

PUBLIC INTEREST REVIEW FOR GROUNDWATER APPLICATIONS

TO: Water Rights Section Date 04/27/2016
 FROM: Groundwater Section Phillip I. Marcy
Reviewer's Name
 SUBJECT: Application G- 18206 Supersedes review of _____
Date of Review(s)

PUBLIC INTEREST PRESUMPTION; GROUNDWATER

OAR 690-310-130 (1) *The Department shall presume that a proposed groundwater use will ensure the preservation of the public welfare, safety and health as described in ORS 537.525. Department staff review groundwater applications under OAR 690-310-140 to determine whether the presumption is established. OAR 690-310-140 allows the proposed use be modified or conditioned to meet the presumption criteria. This review is based upon available information and agency policies in place at the time of evaluation.*

A. GENERAL INFORMATION: Applicant's Name: Paul Kesler County: Malheur

- A1. Applicant(s) seek(s) 3.56 cfs from 2 well(s) in the Malheur Basin,
 _____ subbasin
- A2. Proposed use Supplemental Irrigation (447.2 acres) Seasonality: March 1st – October 31st (245 days)
- A3. Well and aquifer data (attach and number logs for existing wells; mark proposed wells as such under logid):

| Well | Logid | Applicant's Well # | Proposed Aquifer* | Proposed Rate(cfs) | Location (T/R-S QQ-Q) | Location, metes and bounds, e.g. 2250' N, 1200' E fr NW cor S 36 |
|------|------------|--------------------|-------------------|--------------------|-----------------------|--|
| 1 | MALH 54160 | 1 | Alluvium | 1.78 | 19S/46E SW-NE | 2600'S, 3160'E fr NW cor S 14 |
| 2 | MALH 54229 | 2 | Alluvium | 1.78 | 19S/46E NW-SW | 1380'N, 300'E fr SW cor S 14 |
| 3 | | | | | | |
| 4 | | | | | | |
| 5 | | | | | | |

* Alluvium, CRB, Bedrock

| Well | Well Elev ft msl | First Water ft bls | SWL ft bls | SWL Date | Well Depth (ft) | Seal Interval (ft) | Casing Intervals (ft) | Liner Intervals (ft) | Perforations Or Screens (ft) | Well Yield (gpm) | Draw Down (ft) | Test Type |
|------|------------------|--------------------|------------|------------|-----------------|--------------------|-----------------------|----------------------|------------------------------|------------------|----------------|-----------|
| 1 | 2470 | 199 | 76.75 | 11/04/2015 | 504 | 0-196 | +1.5-201 | None | 201-504 | 550 | 15 | Pump |
| 2 | 2463 | 15 | 80.60 | 11/04/2015 | 520 | 0-125 | +1.5-220 | None | 220-488 | 500 | ? | Air |
| | | | | | | | | | | | | |

Use data from application for proposed wells.

- A4. **Comments:** Both wells are constructed to produce groundwater from sand and gravel lenses within the Glens Ferry Formation. Reported yields for each well do not match the requested maximum rate of 800 GPM.
- A5. **Provisions of the Malheur (690-510) Basin rules relative to the development, classification and/or management of groundwater hydraulically connected to surface water are, or are not, activated by this application. (Not all basin rules contain such provisions.)**
 Comments: _____
- A6. **Well(s) # _____, _____, _____, _____, _____, tap(s) an aquifer limited by an administrative restriction. Name of administrative area: _____**
 Comments: _____

B. GROUNDWATER AVAILABILITY CONSIDERATIONS, OAR 690-310-130, 400-010, 410-0070

B1. Based upon available data, I have determined that groundwater* for the proposed use:

- a. is over appropriated, is not over appropriated, or cannot be determined to be over appropriated during any period of the proposed use. * This finding is limited to the groundwater portion of the over-appropriation determination as prescribed in OAR 690-310-130;
- b. will not or will likely be available in the amounts requested without injury to prior water rights. * This finding is limited to the groundwater portion of the injury determination as prescribed in OAR 690-310-130;
- c. will not or will likely to be available within the capacity of the groundwater resource; or
- d. will, if properly conditioned, avoid injury to existing groundwater rights or to the groundwater resource:
 - i. The permit should contain condition #(s) 7N;
 - ii. The permit should be conditioned as indicated in item 2 below.
 - iii. The permit should contain special condition(s) as indicated in item 3 below;

- B2. a. Condition to allow groundwater production from no deeper than _____ ft. below land surface;
- b. Condition to allow groundwater production from no shallower than _____ ft. below land surface;
- c. Condition to allow groundwater production only from the _____ groundwater reservoir between approximately _____ ft. and _____ ft. below land surface;
- d. Well reconstruction is necessary to accomplish one or more of the above conditions. The problems that are likely to occur with this use and without reconstructing are cited below. Without reconstruction, I recommend withholding issuance of the permit until evidence of well reconstruction is filed with the Department and approved by the Groundwater Section.

Describe injury –as related to water availability– that is likely to occur without well reconstruction (interference w/ senior water rights, not within the capacity of the resource, etc): _____

B3. **Groundwater availability remarks:** Little groundwater data is available for this area, but drought measurements for each of the two proposed POA wells in November of 2015 show no evidence of water level decline after 1 season of use. Gannett (1990) concluded that groundwater development within the Glenns Ferry Formation should be approached with caution, due to the possibility that overdrafting may cause infiltration from overlying shallow systems. This could potentially introduce a variety of contaminants into the Glenns Ferry aquifer system.

C. GROUNDWATER/SURFACE WATER CONSIDERATIONS, OAR 690-09-040

C1. **690-09-040 (1):** Evaluation of aquifer confinement:

| Well | Aquifer or Proposed Aquifer | Confined | Unconfined |
|------|----------------------------------|--------------------------|-------------------------------------|
| 1 | Sand lenses with Glens Ferry Fmn | <input type="checkbox"/> | <input checked="" type="checkbox"/> |
| 2 | Sand lenses with Glens Ferry Fmn | <input type="checkbox"/> | <input checked="" type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> |

Basis for aquifer confinement evaluation: Studies conducted by the Department have concluded that the Glens Ferry Formation discharges groundwater to the overlying sand and gravel aquifer (Gannett, 1990). This conclusion is based partially upon the fact that groundwater elevations within wells completed into the Glens Ferry Formation are substantially higher than in wells completed into the near-surface sand and gravel aquifer. While this also illustrates some degree of confinement, our conceptual model of this deeper aquifer includes a lack of laterally continuous lithologies, as reported on local well logs. Within this framework, vertical migration of groundwater is likely inefficient, and variable by location and distribution of fine-grained sediments above the production zone.

C2. **690-09-040 (2) (3):** Evaluation of distance to, and hydraulic connection with, surface water sources. All wells located a horizontal distance less than ¼ mile from a surface water source that produce water from an unconfined aquifer shall be assumed to be hydraulically connected to the surface water source. Include in this table any streams located beyond one mile that are evaluated for PSI.

| Well | SW # | Surface Water Name | GW Elev ft msl | SW Elev ft msl | Distance (ft) | Hydraulically Connected? | | | Potential for Subst. Interfer. Assumed? | |
|------|------|--------------------|----------------|----------------|---------------|-------------------------------------|--------------------------|--------------------------|---|-------------------------------------|
| | | | | | | YES | NO | ASSUMED | YES | NO |
| 1 | 1 | Snake River | 2393 | 2163 | 19000 | <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> |
| 2 | 2 | Snake River | 2382 | 2163 | 21850 | <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> |
| | | | | | | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| | | | | | | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| | | | | | | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| | | | | | | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |

Basis for aquifer hydraulic connection evaluation: The Glens Ferry Formation is incised by the channel of the Snake River, where horizontal movement of groundwater results in discharge to the stream. There is likely a surficial deposit of low-permeability silts and clays within the stream channel and floodplain, which may inhibit this flow to some degree.

Water Availability Basin the well(s) are located within: None

C3a. **690-09-040 (4):** Evaluation of stream impacts for each well that has been determined or assumed to be hydraulically connected and less than 1 mile from a surface water source. Limit evaluation to instream rights and minimum stream flows that are pertinent to that surface water source, and not lower SW sources to which the stream under evaluation is tributary. Compare the requested rate against the 1% of 80% natural flow for the pertinent Water Availability Basin (WAB). If Q is not distributed by well, use full rate for each well. Any checked box indicates the well is assumed to have the potential to cause PSI.

| Well | SW # | Well < ¼ mile? | Qw > 5 cfs? | Instream Water Right ID | Instream Water Right Q (cfs) | Qw > 1% ISWR? | 80% Natural Flow (cfs) | Qw > 1% of 80% Natural Flow? | Interference @ 30 days (%) | Potential for Subst. Interfer. Assumed? |
|------|------|--------------------------|--------------------------|-------------------------|------------------------------|--------------------------|------------------------|------------------------------|----------------------------|---|
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |

C3b. **690-09-040 (4):** Evaluation of stream impacts by total appropriation for all wells determined or assumed to be **hydraulically connected and less than 1 mile** from a surface water source. **Complete only if Q is distributed among wells.** Otherwise same evaluation and limitations apply as in C3a above.

| | SW # | Qw > 5 cfs? | Instream Water Right ID | Instream Water Right Q (cfs) | Qw > 1% ISWR? | 80% Natural Flow (cfs) | Qw > 1% of 80% Natural Flow? | Interference @ 30 days (%) | Potential for Subst. Interfer. Assumed? |
|--|------|--------------------------|-------------------------|------------------------------|--------------------------|------------------------|------------------------------|----------------------------|---|
| | | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |
| | | <input type="checkbox"/> | | | <input type="checkbox"/> | | <input type="checkbox"/> | | <input type="checkbox"/> |

Comments: This section does not apply.

C4a. **690-09-040 (5):** Estimated impacts on **hydraulically connected surface water sources greater than one mile** as a percentage of the proposed pumping rate. Limit evaluation to the effects that will occur up to one year after pumping begins. This table encompasses the considerations required by 09-040 (5)(a), (b), (c) and (d), which are not included on this form. Use additional sheets if calculated flows from more than one WAB are required.

| Non-Distributed Wells | | | | | | | | | | | | | |
|-----------------------|----------|-----|-----|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|---------------|---------------|
| Well | SW# | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| | | % | % | % | % | % | % | % | % | % | % | % | % |
| Well Q as CFS | | | | | | | | | | | | | |
| Interference CFS | | | | | | | | | | | | | |
| Distributed Wells | | | | | | | | | | | | | |
| Well | SW# | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| 1 | 1 | % | % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.01 % | 0.01 % |
| Well Q as CFS | | | | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | | |
| Interference CFS | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 2 | 1 | % | % | 0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % | 0.0 % |
| Well Q as CFS | | | | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 | | |
| Interference CFS | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | % | % | % | % | % | % | % | % | % | % | % | % |
| Well Q as CFS | | | | | | | | | | | | | |
| Interference CFS | | | | | | | | | | | | | |
| | | % | % | % | % | % | % | % | % | % | % | % | % |
| Well Q as CFS | | | | | | | | | | | | | |
| Interference CFS | | | | | | | | | | | | | |
| | | % | % | % | % | % | % | % | % | % | % | % | % |
| Well Q as CFS | | | | | | | | | | | | | |
| Interference CFS | | | | | | | | | | | | | |
| (A) = Total Interf. | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| (B) = 80 % Nat. Q | | | | 467 | 780 | 524 | 324 | 150 | 100 | 84 | 106 | 135 | 132 |
| (C) = 1 % Nat. Q | | | | 4.67 | 7.80 | 5.24 | 3.24 | 1.50 | 1.00 | 0.84 | 1.06 | 1.35 | 1.32 |
| (D) = (A) > (C) | | | | | | | | | | | | | |
| (E) = (A / B) x 100 | | % | % | 0 % | 0 % | 0 % | 0 % | 0 % | 0 % | 0 % | 0 % | 0 % | 0 % |

(A) = total interference as CFS; (B) = WAB calculated natural flow at 80% exceed. as CFS; (C) = 1% of calculated natural flow at 80% exceed. as CFS; (D) = highlight the checkmark for each month where (A) is greater than (C); (E) = total interference divided by 80% flow as percentage.

Basis for impact evaluation: Evaluation of expected impacts to the Snake River were calculated using the model of Hunt (2003) to consider the effects of low-permeability beds within the aquifer in addition to fine-grained fluvial sediments within the stream channel. A range of hydraulic conductivity values were used that fell within the range of local pump test results from the deeper Glens Ferry Formation aquifer. The calculated impacts to the Snake river were negligible for both proposed POAs, largely due to their distance from the stream.

C4b. **690-09-040 (5) (b)** The potential to impair or detrimentally affect the public interest is to be determined by the Water Rights Section.

C5. **If properly conditioned**, the surface water source(s) can be adequately protected from interference, and/or groundwater use under this permit can be regulated if it is found to substantially interfere with surface water:

- i. The permit should contain condition #(s) _____;
- ii. The permit should contain special condition(s) as indicated in "Remarks" below;

C6. **SW / GW Remarks and Conditions:** The large distance of the two proposed POA wells from the Snake River results in minimal projected impacts from the proposed pumping rate.

References Used:

Gannett, M.W. 1990, Hydrogeology of the Ontario Area, Malheur County, Oregon: Oregon Water Resources Department Groundwater Report No. 34.

Ferns, M.L., Brooks, H.C., Evans, J.G., and Cummings, M.L. 1993. Geologic Map of the Vale 30 X 60 Minute Quadrangle, Malheur County, Oregon, and Owyhee County, Idaho: Oregon Department of Geology and Mineral Industries Geological Map Series GMS-77, scale 1:100,000.

Local well log reports; pump tests.

D. WELL CONSTRUCTION, OAR 690-200

D1. Well #: _____ Logid: _____

D2. **THE WELL does not appear to meet current well construction standards based upon:**

- a. review of the well log;
- b. field inspection by _____;
- c. report of CWRE _____;
- d. other: (specify) _____

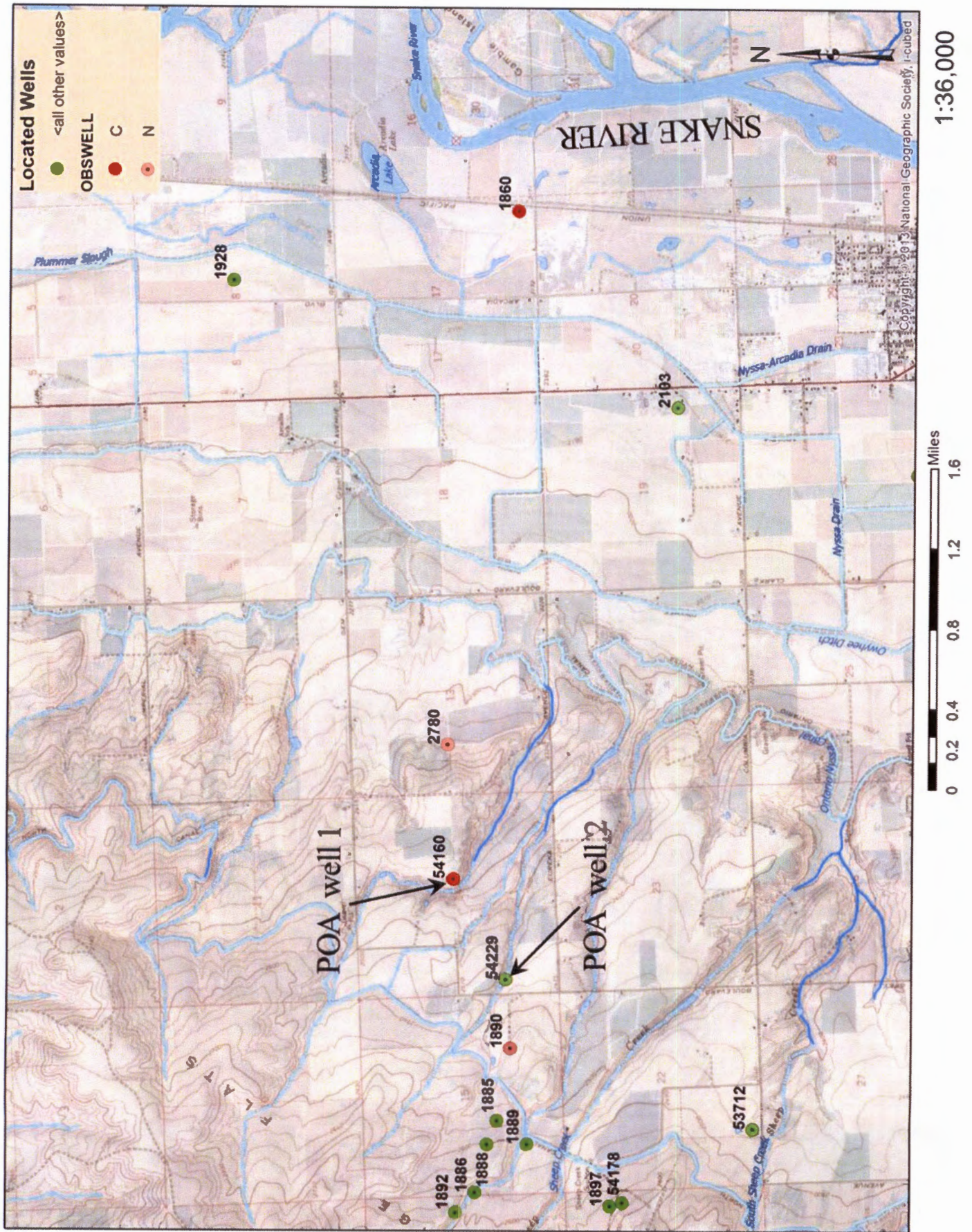
D3. **THE WELL construction deficiency or other comment is described as follows:** _____

D4. Route to the Well Construction and Compliance Section for a review of existing well construction.

Water Availability Tables (nearby WAB to north)

| DETAILED REPORT ON THE WATER AVAILABILITY CALCULATION | | | | | | |
|--|---------------------|--------------------------------|----------------------|----------------------|-----------------------|---------------------|
| Watershed ID #: 31011701 | | MALHEUR R > SNAKE R - AT MOUTH | | | Exceedance Level: 80 | |
| Time: 11:45 AM | | Basin: MALHEUR | | | Date: 04/27/2016 | |
| Month | Natural Stream Flow | Consumptive Use and Storage | Expected Stream Flow | Reserved Stream Flow | Instream Requirements | Net water Available |
| Monthly values are in cfs. Storage is the annual amount at 50% exceedance in ac-ft. | | | | | | |
| JAN | 154.00 | 427.00 | -273.00 | 0.00 | 0.00 | -273.00 |
| FEB | 267.00 | 626.00 | -359.00 | 0.00 | 0.00 | -359.00 |
| MAR | 467.00 | 911.00 | -444.00 | 329.00 | 0.00 | -774.00 |
| APR | 780.00 | 1,060.00 | -278.00 | 470.00 | 0.00 | -748.00 |
| MAY | 524.00 | 957.00 | -433.00 | 0.00 | 0.00 | -433.00 |
| JUN | 324.00 | 857.00 | -533.00 | 0.00 | 0.00 | -533.00 |
| JUL | 150.00 | 686.00 | -536.00 | 0.00 | 0.00 | -536.00 |
| AUG | 99.90 | 540.00 | -440.00 | 0.00 | 0.00 | -440.00 |
| SEP | 83.80 | 376.00 | -292.00 | 0.00 | 0.00 | -292.00 |
| OCT | 106.00 | 209.00 | -103.00 | 0.00 | 0.00 | -103.00 |
| NOV | 135.00 | 223.00 | -87.90 | 0.00 | 0.00 | -87.90 |
| DEC | 132.00 | 297.00 | -165.00 | 0.00 | 0.00 | -165.00 |
| ANN | 338,000 | 432,000 | 29,500 | 48,200 | 0 | 0 |

Well Location Map



Water-Level Trends in Nearby Wells

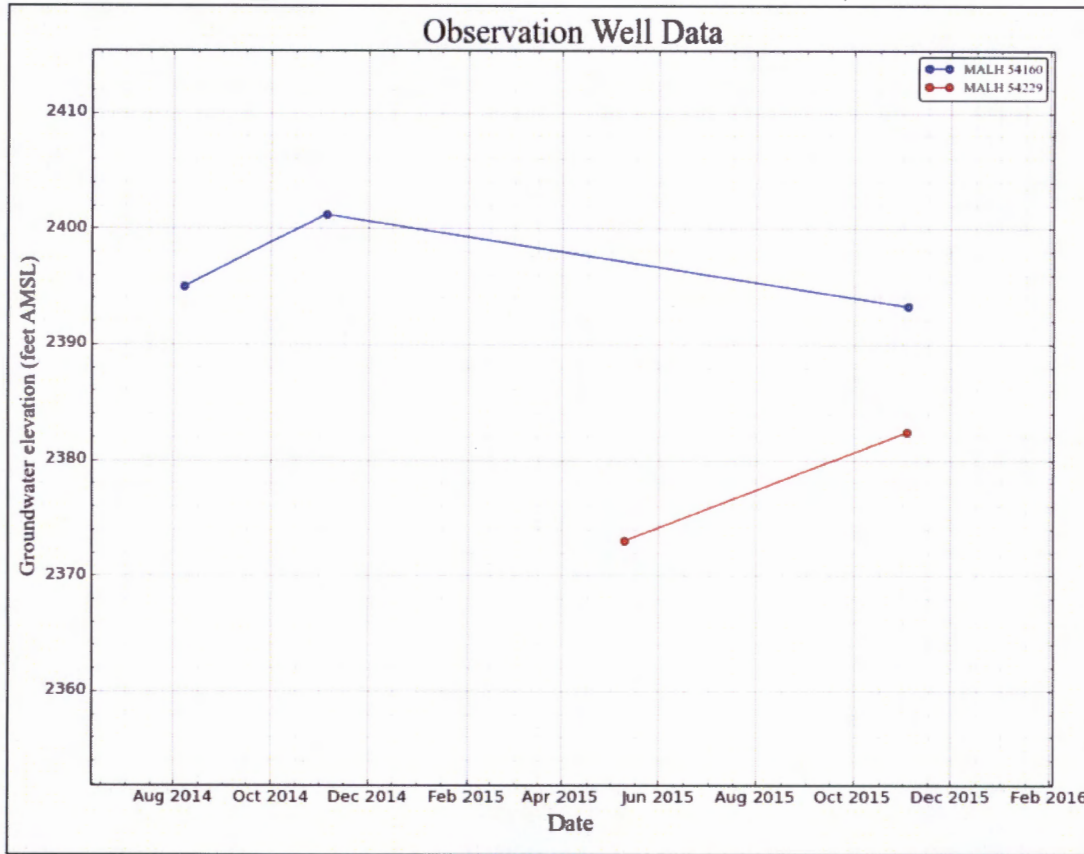
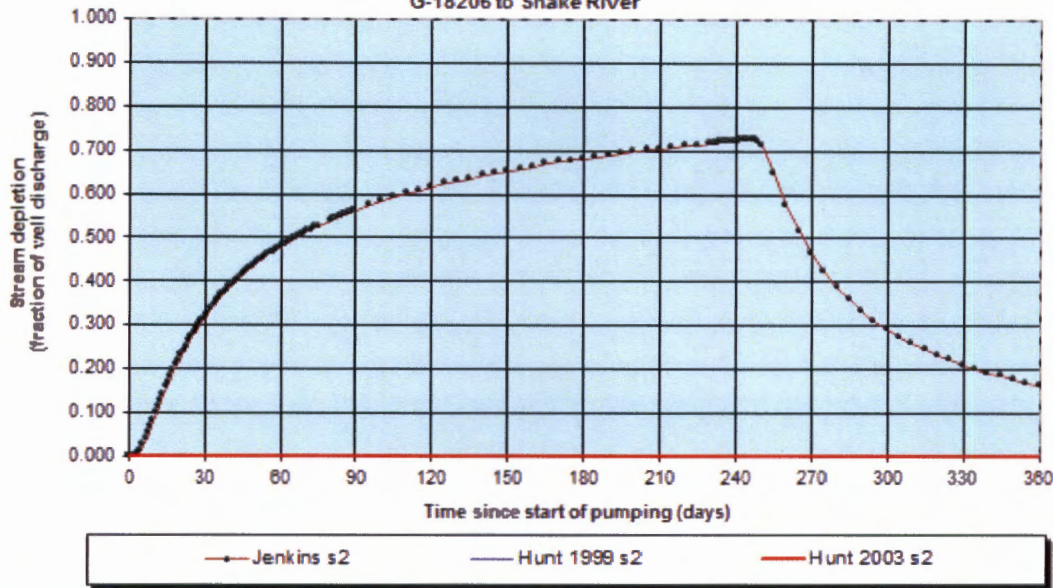


Figure 1: Recent water level data from the two POA wells on this application do not indicate measurable declines from pumping under drought permit in 2015. Little other groundwater data is available for this area, particularly for wells within the Glenns Ferry Formation.

Transient Stream Depletion (Jenkins, 1970; Hunt, 1999, 2003)

G-18206 to Snake River



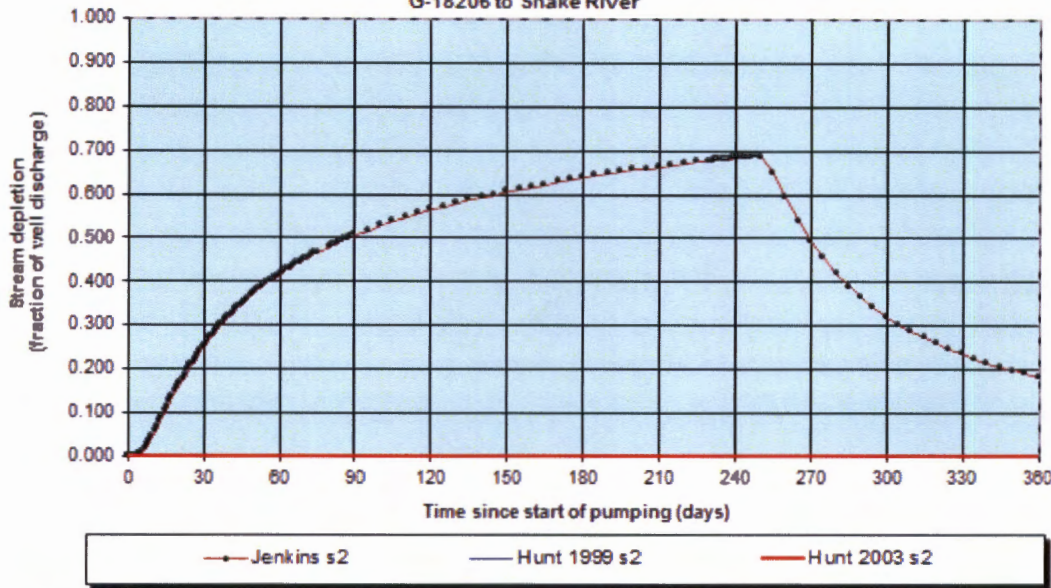
| Output for Stream Depletion, Scenerio 2 (s2): | | | | | | | | | | | | | Time pump on (pumping duration) = 245 days | |
|---|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|-------|--|--|
| Days | 30 | 60 | 90 | 120 | 150 | 180 | 210 | 240 | 270 | 300 | 330 | 360 | | |
| JSD | 31.7% | 47.9% | 56.3% | 61.7% | 65.4% | 68.3% | 70.5% | 72.3% | 46.6% | 29.2% | 21.1% | 16.3% | | |
| HSD 1999 | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | | |
| HSD 2003 | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | 0.01% | 0.01% | 0.01% | 0.01% | | |
| Q _w , cfs | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | | |
| HSD 99, cfs | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | | |
| HSD 03, cfs | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | |

| Parameters: | | Scenario 1 | Scenario 2 | Scenario 3 | Units |
|---|------------------|-------------|--------------|--------------|----------------------|
| Net steady pumping rate of well | Q _w | 1.78 | 1.78 | 1.78 | cfs |
| Time pump on (pumping duration) | t _{pon} | 245 | 245 | 245 | days |
| Perpendicular from well to stream | a | 19000 | 19000 | 19000 | ft |
| Well depth | d | 504 | 504 | 504 | ft |
| Aquifer hydraulic conductivity | K | 50 | 50 | 50 | ft/day |
| Aquifer saturated thickness | b | 120 | 120 | 120 | ft |
| Aquifer transmissivity | T | 6000 | 6000 | 6000 | ft ² /day |
| Aquifer storativity or specific yield | S | 0.001 | 0.001 | 0.001 | |
| Aquitard vertical hydraulic conductivity | K _{va} | 0.5 | 5 | 25 | ft/day |
| Aquitard saturated thickness | b _a | 20 | 20 | 20 | ft |
| Aquitard thickness below stream | b _{abs} | 3 | 3 | 3 | ft |
| Aquitard porosity | n | 0.2 | 0.2 | 0.2 | |
| Stream width | w _s | 500 | 500 | 500 | ft |
| Streambed conductance (lambda) | sbc | 83.333333 | 833.333333 | 4166.666667 | ft/day |
| Stream depletion factor | sdf | 60.166667 | 60.166667 | 60.166667 | days |
| Streambed factor | sbf | 263.888889 | 2638.888889 | 13194.444444 | |
| input #1 for Hunt's Q ₄ function | t' | 0.016620 | 0.016620 | 0.016620 | |
| input #2 for Hunt's Q ₄ function | K' | 1504.166667 | 15041.666667 | 75208.333333 | |
| input #3 for Hunt's Q ₄ function | epsilon' | 0.005000 | 0.005000 | 0.005000 | |
| input #4 for Hunt's Q ₄ function | lamda' | 263.888889 | 2638.888889 | 13194.444444 | |

Figure 2: Hunt (2003) calculation of expected stream interference from pumping at POA 1.

Transient Stream Depletion (Jenkins, 1970; Hunt, 1999, 2003)

G-18206 to Snake River



| Output for Stream Depletion, Scenario 2 (s2): | | | | | | | | | | | | | Time pump on (pumping duration) = 245 days | | | |
|---|--------|--------|--------|--------|--------|--------|--------|--------|-------|-------|-------|-------|--|--|--|--|
| Days | 30 | 60 | 90 | 120 | 150 | 180 | 210 | 240 | 270 | 300 | 330 | 360 | | | | |
| JSD | 24.9% | 41.5% | 50.6% | 56.5% | 60.7% | 63.8% | 66.3% | 68.4% | 49.4% | 32.1% | 23.5% | 18.3% | | | | |
| HSD 1999 | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | | | | |
| HSD 2003 | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | -0.01% | 0.00% | 0.00% | 0.00% | 0.00% | | | | |
| Q _w , cfs | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | 1.780 | | | | |
| HSD 99, cfs | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | ##### | | | | |
| HSD 03, cfs | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | | | |

| Parameters: | | Scenario 1 | Scenario 2 | Scenario 3 | Units |
|---|------------------|-------------|--------------|--------------|----------------------|
| Net steady pumping rate of well | Q _w | 1.78 | 1.78 | 1.78 | cfs |
| Time pump on (pumping duration) | t _{pon} | 245 | 245 | 245 | days |
| Perpendicular from well to stream | a | 21850 | 21850 | 21850 | ft |
| Well depth | d | 504 | 504 | 504 | ft |
| Aquifer hydraulic conductivity | K | 50 | 50 | 50 | ft/day |
| Aquifer saturated thickness | b | 120 | 120 | 120 | ft |
| Aquifer transmissivity | T | 6000 | 6000 | 6000 | ft ² /day |
| Aquifer storativity or specific yield | S | 0.001 | 0.001 | 0.001 | |
| Aquitard vertical hydraulic conductivity | K _{va} | 1 | 5 | 10 | ft/day |
| Aquitard saturated thickness | b _a | 20 | 20 | 20 | ft |
| Aquitard thickness below stream | b _{abs} | 3 | 3 | 3 | ft |
| Aquitard porosity | n | 0.2 | 0.2 | 0.2 | |
| Stream width | w _s | 500 | 500 | 500 | ft |
| Streambed conductance (lambda) | sbc | 166.666667 | 833.333333 | 1666.666667 | ft/day |
| Stream depletion factor | sdf | 79.570417 | 79.570417 | 79.570417 | days |
| Streambed factor | sbf | 606.944444 | 3034.722222 | 6069.444444 | |
| input #1 for Hunt's Q ₄ function | t' | 0.012567 | 0.012567 | 0.012567 | |
| input #2 for Hunt's Q ₄ function | K' | 3978.520833 | 19892.604167 | 39785.208333 | |
| input #3 for Hunt's Q ₄ function | epsilon' | 0.005000 | 0.005000 | 0.005000 | |
| input #4 for Hunt's Q ₄ function | lamda' | 606.944444 | 3034.722222 | 6069.444444 | |

Figure 3: Hunt (2003) calculation of expected stream interference due to pumping at POA 2.