inspection by _____;
c. ☐ report of CWRE _____;
d. ☐ other: (specify) _____

D3. **THE WELL construction deficiency**:
a. ☐ constitutes a health threat under Division 200 rules;
b. ☐ commingles water from more than one ground water reservoir;
c. ☐ permits the loss of artesian head;
d. ☐ permits the de-watering of one or more ground water reservoirs;
e. ☐ other: (specify) _____

D4. **THE WELL construction deficiency is described as follows:** _____

D5. **THE WELL**
a. ☐ **was**, *or* ☐ **was not** constructed according to the standards in effect at the time of original construction or most recent modification.

b. ☒ I don't know if it met standards at the time of construction.

Comments: _____

Special Condition for groundwater production: "All POA wells under this permit shall comply with existing well construction standards. Groundwater production shall occur from the predominantly basalt unit below the predominantly basin fill unit by continuous casing and continuous seal through the predominantly basin fill unit and into the predominantly basalt unit."

D6. ☐ **Route to the Enforcement Section.** I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Enforcement Section and the Ground Water Section.

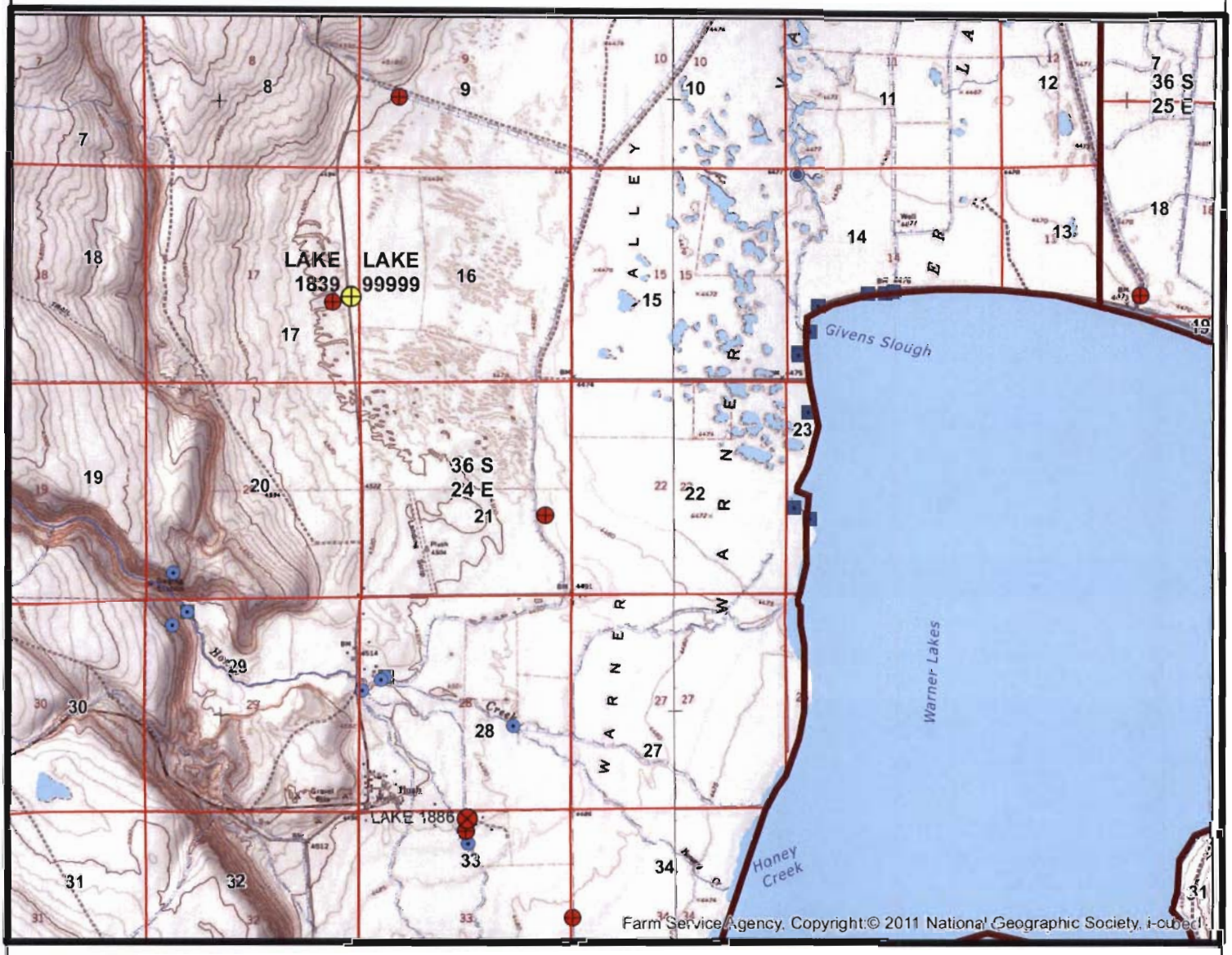
THIS SECTION TO BE COMPLETED BY ENFORCEMENT PERSONNEL

D7. ☐ Well construction deficiency has been corrected by the following actions: _____

_____ _____, 200____.
(Enforcement Section Signature)

D8. ☐ **Route to Water Rights Section (attach well reconstruction logs to this page).**

Groundwater Right Application G-17686
Fitzgerald Ranch, Inc.



0 0.5 1 2 3

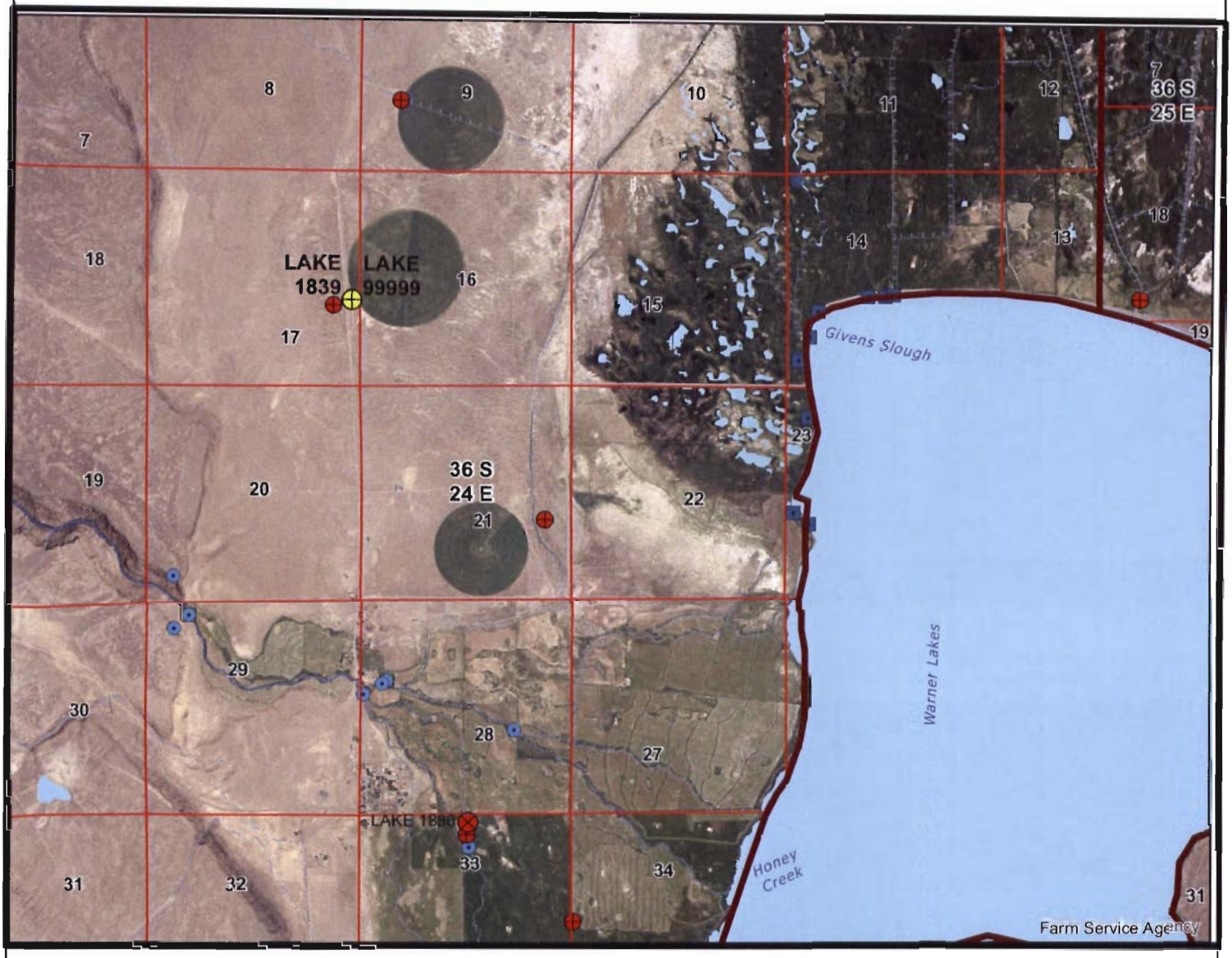
Miles

Yellow = Application Noted Well(s)
Red = Other Existing or Proposed Wells

Blue and Other = surface water rights

N

Groundwater Right Application G-17686
Fitzgerald Ranch, Inc.



0 0.5 1 2 3

Miles

Yellow = Application Noted Well(s)
Red = Other Existing or Proposed Wells

Blue and Other = surface water rights

N

STATE ENGINEER
Salem, Oregon

Lake 1839

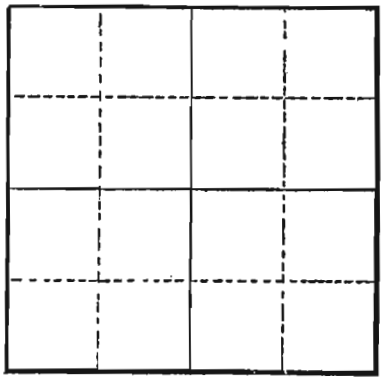
Well Record

STATE WELL NO. 36/24-17J(1)
COUNTY Lake
APPLICATION NO. .....

OWNER: J. P. Eagan
MAILING ADDRESS: .....

LOCATION OF WELL: Owner's No. .....
CITY AND STATE: .....

NE ¼ SE ¼ Sec. 17 T. 36 ~~N.~~ S., R. 24 ~~E.~~ W, W.M.



Bearing and distance from section or subdivision corner .....

Altitude at well 4495

TYPE OF WELL: drilled Date Constructed .....

Depth drilled 128 Depth cased 75

Section .....

CASING RECORD: 10 inch

FINISH:

AQUIFERS: Volcanic breccia (?)

WATER LEVEL: 20

PUMPING EQUIPMENT: Type turbine H.P. .....
Capacity 1000 G.P.M.

WELL TESTS:
Drawdown ..... ft. after ..... hours ..... G.P.M.
Drawdown ..... ft. after ..... hours ..... G.P.M.

USE OF WATER irrigation Temp. ..... °F. ....., 19.....
SOURCE OF INFORMATION .....
DRILLER or DIGGER .....
ADDITIONAL DATA:
Log X Water Level Measurements ..... Chemical Analysis X Aquifer Test .....

REMARKS: Reported drawdown 20 ft. when pumped at 1000 gpm.

State Printing 89316

STATE ENGINEER
Salem, Oregon

State Well No. 36/24-17J(1)
County Lake
Application No.

Well Log

Owner: J. P. Eagan Owner's No.

Driller: Frank Williams Date Drilled 1949

CHARACTER OF MATERIAL	(Feet below land surface) From	To	Thickness (feet)
Soil	0	1	1
Older valley fill:			
Clay, light gray	1	22	21
Sand, gray	22	22½	½
Clay, light gray	22½	50	27½
Sand, water-bearing	50	75	25
Tertiary volcanic rock:			
Lava rock	75	87	12
"Cinders" volcanic breccia(?), water-bearing	87	105	18
Lava rock	105	128	23

STATE ENGINEER
Salem, Oregon

State Well No. 36/24-17J0

County Lake

Application No. .....

Chemical Analysis

OWNER J. P. Eagan OWNER'S NO. .....

ANALYST U. S. G. S. Address .....

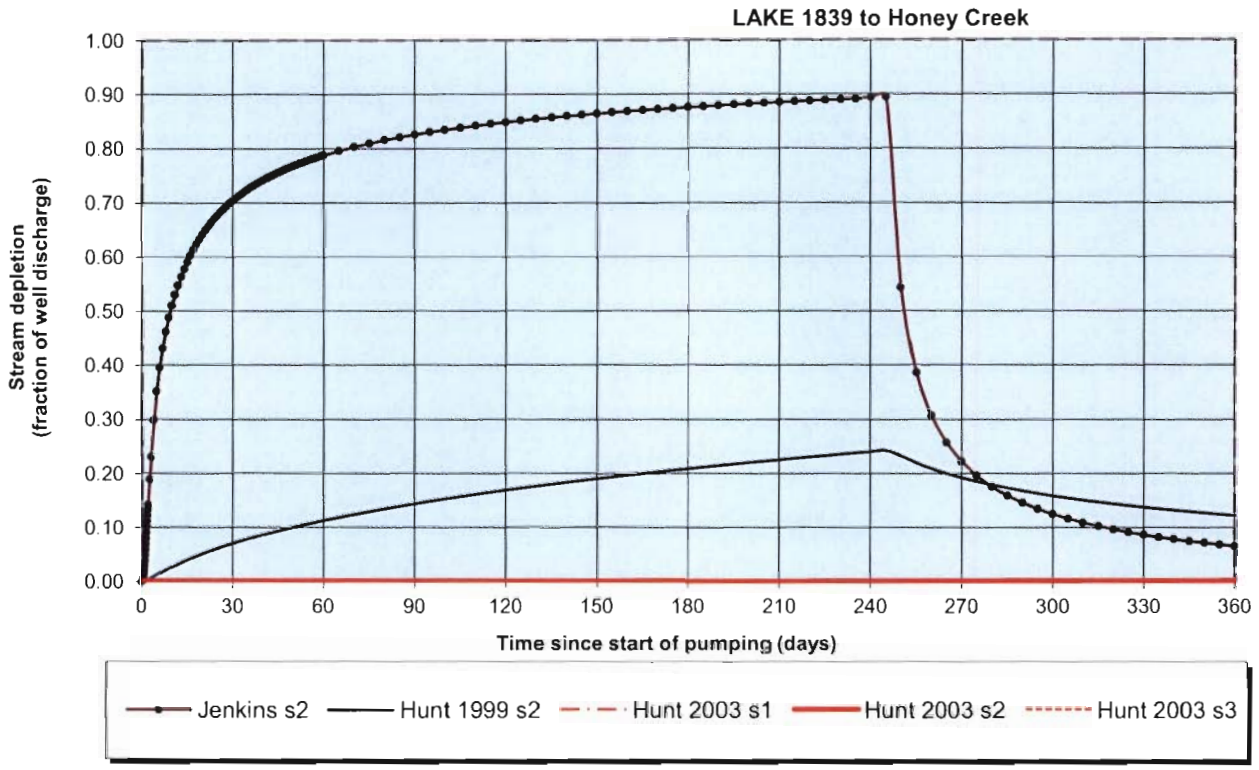
Date of Collection Feb. 13, 1950

Point of Collection .....

	P.P.M.	E.P.M.
Silica (SiO_2)	45	
Iron (Fe) Total	.16	
Manganese (Mn)		
Calcium (Ca)	13	.65
Magnesium (Mg)	8.7	.71
Sodium (Na)	21	.91
Potassium (K)	7	.18
Bicarbonate (HCO_3)	122	2.
Carbonate (CO_3)		
Sulfate (SO_4)	8.5	.18
Chloride (Cl)	5.0	.14
Fluoride (F)	.2	.01
Nitrate (NO_3)	1.9	.03
Boron (B)	.01	.00
Dissolved Solids	170	
Hardness as $CaCO_3$	69	
Specific Conductance (Micromhos at 25°C)	225	
pH	8.1	
Percent Sodium	37	
Sodium Absorption Ratio (S.A.R.)		
CLASS		

State Printing 89313

Transient Stream Depletion (Jenkins, 1970; Hunt, 1999, 2003)



Output for Stream Depletion, Scenerio 2 (s2):						Time pump on (pumping duration) = 245 days						
Days	30	60	90	120	150	180	210	240	270	300	330	360
J SD	70.4%	78.8%	82.6%	84.9%	86.5%	87.7%	88.6%	89.3%	22.2%	12.5%	8.7%	6.6%
H SD 1999	7.1%	11.4%	14.5%	17.0%	19.1%	21.0%	22.6%	24.1%	19.2%	15.9%	13.8%	12.3%
H SD 2003	0.0%	0.0%	0.0%	0.0%	0.1%	0.1%	0.1%	0.1%	0.2%	0.2%	0.2%	0.2%
Qw, cfs	0.420	0.420	0.420	0.420	0.420	0.420	0.420	0.420	0.420	0.420	0.420	0.420
H SD 99, cfs	0.030	0.048	0.061	0.071	0.080	0.088	0.095	0.101	0.081	0.067	0.058	0.052
H SD 03, cfs	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001	0.001	0.001	0.001

Parameters:		Scenario 1	Scenario 2	Scenario 3	Units
Net steady pumping rate of well	Qw	0.42	0.42	0.42	cfs
Time pump on (pumping duration)	tpon	245	245	245	days
Perpendicular from well to stream	a	9300	9300	9300	ft
Well depth	d	128	128	128	ft
Aquifer hydraulic conductivity	K	100	100	100	ft/day
Aquifer saturated thickness	b	100	100	100	ft
Aquifer transmissivity	T	10000	10000	10000	ft*ft/day
Aquifer storativity or specific yield	S	0.001	0.001	0.001	
Aquitard vertical hydraulic conductivity	Kva	1	1	1	ft/day
Aquitard saturated thickness	ba	150	150	150	ft
Aquitard thickness below stream	babs	150	150	150	ft
Aquitard porosity	n	0.2	0.2	0.2	
Stream width	ws	20	20	20	ft
Streambed conductance (lambda)	sbc	0.133333	0.133333	0.133333	ft/day
Stream depletion factor	sdf	8.649000	8.649000	8.649000	days
Streambed factor	sbf	0.124000	0.124000	0.124000	
input #1 for Hunt's Q_4 function	t'	0.115620	0.115620	0.115620	
input #2 for Hunt's Q_4 function	K'	57.660000	57.660000	57.660000	
input #3 for Hunt's Q_4 function	epsilon'	0.005000	0.005000	0.005000	
input #4 for Hunt's Q_4 function	lamda'	0.124000	0.124000	0.124000	

Drawdown Calculations Using Theis Equation

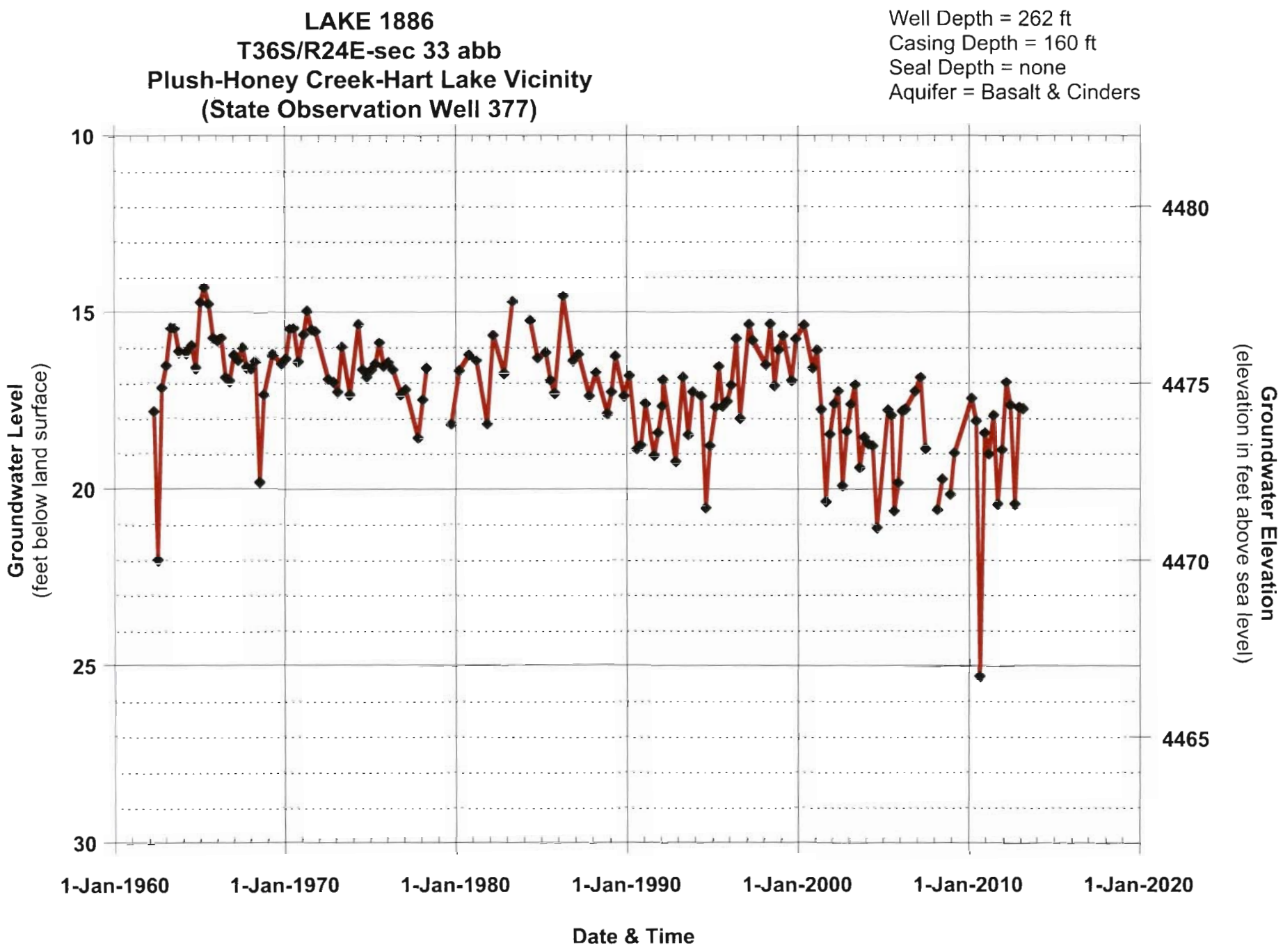
Theis Equation: $s = [Q/(4*T*pi)][W(u)]$

$u = (r*r*S)/(4*T*t)$

$W(u) = (-\ln u)-(0.5772157)+(u/1*1!)-(u*u/2*2!)+(u*u*u/3*3!)-(u*u*u*u/4*4!)+\ldots$

s = drawdown (L)
T = transmissivity (L*L/T)
S = storage coefficient (dimensionless)
pi = 3.141592654
r = radial distance (L)
t = time (T)
u = dimensionless
W(u) = well function

Transmissivity T (gpd/ft)	Transmissivity T (ft2/day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft3/sec)	Time t (days)	Distance r (feet)	pi	u	W(u)	Drawdown s (feet)	Comments
								Note : W(u) calculation valid when u < 7.1			
Note: yellow grid areas are where values are calculated								7.0000	1.1545E-04		W(u) calculation test
Proposed Well (LAKE 1839) to Hart Lake (Transmissivity from specific capacity data)											
74,805.20	10,000.00	0.00100	381.51	0.85	30.00	11,400.00	3.14	0.1083	1.7511	1.0234	Continuous Pumping at Full Rate
74,805.20	10,000.00	0.00100	381.51	0.85	245.00	11,400.00	3.14	0.0133	3.7589	2.1968	Continuous Pumping at Full Rate
74,805.20	10,000.00	0.00100	188.97	0.42	30.00	11,400.00	3.14	0.1083	1.7511	0.5069	Pro-Rated Pumping Rate
74,805.20	10,000.00	0.00100	188.97	0.42	245.00	11,400.00	3.14	0.0133	3.7589	1.0881	Pro-Rated Pumping Rate


LAKE 1886
T36S/R24E-sec 33 abb
Plush-Honey Creek-Hart Lake Vicinity
(State Observation Well 377)
Well Depth = 262 ft
Casing Depth = 160 ft
Seal Depth = none
Aquifer = Basalt & Cinders
Groundwater Level
(feet below land surface)
10
15
20
25
30
Groundwater Elevation
(elevation in feet above sea level)
4480
4475
4470
4465
1-Jan-1960
1-Jan-1970
1-Jan-1980
1-Jan-1990
1-Jan-2000
1-Jan-2010
1-Jan-2020
Date & Time

Drawdown Calculations Using Theis Equation

Theis Equation: $s = [Q/(4*T*pi)][W(u)]$

$u = (r*r*S)/(4*T*t)$

$W(u) = (-\ln u)-(0.5772157)+(u/1*1!)-(u*u/2*2!)+(u*u*u/3*3!)-(u*u*u*u/4*4!)+...$

s = drawdown (L)
T = transmissivity (L*L/T)
S = storage coefficient (dimensionless)
pi = 3.141592654
r = radial distance (L)
t = time (T)
u = dimensionless
W(u) = well function

Transmissivity T (gpd/ft)	Transmissivity T (ft2/day)	Storage Coefficient S	Pumping Rate Q (gal/min)	Pumping Rate Q (ft3/sec)	Time t (days)	Distance r (feet)	pi	u	W(u)	Drawdown s (feet)	Comments
								Note : W(u) calculation valid when u < 7.1			
Note: yellow grid areas are where values are calculated								7.0000	1.1545E-04		W(u) calculation test
Proposed Well (LAKE 1839) to Hart Lake (Transmissivity from specific capacity data)											
74,805.20	10,000.00	0.00100	381.51	0.85	30.00	11,400.00	3.14	0.1083	1.7511	1.0234	Continuous Pumping at Full Rate
74,805.20	10,000.00	0.00100	381.51	0.85	245.00	11,400.00	3.14	0.0133	3.7589	2.1968	Continuous Pumping at Full Rate
74,805.20	10,000.00	0.00100	188.97	0.42	30.00	11,400.00	3.14	0.1083	1.7511	0.5069	Pro-Rated Pumping Rate
74,805.20	10,000.00	0.00100	188.97	0.42	245.00	11,400.00	3.14	0.0133	3.7589	1.0881	Pro-Rated Pumping Rate