WATER RESOURCES DEPARTMENT

Decem	ber	21	,20	15

TO: Application G-<u>18121</u>

FROM: GW: <u>Aurora Boucher</u> (Reviewer's Name)

SUBJECT: Scenic Waterway Interference Evaluation

- YES
 The source of appropriation is within or above a Scenic Waterway
 NO
 YES
 Use the Scenic Waterway condition (Condition 7J)
 NO
- Per ORS 390.835, the Groundwater Section is **able** to calculate ground water interference with surface water that contributes to a Scenic Waterway. The calculated interference is distributed below.
- Per ORS 390.835, the Groundwater Section is **unable** to calculate ground water interference with surface water that contributes to a scenic waterway; **therefore**, **the Department is unable to find that there is a preponderance of evidence that the proposed use will measurably reduce the surface water flows necessary to maintain the free-flowing character of a scenic waterway.**

DISTRIBUTION OF INTERFERENCE

Calculate the percentage of consumptive use by month and fill in the table below. If interference cannot be calculated, per criteria in 390.835, do not fill in the table but check the "unable" option above, thus informing Water Rights that the Department is unable to make a Preponderance of Evidence finding.

Exercise of this permit is calculated to reduce monthly flows in ______ Scenic Waterway by the following amounts expressed as a proportion of the consumptive use by which surface water flow is reduced.

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec

¥?

PUB.	LIC INTER	EST REVIEW	FOR GROUNDV	VATER APPL	ICATIONS	
TO:	W	ater Rights Secti	on		Date	December 21, 2015
FROM	M: G	roundwater Secti	on	Aurora C Bo	uchier / Ken Lite	
SUBJ	ECT: A	pplication G- 181	121	Reviewer's Nan Supersedes	ne s review of	
						Date of Review(s)
PUBI	LIC INTER	EST PRESUMP	TION: GROUND	WATER		
to dete the pro	ermine whethe esumption crite	r the presumption i eria. This review i	is established. OAR 6 s based upon availa	590-310-140 allow	ws the proposed use be n and agency policies in r	nodified or conditioned to meet
A. <u>GI</u> A1.	ENERAL IN Applicant(s	FORMATION:) seek(s) 0.003	Applicant's Na	me: Randal well(s) in the	l Arnett Deschutes	County: <u>Crook</u> Basin,
A. <u>GI</u> A1.	ENERAL IN Applicant(s Low	FORMATION:) seek(s) <u>0.003</u> er Crooked	Applicant's Nacfs from2	me: <u>Randal</u> well(s) in the	l Arnett Deschutes	County: <u>Crook</u> Basin,
A. <u>GI</u> A1. A2. A3.	ENERAL IN Applicant(s Low Proposed u Well and ad	FORMATION:) seek(s) 0.003 (er Crooked se Pond r uifer data (attach	Applicant's Na _cfs from <u>2</u> maintenance and number logs fo	me:Randal well(s) in the subbasin Seasonality: r existing wells;	l Arnett Deschutes January 1 – Decem mark proposed wells a	County: <u>Crook</u> Basin, ber 31s such under logid):
A. <u>GI</u> A1. A2. A3. Well	ENERAL IN Applicant(s Low Proposed u Well and ac Logid	FORMATION:) seek(s) 0.003 /er Crooked se Pond r juifer data (attach Applicant's Well #	Applicant's Na _cfs from <u>2</u> maintenance and number logs fo Proposed Aquifer*	me: <u>Randal</u> well(s) in the subbasin Seasonality: r existing wells; Proposed Rate(cfs)	I Arnett Deschutes January 1 – Decem mark proposed wells a: Location (T/R-S QQ-Q)	County: <u>Crook</u> Basin, ber 31 s such under logid): Location, metes and bounds, e.g. 2250' N, 1200' E fr NW cor S 36
A. <u>G</u> A1. A2. A3. Well	ENERAL IN Applicant(s Low Proposed u Well and ac Logid CROO 365	FORMATION:) seek(s) 0.003 (er Crooked se Pond r juifer data (attach Applicant's Well # 1	Applicant's Na _cfs from <u>2</u> maintenance and number logs fo Proposed Aquifer* Alluvium	me: <u>Randal</u> well(s) in the subbasin Seasonality: r existing wells; Proposed Rate(cfs) 0.003	I Arnett Deschutes January 1 – Decem mark proposed wells as Location (T/R-S QQ-Q) T13S/R17E-S25 SE-NE	County: Crook Basin, ber 31 s such under logid): Location. metes and bounds, e.g. 2250' N, 1200' E fr NW cor S 36 1780' S, 80'W of NE cor S 25

 $\begin{array}{c|cccc} wen & Elev & water \\ \hline ft msl & ft bls \\ \hline 1 & 3530 & 40 & 10 \\ \end{array}$

First

Water

13

SWL

28

SWL

Date

2/27/1992

6/24/2015

Alluvium, CRB, Bedrock

Well

Elev

3540

4

Well

2

 Use data from application for proposed wells.
 A4. Comments: Mill Creek is a perennial stream cutting into low permeability units of the Clarno and John Day formations. Mill Creek is a regional sink for groundwater discharge with numerous springs along its valley and at the source of many of the tributaries to Mill Creek. Any withdrawals from Mill Creek will likely affect downstream water rights. According to Water Master Jeremy Giffin (personal communication 7/21/2015), this is the most heavily regulated creek in the basin.

Seal

Interval

(ft)

0-22

0-59

Casing

Intervals

(ft)

+1-50

+2-59

Liner

Intervals

(ft)

Well

Depth

 (\mathbf{ft})

60

196

Both wells are located on an elevated alluvial terrace above Mill Creek. Well 1 (CROO 365) is constructed into the alluvium. Well 2 (CROO 54251) is constructed into a water-bearing zone within a basalt flow of the Clarno Formation. Hydraulic head is coincident with overlying terrace gravel and the creek.

- A6. Well(s) # ____

____, _____, _____, ____, tap(s) an aquifer limited by an administrative restriction.

Name of administrative area: _____ Comments: Well

Yield

(gpm)

10

30

Draw

Down

(ft)

40

Test

Туре

Pump

Air

Perforations

Or Screens

(ft)

30-50

156-196**

B. GROUNDWATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070

- Based upon available data, I have determined that groundwater* for the proposed use: B1.
 - is over appropriated, is not over appropriated, or annot be determined to be over appropriated during any a. period of the proposed use. * This finding is limited to the groundwater portion of the over-appropriation determination as prescribed in OAR 690-310-130;
 - will not or will likely be available in the amounts requested without injury to prior water rights. * This finding b. is limited to the groundwater portion of the injury determination as prescribed in OAR 690-310-130;
 - will not or will likely to be available within the capacity of the groundwater resource; or c.
 - will, if properly conditioned, avoid injury to existing groundwater rights or to the groundwater resource: d. i. The permit should contain condition #(s) 7N, 7J
 - The permit should be conditioned as indicated in item 2 below. ii.
 - iii. The permit should contain special condition(s) as indicated in item 3 below;

Condition to allow groundwater production from no deeper than ______ ft. below land surface; B2. a.

- Condition to allow groundwater production from no shallower than ______ ft. below land surface; b.
- Condition to allow groundwater production only from the groundwater reservoir between approximately______ft. and ______ft. below Condition to allow groundwater production only from the c. land surface:
- Well reconstruction is necessary to accomplish one or more of the above conditions. The problems that are likely d. to occur with this use and without reconstructing are cited below. Without reconstruction, I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Groundwater Section.

Describe injury -as related to water availability- that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc):

B3. Groundwater availability remarks:

Condition with 7N and 7J.

Both wells are located on an elevated alluvial terrace above Mill Creek. Well 1 (CROO 365) is constructed into the alluvium. Well 2 (CROO 54251) is constructed into water-bearing zones within a basalt layer of the Clarno Formation. The Clarno Formation is Eocene in age and consists of lava flows, mudflows, and tuffs which are mainly of basaltic and andesitic composition (Waters, 1968). Due to its age, the Clarno Formation generally has very low permeability as much of the tuffaceous material has devitrified and the lava flows have weathered and contain abundant secondary minerals. Productive permeability in the Clarno Formation tends to be secondary, such as along fractures zones. In Well 2 the hydraulic head is coincident with overlying terrace gravel within a 1/4 mile of the well. The groundwater in the basalt may be hydraulically connected to the overlying sediment via a fracture network, and therefore, when saturated, the underlying basalt may be hydraulically connected to surface water. The orientation of any local fracture network is unknown. Other wells in the area appear to be producing water from both the alluvium and water-bearing zones in the Clarno Formation (CROO 680, CROO 683, and CROO 51917).

There are no nearby wells for which water level trends are available.

C. GROUNDWATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. 690-09-040 (1): Evaluation of aquifer confinement:

Well	Aquifer or Proposed Aquifer	Confined	Unconfined
1	Alluvium		\square
2	Bedrock (Basalt)		\square

Basis for aquifer confinement evaluation: Well 1 (CROO 365) is producing water from the Quaternary alluvium. Although the well log shows a clay layer from 16-30 feet and lists a static water level above the water bearing zone at which it was encountered, it is likely that the well has an efficient connection with the creek due to the elevation of the static water level in the well being coincident with that of the adjacent section of the creek.

The well log for Well 2 (CROO 54251) lists 110 feet of basalt overlying the water bearing zone. Given the age of the formation, the groundwater in the basalt is likely hydraulically connected to the overlying sediment and subsequently to surface water through secondary porosity in the form of a fracture network. An indication that the bedrock is likely fractured is the static water level in Well 2 being coincident with the elevation of the stream within a ¼ mile of the well, although the orientation of any fractures is unknown.

C2. **690-09-040** (2) (3): Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¹/₄ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

Well	SW #	Surface Water Name	GW Elev ft msl	SW Elev ft msl	Distance (ft)	Hy C YES	ydrau Conne NO	lically cted? ASSUMED	Potentia Subst. Int Assume YES	l for erfer. ed? NO
1	1	Mill Creek	3520	3520	120	\square			\boxtimes	
2	1	Mill Creek	3512	3520	300	\square			\boxtimes	

Basis for aquifer hydraulic connection evaluation: The elevation of the static water level listed on the well log for CROO 365 is coincident with the elevation of the adjacent segment of Mill Creek. The elevation of the static water level listed on the well log for CROO 54251 is lower than the elevation of the adjacent segment of Mill Creek. However, the elevation of the static water level for CROO 54251 is coincident with the elevation of a segment of Mill Creek located less than 1/4 mile (~900 ft) downstream from the well.

Water Availability Basin the well(s) are located within: <u>70611: OCHOCO CR > CROOKED R - AT MOUTH</u>

C3a. 690-09-040 (4): Evaluation of stream impacts for <u>each well</u> that has been determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that surface water source, and not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% *natural* flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked 🖾 box indicates the well is assumed to have the potential to cause PSI.

Well	SW #	Well < ¼ mile?	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw> 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?
1	1	\boxtimes		-	-		3.35		30-40%	٦
2	1	\boxtimes		-	-		3.35		See	
									comments	

C3b. 690-09-040 (4): Evaluation of stream impacts by total appropriation for all wells determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Complete only if Q is distributed among wells. Otherwise same evaluation and limitations apply as in C3a above.

SW #	Qw > 5 cfs?	Instream Water Right ID	Instream Water Right Q (cfs)	Qw > 1% ISWR?	80% Natural Flow (cfs)	Qw > 1% of 80% Natural Flow?	Interference @ 30 days (%)	Potential for Subst. Interfer. Assumed?

Comments: For Well 1 (CROO 365), interference with Mill Creek at 30 days was estimated using the Hunt 1999 model and assuming a 3 foot streambed thickness. The aquifer storativity values were ranged between .15 and .3 based on published values for unconsolidated gravel (Driscoll, 1986).

Well 2 (CROO 54251) is likely impacting surface water along Mill Creek. However, the nature of the aquifer unit precludes the use of available analytical models to evaluate the timing of interference.

C4a. **690-09-040 (5):** Estimated impacts on **hydraulically connected surface water sources greater than one mile** as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

Non-Di Well	stributed SW#	Wells Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
	0	0%	0%	0%	0%	70	70	9%	70	90	%	%	%
Well O	as CES	10	10	10	10	10	10	10	10				
Interfere	ence CFS												
D! / 1						18	1			- 1 - 9 - 1			
Distrib	cw/#	Ton	Eab	Mor	Ann	May	Inn	Inl	Aug	Sen	Oct	Nov	Dec
wen	244	Jan	reu	Iviai	Apr	Iviay	Jun	Jui	Aug	Sep	000	1107	Dec
111.11.0	OFC	%	%	%	%	%	%	%	%	%0	70	%	7/0
wen Q	as CFS	-											
Intertere	ence CFS						~	~	~	~	~	~	
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
Interfere	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS												
Interfere	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well Q	as CFS								-				
Interfere	ence CFS												
		%	%	%	%	%	%	%	%	%	%	%	%
Well O	as CFS												
Interfere	ence CFS												
		90	%	%	%	%	%	%	%	%	%	%	%
Well O	as CFS	10											
Interfere	ence CFS												
									No. 1				
$(\mathbf{A}) = \mathbf{To}$	tal Interf.						-				_		
(B) = 80	% Nat. Q												
(C) = 1	% Nat. O			-									

(D) = (A) > (C)												
$(E) = (A / B) \times 100$	%	%	%	%	%	%	%	%	%	%	%	%

(A) = total interference as CFS: (B) = WAB calculated natural flow at 80% exceed. as CFS; (C) = 1% of calculated natural flow at 80% exceed. as CFS; (D) = highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage.

Basis for impact evaluation:

C4b. 690-09-040 (5) (b) The potential to impair or detrimentally affect the public interest is to be determined by the Water Rights Section.

C5. If properly conditioned, the surface water source(s) can be adequately protected from interference, and/or groundwater use under this permit can be regulated if it is found to substantially interfere with surface water:

- i. The permit should contain condition #(s)____
- ii. The permit should contain special condition(s) as indicated in "Remarks" below;

C6. SW / GW Remarks and Conditions:

References Used:

Application file: G-18121.

Driscoll, F.G. (editor), 1986. Groundwater and Wells, Second Edition.

Hunt, B., 1999. Unsteady stream depletion from ground water pumping: Ground Water, v. 37, no. 1, p. 98-102.

OWRD files for Emergency Drought Application G-1811.

Water, A.C., and Vaughan, R.H., 1968. Reconnaissance Geologic Map of the Ochoco Reservoir Quadrangle, Crook County, Oregon: United States Geological Survey, Miscellaneous Geologic Investigations Map I-541.

Well logs for CROO 365 and CROO 54251, as well as nearby CROO 680, CROO 683, and CROO51917.

D. WELL CONSTRUCTION, OAR 690-200

D4. **C** Route to the Well Construction and Compliance Section for a review of existing well construction.

Water Availability Tables

burner all real		DETAILED REPORT	ON THE WATER AVAIL	ABILITY CALCULATIO	N	in the second second	
Watershed ID #: Time: 11:29 AM	70611	осно	Exceed	Exceedance Level: 80 Date: 12/16/2015			
Month	Natural Stream Flow	Consumptive Use and Storage	Expected Stream Flow	Reserved Stream Flow	Instream Requirements	Net Water Available	
		Storage is 1	Monthly values a the annual amount a	are in cfs. t 50% exceedance i	n ac-ft.	3	
JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC	15.20 35.40 71.10 96.50 62.30 43.10 12.80 5.78 5.95 3.35 4.94 11.00	58.00 97.80 84.00 109.00 105.00 103.00 130.00 94.90 41.50 5.31 8.63 42.10	-42.80 -62.40 -12.90 -12.30 -42.60 -60.10 -117.00 -89.10 -35.50 -1.96 -3.69 -31.10	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	23.00 35.00 45.00 45.00 35.00 14.70 6.27 6.50 6.89 8.62 23.00	-65.80 -97.40 -57.90 -57.30 -95.10 -132.00 -95.40 -42.00 -8.85 -12.30 -54.00	
ANN	44,600	42.10 53,000	-31.10 11,300	0.00	23.00 17,700	-54.10 5,240	

Well Location Map



Water-Level Trends in Nearby Wells Non available.

Application G-18121

Transient Stream Depletion

		.	Tra	nsient	Stream	Denle	tion (.le	nkins	1970 H	lunt 1	1999			
			Trai	ISIGIN.	Juean	ROO 36	5 to Mill	Creek	1370, 1	MIL, I	5551			
	1.0													
		-			******		*****	******	****					
Stream depletion (fraction of well discharge)	0.9													
	0.8							-			_			
	1													
	0.7										-	-		
			-	_					1					
	0.6						-							
	0.5				_	-					-	_		
	1			-										
	0.4				-				-		-	-		
	0.2													
	0.5	/												
	0.2						-			-				
	1/													
	0.1			-	-									
	00													
	0	30	60	90	120	150	180	210	240	270	300	330	360	
		Time since start of numping (days)												
		1							()-/					
	Jenkins s2				Hunt s1			Hunt s2						
	Jenkins s2 residua			Hunt s3			Hunt s2 residual							
Output	for Hunt	Stream D	Depletion	, Scene	rio 2 (s2)	:	lime pur	np on = 3	65 days					
Days		30	60	90	120	150	180	210	240	270	300	330	360	
Qw, cfs		0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	
Jenk SD s2 %		91.28	93.83	94.96	95.63	96.09	96.43	96.70	96.91	97.09	97.24	97.37	97.48	
Jen SD s2 cfs		0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	
Hunt SD s2 %		30.47	39.92	45.80	50.03	53.30	55.95	58.16	60.04	61.68	63.12	64.40	65.55	
Hunt S	D s2 cfs	0.001	0.001	0.001	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	
-														
Demm	-					6				C			88-24-	
Not stoody pumping sets					0	Scenario 1		Scenario 2		Scenario 3		Units		
Distance to stream					Caw	0.003		0.003		0.003		CIS		
Aquifer bydraulic conductivity					d	120		120		120		Hidau		
Aquifer thickness					N.	300		300		300		ivday		
Aquifer tranemic civity					T	20		20		6000		T.		
Aquiter storage coefficient					e	6000		0000		0000		n-n/day		
Stream width					S NIC	0.3		20		0.3		4		
Streambed hydraulic conductivity					Ke	20		20		20		Ridou		
Streambed thickness					he	3		2		2		IVday		
Streambed conductance					shc	6 666666667		6 666666667		6 666666667		fi/day		
Stream depletion factor (Jenkins)					sdf	0.0000007		0.72		0.72			dave	
Streambed factor (Hunt)					shf	0.133333333		0.133333333		0.133333333				

8

9

